

INTEGRATED design solutions architecture engineering interiors & technology

AREA "A"

SAVAGE RD

LEGAL DESCRIPTION

1441 west long lake, suite 200 troy, michigan 48098

5211 cascade road SE, suite 300 grand rapids, michigan 49546 248.823.2100 www.ids-michigan.com

CIVIL ENGINEER

SPALDING DeDECKER 905 south blvd. E rochester hills, michigan 48307 800.598.1600 www.sda-eng.com

STRUCTURAL ENGINEER

SDI Structures 275 east liberty ann arbor, michigan 48104 734.213.6091 www.sdistructures.com



Van Buren Public Schools

The Early Childhood **Development Center**

Belleville, MI 48111

Project Administra	ator
V. Gra	ant
Project Desig	
J. Ensl	еу
Project Architect / Engine	
J. Ensl	
Drawn	-
C. Ya	
Q.M. Revi	
T. Sov	
Approv	
T. So	
Drawing Sc As Not	
AS NO	.ec
Issued for Issue Da	ite
Design Development 06-19-20	20
Bid Package 1 08-14-20	20
Addendum No. 3 09-08-20	20
City Engineering Review No. 2 11-02-20	20
Bulletin No. 1 11-04-20	20
City Engineering Review No. 3 11-18-20	20
City Engineering Revisions 12-07-20	20
EGLE Water Supply Permit 12-07-20	20
Bulletin No. 1 Revised 12-08-20	20

© 2020 INTEGRATED design solutions, LLC

IDS Drawing Title

General Plan

ISSUED FOR REFERENCE ONLY

ī**D** § Project Number

OWNER

VAN BUREN PUBLIC SCHOOLS

555 W. COLUMBIA AVE.

PHONE: (734) 697-9123

BELLEVILLE, MI 48111

FAX: (734) 697-6385

Drawing Number C0.1



INTEGRATED design SOLUTIONS architecture engineering interiors & technology

1441 west long lake, suite 200 troy, michigan 48098 5211 cascade road SE, suite 300 grand rapids, michigan 49546 248.823.2100

CIVIL ENGINEER

SPALDING DeDECKER 905 south blvd. E rochester hills, michigan 48307 800.598.1600 www.sda-eng.com

STRUCTURAL ENGINEER SDI Structures

275 east liberty ann arbor, michigan 48104 734.213.6091 www.sdistructures.com



Van Buren Public Schools

The Early Childhood **Development Center**

Belleville, MI 48111

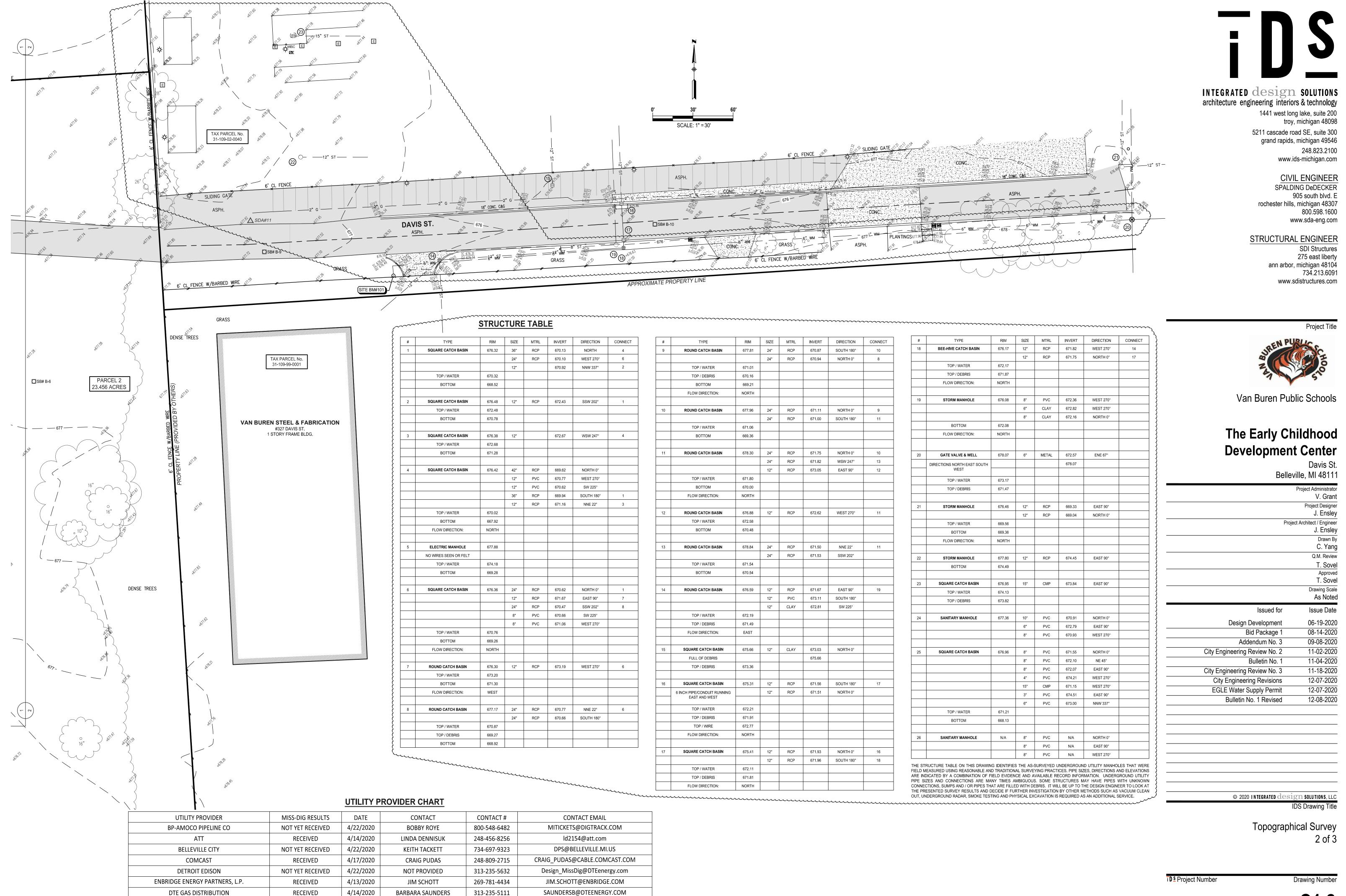
	Project Designer
	J. Ensley
Proj	ect Architect / Engineer
	J. Ensley
	Drawn By
	C. Yang
	Q.M. Review
	T. Sovel
	Approved
	T. Sovel
	Drawing Scale
	As Noted
Issued for	Issue Date
Design Development	06-19-2020
Bid Package 1	08-14-2020
Addendum No. 3	09-08-2020
City Engineering Review No. 2	11-02-2020
Bulletin No. 1	11-04-2020
City Engineering Review No. 3	11-18-2020
City Engineering Revisions	12-07-2020
	12-07-2020
EGLE Water Supply Permit	12-01-2020
EGLE Water Supply Permit Bulletin No. 1 Revised	12-07-2020

© 2020 INTEGRATED design solutions, LLC IDS Drawing Title

> Topographical Survey 1 of 3

> > Drawing Number

C1.1



MLADD@VANBUREN-MI.ORG

LOUIS_KRAUS@WPLCO.COM

VAN BUREN TOWNSHIP

WOLVERINE PIPELINE CO

4/22/2020

4/14/2020

MARTY LADD

LOUIS KRAUS

734-699-8900

269-323-2491

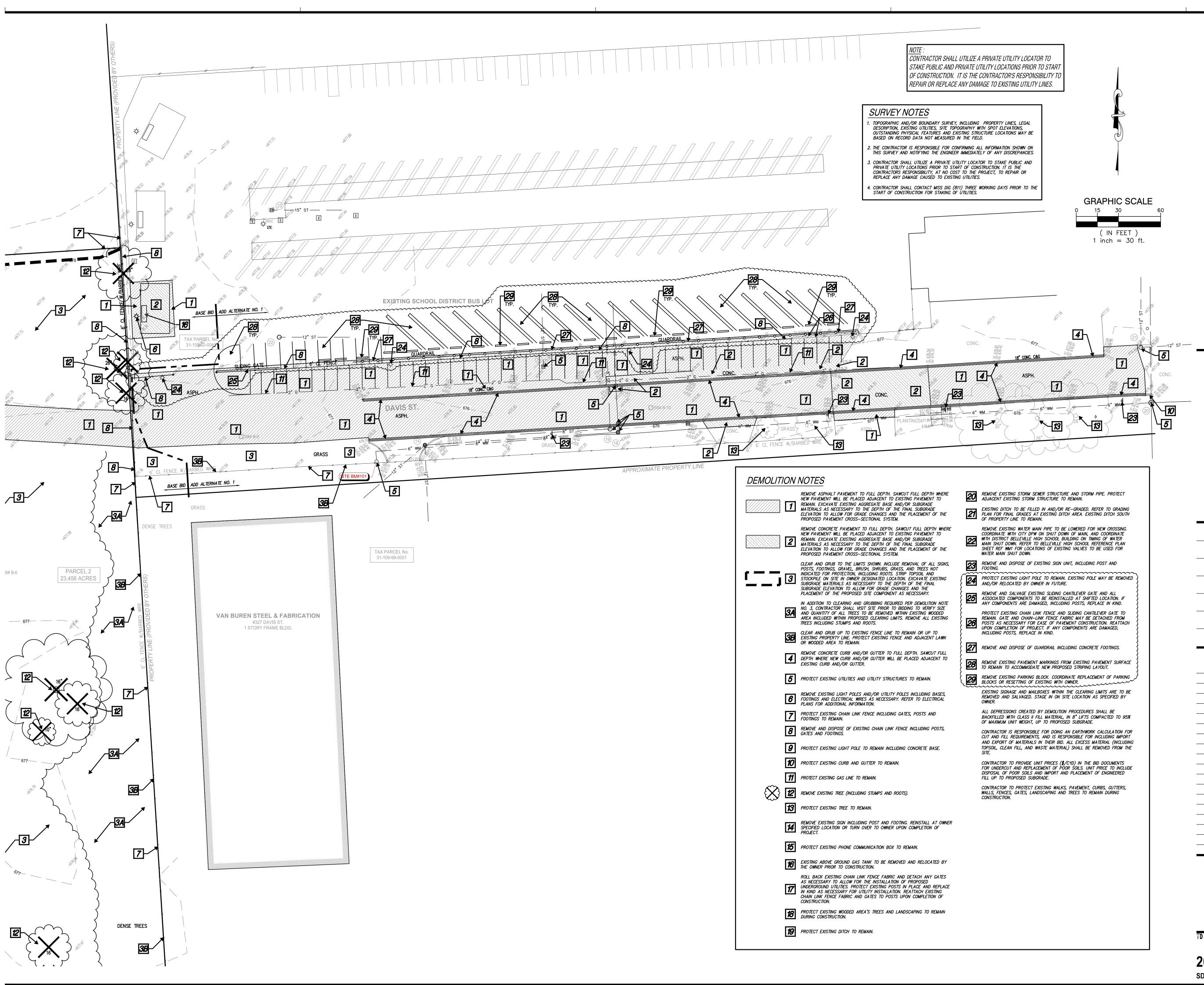
NOT YET RECEIVED

RECEIVED



Project Administrator	
V. Grant	
Project Designer	
J. Ensley	
t Architect / Engineer	
J. Ensley	
Drawn By	
C. Yang	
Q.M. Review	
T. Sovel	
Approved	
T. Sovel	
Drawing Scale	
As Noted	
Issue Date	Issued for
06-19-2020	Design Development
08-14-2020	Bid Package 1
09-08-2020	Addendum No. 3
11-02-2020	City Engineering Review No. 2
11-04-2020	Bulletin No. 1
11-18-2020	City Engineering Review No. 3
40.07.0000	Oit - Englis a guina Daviaiana

SDA Project No. NP20062



INTEGRATED design SOLUTIONS architecture engineering interiors & technology 1441 west long lake, suite 200

troy, michigan 48098
5211 cascade road SE, suite 300
grand rapids, michigan 49546
248.823.2100

CIVIL ENGINEER
SPALDING DeDECKER
905 south blvd. E
rochester hills, michigan 48307

www.ids-michigan.com

800.598.1600

www.sda-eng.com

STRUCTURAL ENGINEER

SDI Structures
275 east liberty

275 east liberty ann arbor, michigan 48104 734.213.6091 www.sdistructures.com

Project Title



Van Buren Public Schools

The Early Childhood Development Center

Davis St. Belleville, MI 48111

•	
Project Administrator V. Grant	
Project Designer J. Ensley	
ct Architect / Engineer J. Ensley	
Drawn By C. Yang	
Q.M. Review	
T. Sovel	
Approved T. Sovel	
Drawing Scale As Noted	
Issue Date	Issued for
06-19-2020	Design Development
08-14-2020	Bid Package 1
09-08-2020	Addendum No. 3
11-02-2020	City Engineering Review No. 2
11-04-2020	Bulletin No. 1
11-18-2020	City Engineering Review No. 3
40.07.000	01/ = 1 1 5 11

City Engineering Revisions

EGLE Water Supply Permit

Bulletin No. 1 Revised

Bulletin No. 6

Bulletin No. 8

© 2020 INTEGRATED design solutions, LLC IDS Drawing Title

Demolition Plan Area "A"

12-07-2020

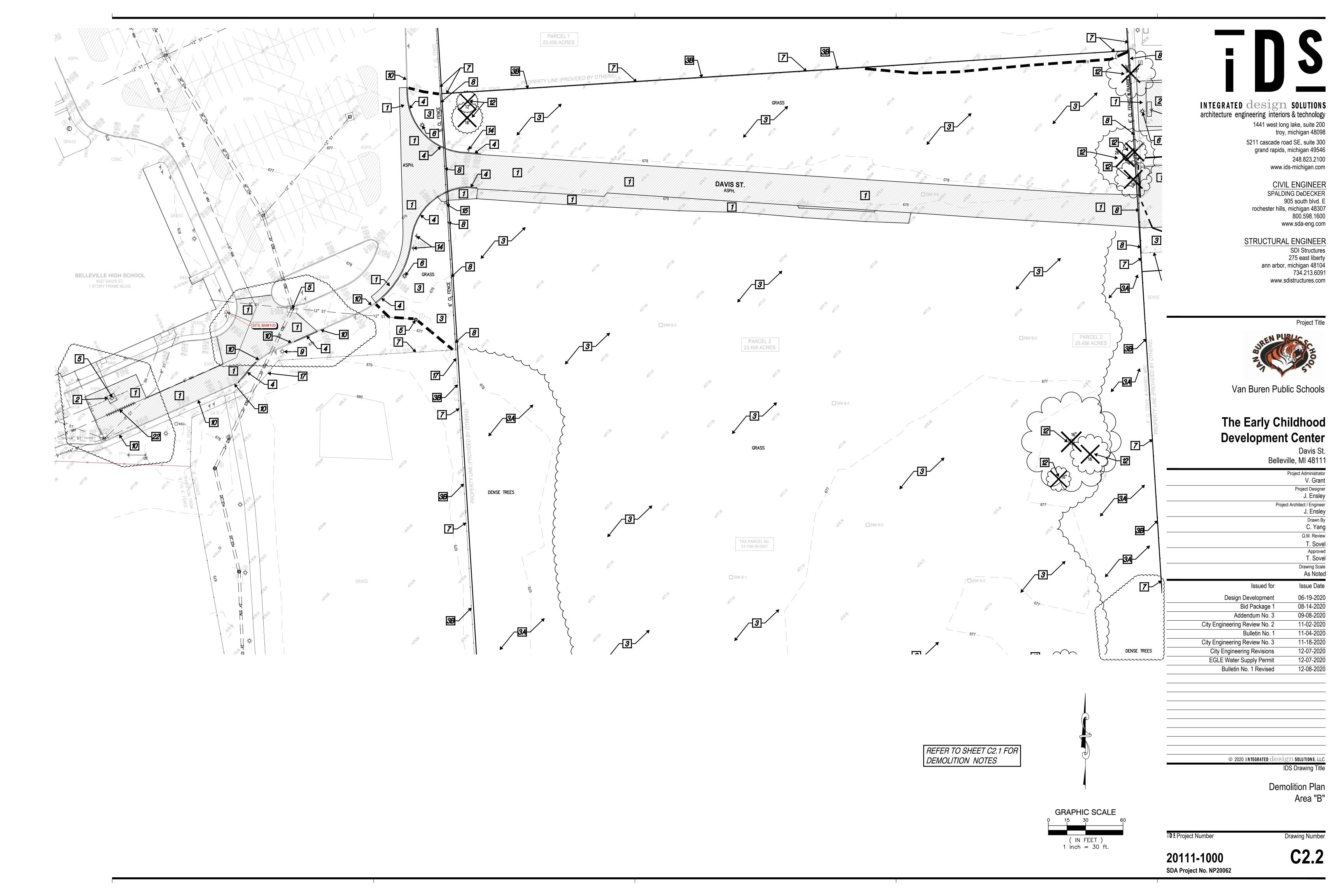
12-08-2020

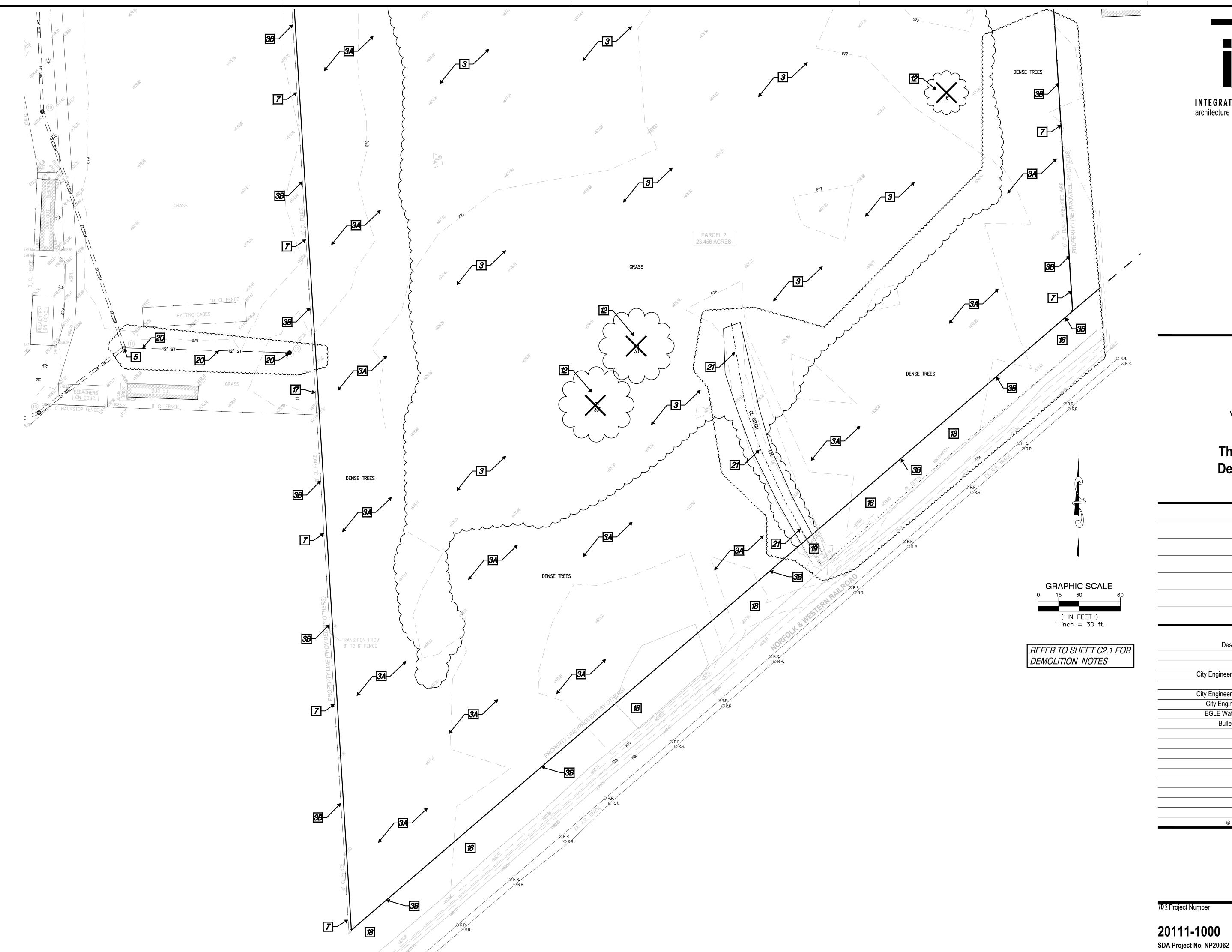
06-16-2021

09-28-2021

ī**D** § Project Number

Drawing Number





INTEGRATED design solutions architecture engineering interiors & technology

1441 west long lake, suite 200 troy, michigan 48098 5211 cascade road SE, suite 300 grand rapids, michigan 49546

248.823.2100 www.ids-michigan.com

CIVIL ENGINEER
SPALDING DeDECKER
905 south blvd. E
rochester hills, michigan 48307
800.598.1600
www.sda-eng.com

STRUCTURAL ENGINEER

SDI Structures
275 east liberty
ann arbor, michigan 48104
734.213.6091
www.sdistructures.com



Van Buren Public Schools

The Early Childhood **Development Center**

Davis St. Belleville, MI 48111

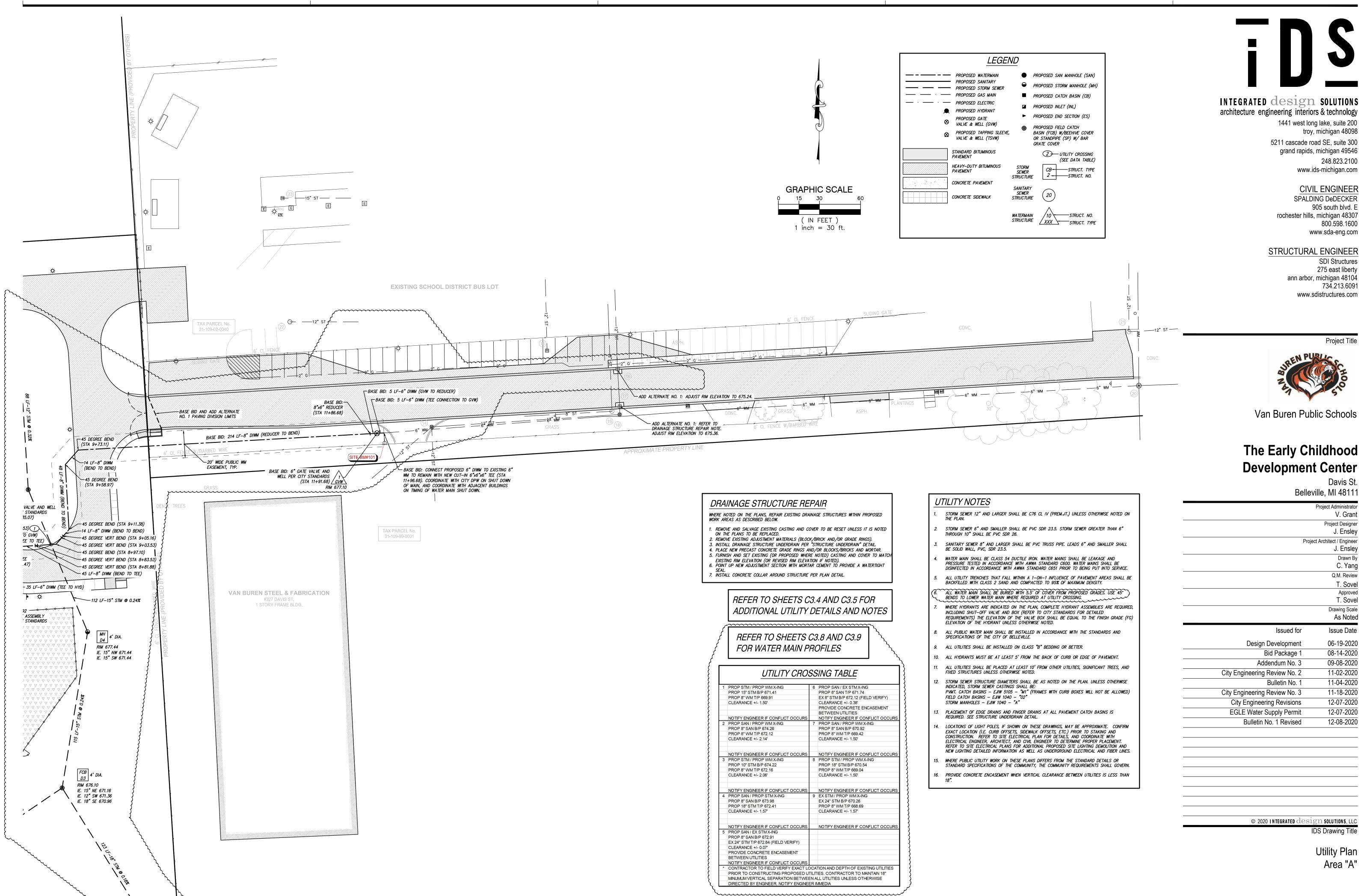
	Project Administrator
	V. Grant
	Project Designer
	J. Ensley
	Project Architect / Engineer
	J. Ensley
	Drawn By
	C. Yang
	Q.M. Review
	T. Sovel
	Approved
	T. Sovel
	Drawing Scale
	As Noted
Issued for	r Issue Date
Design Development	06-19-2020
Bid Package 1	08-14-2020
Addendum No. 3	09-08-2020
City Engineering Review No. 2	11-02-2020
Bulletin No. 1	11-04-2020
City Engineering Review No. 3	11-18-2020
City Engineering Revisions	12-07-2020
EGLE Water Supply Permit	12-07-2020
Bulletin No. 1 Revised	12-08-2020

 \circ 2020 integrated design solutions, LLC IDS Drawing Title

Demolition Plan Area "C"

Drawing Number

C2.3



RIM 677.00

IE. 18" NW 670.74

ī**D** § Project Number **Drawing Number**

248.823.2100

800.598.1600

SDI Structures 275 east liberty

734.213.6091

Project Administrator

V. Grant

J. Ensley

Drawn By

C. Yang

Approved

T. Sovel

Drawing Scale

Issue Date

06-19-2020

08-14-2020

09-08-2020

11-02-2020

11-04-2020

11-18-2020

12-07-2020

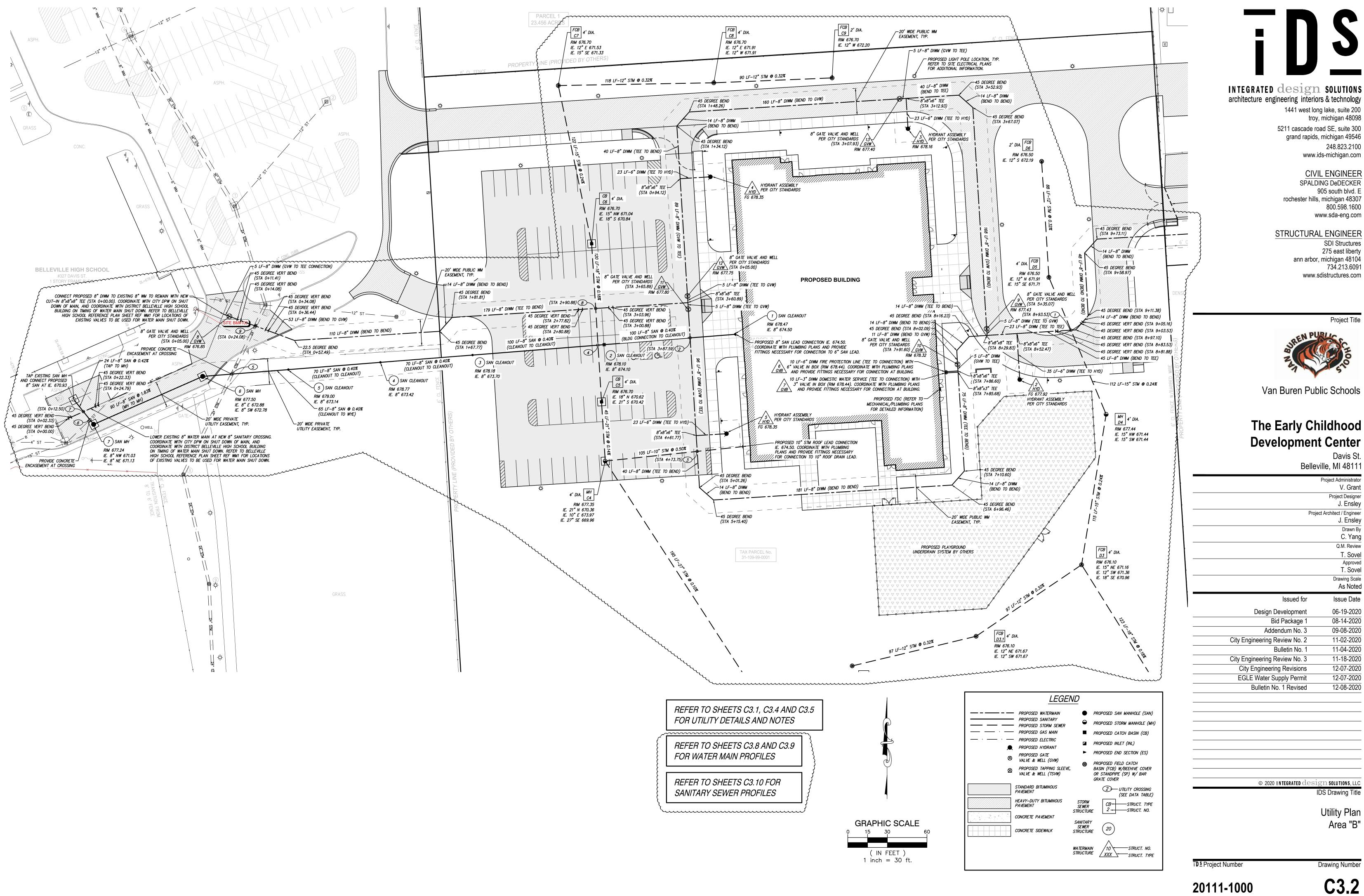
12-07-2020

12-08-2020

As Noted

Q.M. Review

Project Designer



CIVIL ENGINEER SPALDING DeDECKER

905 south blvd. E 800.598.1600 www.sda-eng.com

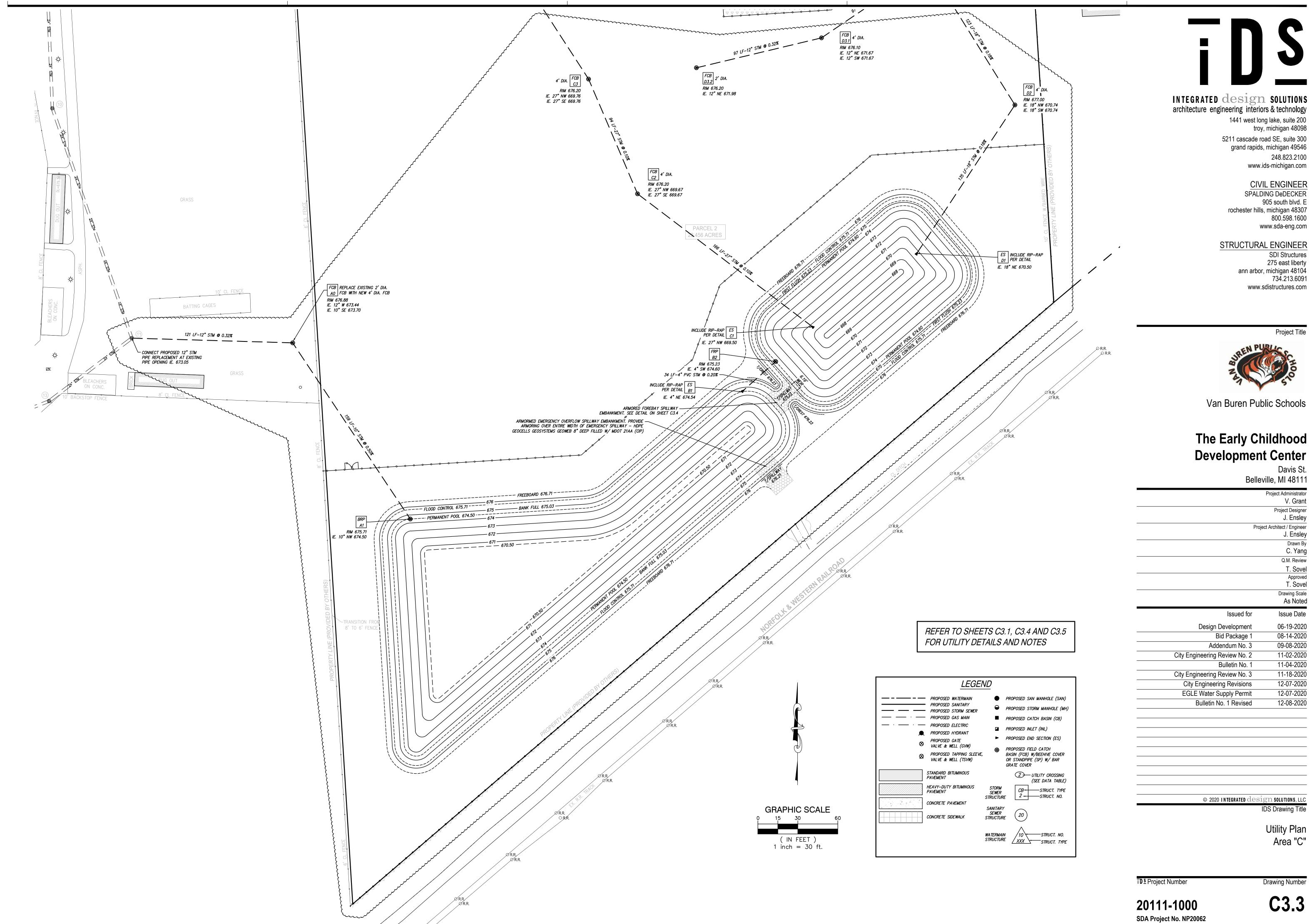
SDI Structures 275 east liberty ann arbor, michigan 48104 734.213.6091



	V. Grant
	Project Designer
	J. Ensley
	Project Architect / Engineer
	J. Ensley
	Drawn By
	C. Yang
	Q.M. Review
	T. Sovel
	Approved T. Sovel
	Drawing Scale
	As Noted
	713 110100
Issued for	Issue Date
Issued for Design Development	Issue Date 06-19-2020
Design Development	06-19-2020
Design Development Bid Package 1	06-19-2020 08-14-2020
Design Development Bid Package 1 Addendum No. 3	06-19-2020 08-14-2020 09-08-2020
Design Development Bid Package 1 Addendum No. 3 City Engineering Review No. 2	06-19-2020 08-14-2020 09-08-2020 11-02-2020
Design Development Bid Package 1 Addendum No. 3 City Engineering Review No. 2 Bulletin No. 1	06-19-2020 08-14-2020 09-08-2020 11-02-2020 11-04-2020
Design Development Bid Package 1 Addendum No. 3 City Engineering Review No. 2 Bulletin No. 1 City Engineering Review No. 3	06-19-2020 08-14-2020 09-08-2020 11-02-2020 11-04-2020 11-18-2020
Design Development Bid Package 1 Addendum No. 3 City Engineering Review No. 2 Bulletin No. 1 City Engineering Review No. 3 City Engineering Revisions	06-19-2020 08-14-2020 09-08-2020 11-02-2020 11-04-2020 11-18-2020 12-07-2020

Utility Plan

SDA Project No. NP20062



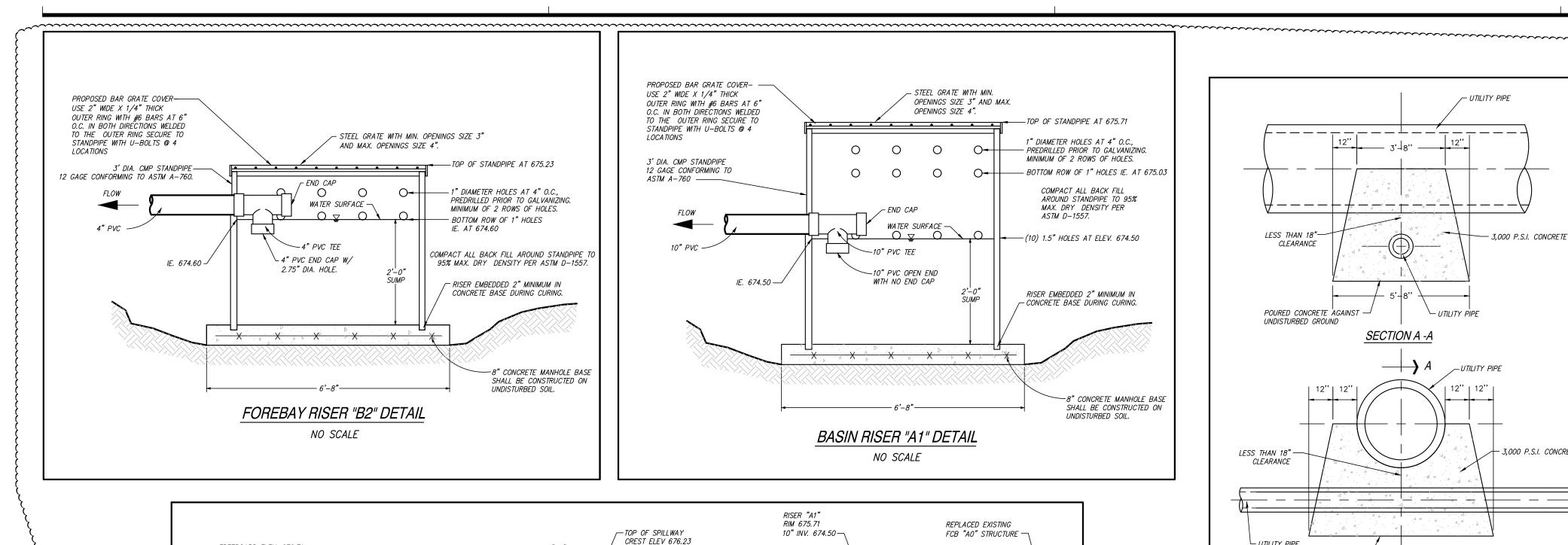
www.ids-michigan.com

905 south blvd. E www.sda-eng.com



Development Center

	Project Administrator
	V. Grant
	Project Designer
	J. Ensley
Pro	ject Architect / Engineer
	J. Ensley
	Drawn By
	C. Yang
	Q.M. Review
	T. Sovel Approved
	T. Sovel
	Drawing Scale
	As Noted
Issued for	Issue Date
Design Development	06-19-2020
Bid Package 1	08-14-2020
Addendum No. 3	09-08-2020
City Engineering Review No. 2	11-02-2020
Bulletin No. 1	11-04-2020
City Engineering Review No. 3	11-18-2020
City Engineering Revisions	12-07-2020
EGLE Water Supply Permit	12-07-2020
Bulletin No. 1 Revised	12-08-2020



– RISER "B2" RIM 675.23

2' SUMP

RISER OUTLET PIPE

INV. 674.60

H.W.L. 675.71

STORMWATER INLET ES "C1"

OUTLET END SECTION INLET END SECTION E TO BE THE SAME AS EINFORCED CONCRETE STIGNATION C 76.

T DIAMETER T

INLET IE. 669.50 -

RIP-RAP -

PERMANENT POOL-

FIRST FLUSH 675.23

MDOT 6A STONE

4" WASHED STONE—

NO SCALE

ELEV=675.23

6.19' WEIR

FOREBAY SPILLWAY CROSS SECTION

NO SCALE

T DIAMETER T

PRECAST CONCRETE END SECTION

DETENTION BASIN & FOREBAY SECTION

/— RIP-RAP

-COMPACTED EARTH

FOREBAY OVERFLOW

SPILLWAY @ 675.23

INV. 674.54 -

4' PERMANENT POOL-

ELEV 674.60

RIP-RAP (TYP.)_/

H.W.L. 675.71

MDOT 6A STONE -

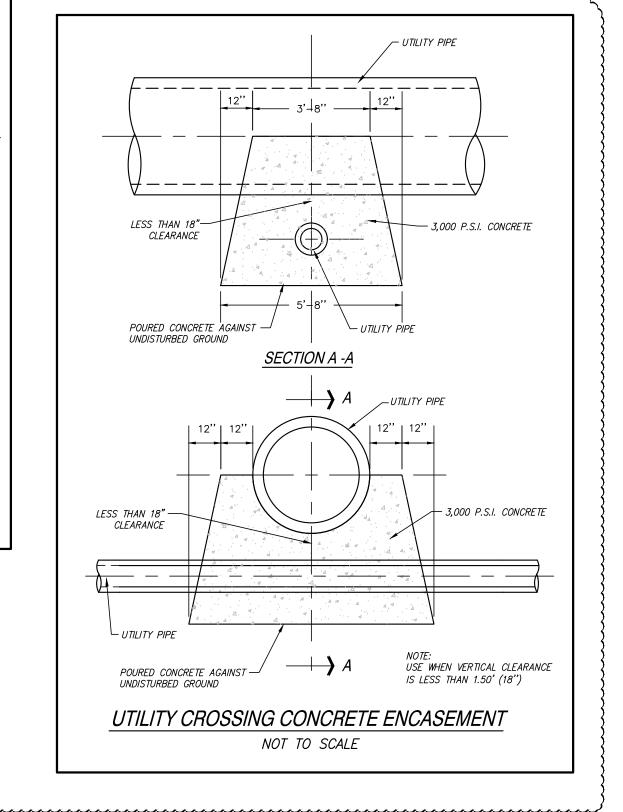
4" WASHED STONE-

OVERFLOW SPILLWAY

8" DEEP FILLED W/

OF EMERGENCY SPILLWAY HDPE GEOCELLS GEOSYSTEMS GEOWEB

SEE RISER DETAIL— FOR HOLES TO BE PLACED IN RISER



-COBBLESTONE RIP-RAP (6" TO 8" DIA.)



INTEGRATED design solutions architecture engineering interiors & technology

1441 west long lake, suite 200

troy, michigan 48098 5211 cascade road SE, suite 300 grand rapids, michigan 49546 248.823.2100 www.ids-michigan.com

CIVIL ENGINEER

SPALDING DeDECKER 905 south blvd. E rochester hills, michigan 48307 800.598.1600 www.sda-eng.com

STRUCTURAL ENGINEER

SDI Structures 275 east liberty ann arbor, michigan 48104 734.213.6091

www.sdistructures.com



Van Buren Public Schools

The Early Childhood **Development Center**

Belleville, MI 48111

Project Administrator

V. Grant

Froject Design	
J. Ensle	
Project Architect / Engine	F
J. Ensle	
Drawn I	
C. Yar	
Q.M. Revie	
T. Sov	
Approv	
T. Sov	
Drawing Sca	
As Note	
Issue Dat	Issued for
06-19-202	Design Development
08-14-202	Bid Package 1
09-08-202	Addendum No. 3
11 02 202	City Engineering Deview No. 2

	Drawing Sc As Not
Issued for	Issue Da
Design Development	06-19-20
Bid Package 1	08-14-202
Addendum No. 3	09-08-202
City Engineering Review No. 2	11-02-20
Bulletin No. 1	11-04-20
City Engineering Review No. 3	11-18-20
City Engineering Revisions	12-07-202
EGLE Water Supply Permit	12-07-202
Bulletin No. 1 Revised	12-08-20

© 2020 INTEGRATED design solutions, LLC **IDS Drawing Title**

Utility Details and Notes

C3.4

Drawing Number

20111-1000 SDA Project No. NP20062

SEWER PIPE SIZE Ø (I.D.) BOTTOM DIA (IF NOT ON PLANS)

36" OR LESS 48"

42" 60" 48" & 54" 72" BOTTOM DIAMETER CONCRETE PRECAST OR POURED CONC.

BASE - 2500 PSI AT 28 DAYS ID PROJECT Number (IF PRECAST IS USED PLACE 2" MIN. SAND SUB-BASE)

STORM SEWER MANHOLE

NO SCALE

(DIAMETER PER PLANS)

E.J.I.W. *1570 CASTING

PLUG (WHERE

SANITARY SEWER 6" CLEANOUT DETAIL

NO SCALE

REQUIRED)

REFER TO UTILITY PLAN FOR SIZE AND TYPE OF SEWER PIPE AND FITTINGS TO BE USED.

FRAME AND COVER

(SEE NOTES)

24" DIA.

— #4 BARS AT 12" O.C.

EACH WAY

2' DIAMETER STORM CATCH BASIN DETAIL

NO SCALE

W/SOLID COVER

TWO COURSE OF BRICK

UNDER CASTING

- FINISHED ASPHALT GRADE

- SEWER CLEANOUT PIPE

(LENGTH TO BE DETERMINED

AT TIME OF CONSTRUCTION)

— PLACE FRAME IN FULL

BED OF MORTAR

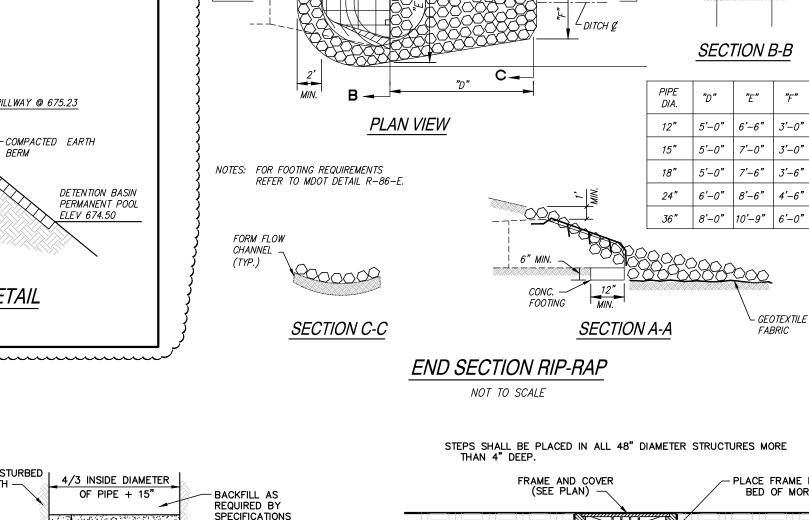
— PRECAST OR POURED CONC. BASE – 2500 PSI AT 28 DAYS

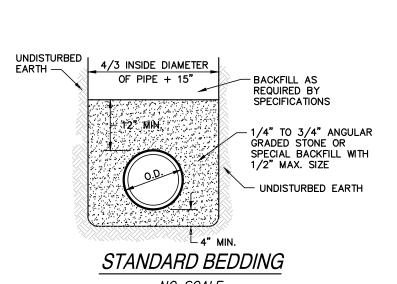
(IF PRECAST IS USED PLACE 2" MIN. SAND SUB-BASE)

— PLACE FRAME IN FULL BED OF MORTAR

BRICK, CONCRETE BLOCK OR PRECAST

-WROUGHT IRON OR ALUMINUM STEP, 16" OC BOTTOM STEP MAX 24"





INV. 673.70-

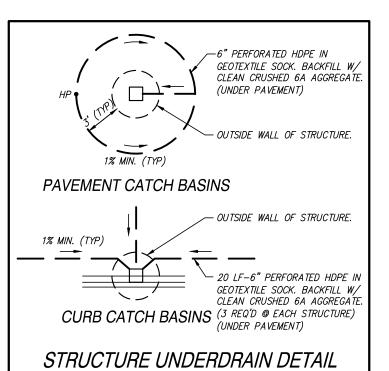
159 LF-10" — PVC @ 0.50%

CREST @ 676.23

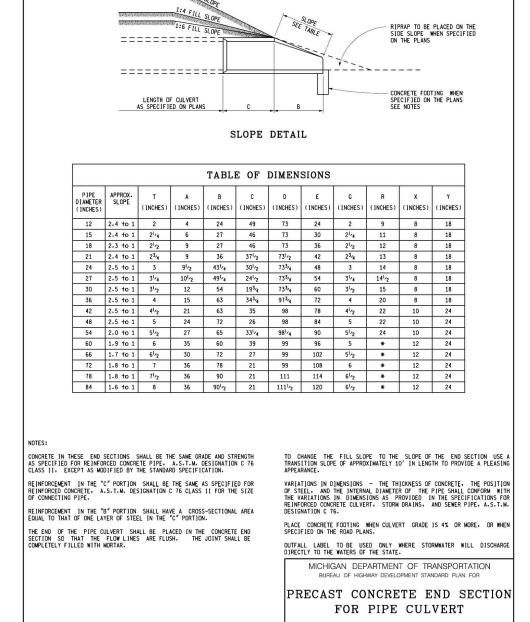
FOREBAY SPILLWAY ARMORING DETAIL

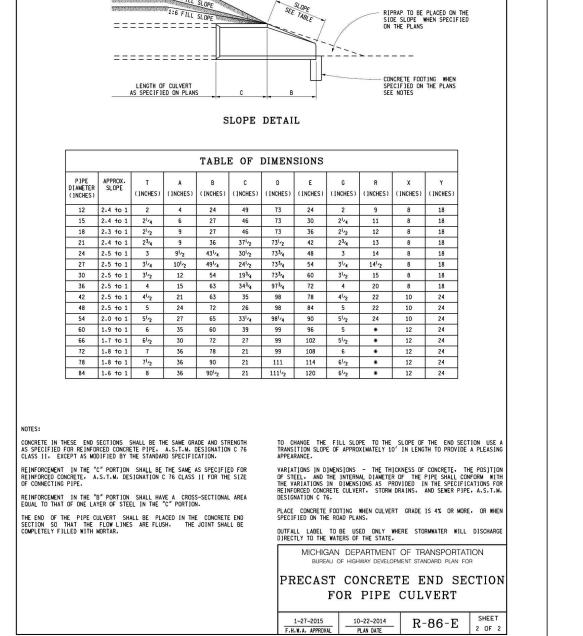
NO SCALE

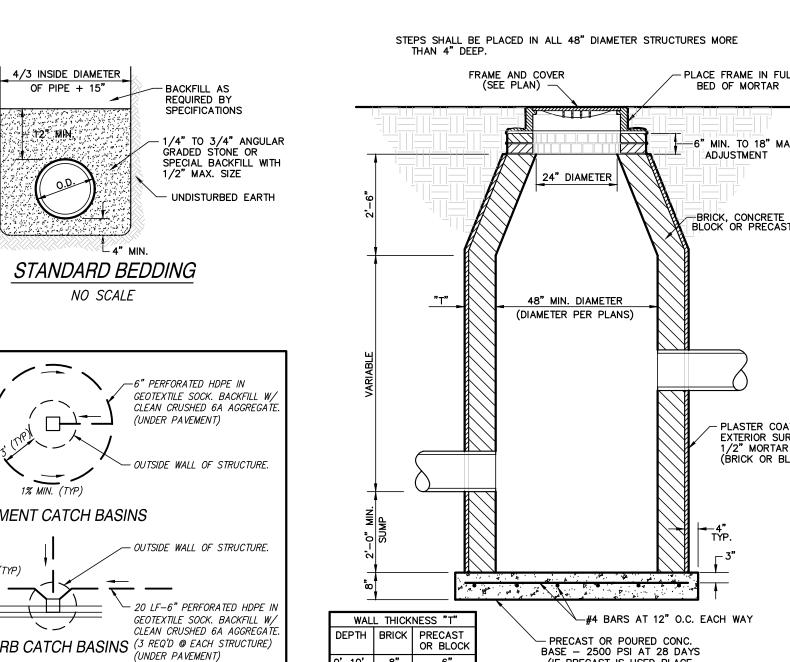
OVERFLOW SPILLWAY @ 675.23

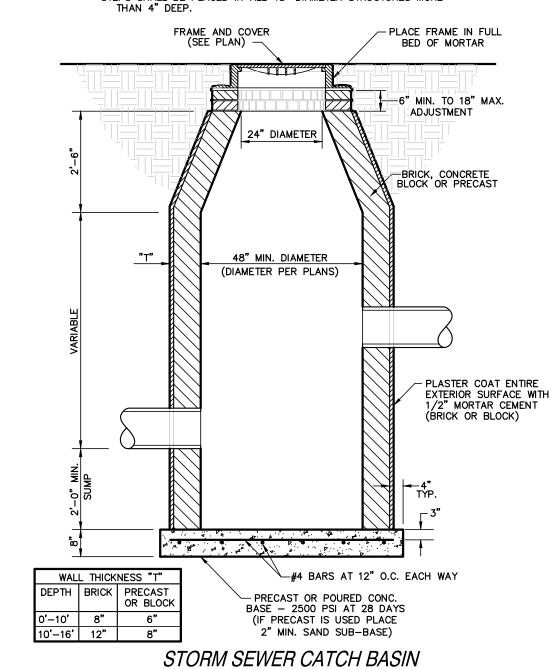


NO SCALE

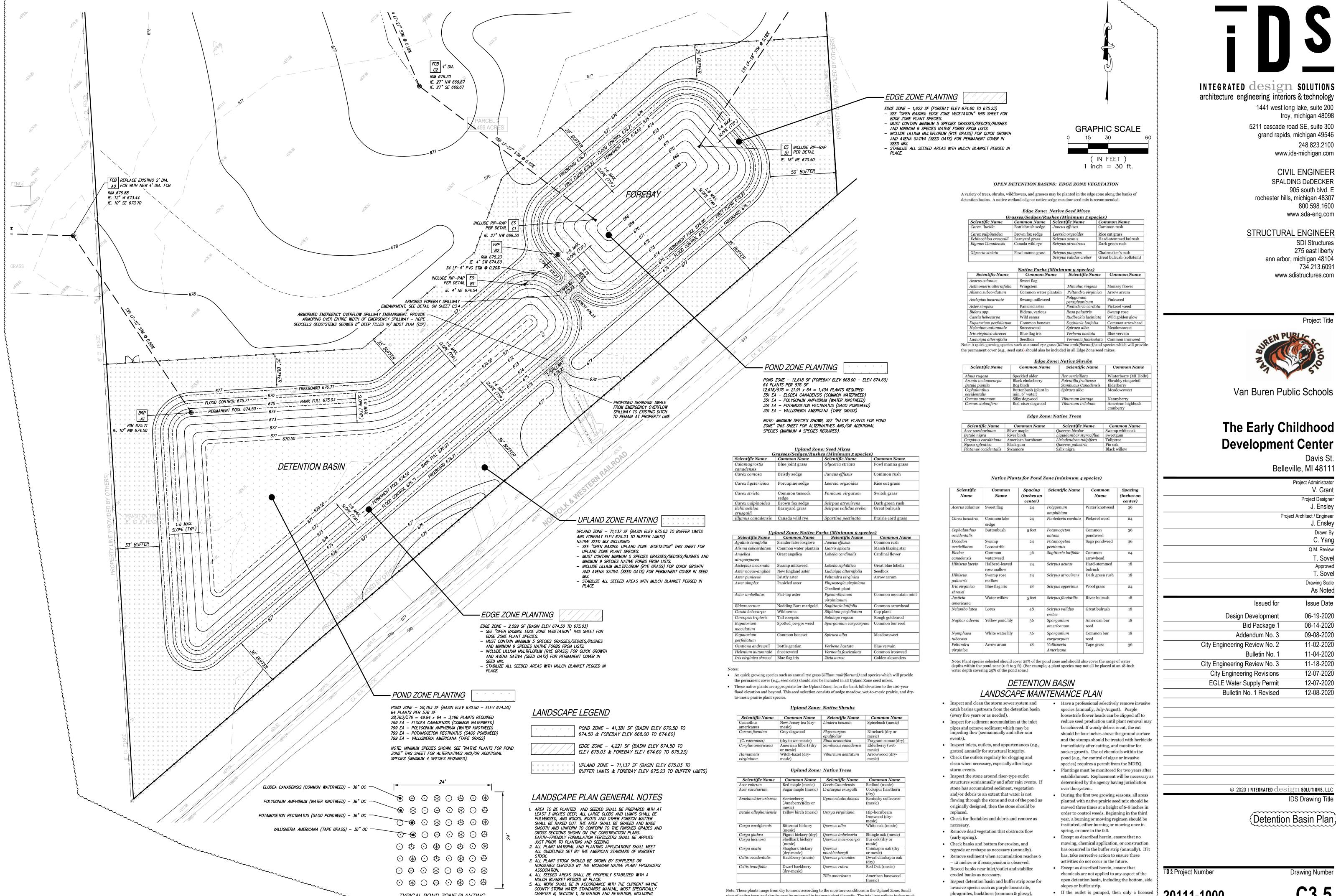








NO SCALE



sizes of native trees and shrubs may be proposed to increase plant diversity. The total tree caliper inches must

equal the calculated caliper inches of required trees.

TYPICAL POND ZONE PLANTING

905 south blvd. E 800.598.1600 www.sda-eng.com

SDI Structures 275 east liberty ann arbor, michigan 48104 734.213.6091



The Early Childhood

Belle	eville, MI 48111
	Project Administrator
	V. Grant
	Project Designer
	J. Ensley
Pro	ject Architect / Engineer
	J. Ensley
	Drawn By
	C. Yang
	Q.M. Review
	T. Sovel
	Approved T. Sovel
	Drawing Scale
	As Noted
	713 140100
Issued for	Issue Date
Design Development	06-19-2020
Bid Package 1	08-14-2020
Addendum No. 3	09-08-2020
City Engineering Review No. 2	11-02-2020
Bulletin No. 1	11-04-2020
City Engineering Review No. 3	11-18-2020
City Engineering Revisions	12-07-2020
FGLE Water Supply Permit	12-07-2020

Detention Basin Plan

electrician or company that provided the pump

SDA Project No. NP20062

system should conduct maintenance.

honeysuckle and autumn olive that out-compete

native vegetation (annually - July).



INTEGRATED design SOLUTIONS architecture engineering interiors & technology

1441 west long lake, suite 200 troy, michigan 48098
5211 cascade road SE, suite 300 grand rapids, michigan 49546
248.823.2100
www.ids-michigan.com

CIVIL ENGINEER
SPALDING DeDECKER
905 south blvd. E

905 south blvd. E rochester hills, michigan 48307 800.598.1600 www.sda-eng.com

STRUCTURAL ENGINEER

SDI Structures
275 east liberty
ann arbor, michigan 48104
734.213.6091
www.sdistructures.com

D : (T::



Van Buren Public Schools

The Early Childhood Development Center

Davis St. Belleville, MI 48111

Project Administrator

V. Grant

	-,
	J. Ensley
	Project Architect / Engineer
	J. Ensley
	Drawn By
	C. Yang
	Q.M. Review
	T. Sovel
	Approved
	T. Sovel
	Drawing Scale
	As Noted
Issued fo	r Issue Date
Design Developmen	t 06-19-2020
Bid Package	08-14-2020
Addendum No. 3	09-08-2020
City Engineering Review No. 2	2 11-02-2020
Bulletin No. 1	11-04-2020
City Engineering Review No. 3	11-18-2020
City Engineering Revisions	12-07-2020
EGLE Water Supply Permi	12-07-2020
Bulletin No. 1 Revised	12-08-2020

© 2020 INTEGRATED design solutions, LLC IDS Drawing Title

(Storm Sewer Drainage Map)

ī**D** § Project Number

Drawing Number

20111-1000SDA Project No. NP20062

(C3.

A (Ac.) C A*C 0.71 0.95 0.67 1.91 0.95 1.81 1.17 1.00 1.17 1.00 0.1.17 1.19 4.86 Interpretable of the first flush of runoff from the site. **BFIRST FLUSH VOLUME & ORIFICE CALCULATIONS** forebay volume required to store the first flush of runoff from the site. **BFIRST FLUSH VOLUME & ORIFICE CALCULATIONS** forebay volume required to store the first flush of runoff from the site. **BFIRST FLUSH VOLUME & ORIFICE CALCULATIONS** forebay volume required to store the first flush of runoff from the site. **BFIRST FLUSH VOLUME & ORIFICE CALCULATIONS** forebay volume required to store the first flush of runoff from the site. **BFIRST FLUSH VOLUME & ORIFICE CALCULATIONS** forebay volume required to store the first flush of runoff from the site. **BFIRST FLUSH VOLUME & ORIFICE CALCULATIONS** forebay volume required to store the first flush storage volume. **BFIRST FLUSH VOLUME & ORIFICE CALCULATIONS** forebay is used to store the first flush of runoff from the site. **BFIRST FLUSH VOLUME & ORIFICE CALCULATIONS** forebay is used to store the first flush of runoff from the site. **BFIRST FLUSH VOLUME & ORIFICE CALCULATIONS** forebay is used to store the first flush of runoff from the site. **BFIRST FLUSH VOLUME & ORIFICE CALCULATIONS** forebay is used to store the first flush of runoff from the site. **BFIRST FLUSH VOLUME & ORIFICE CALCULATIONS** forebay is used to store the first flush of runoff from the site. **BFIRST FLUSH VOLUME & ORIFICE CALCULATIONS** forebay is used to store the first flush of runoff from the site. **BFIRST FLUSH VOLUME & ORIFICE CALCULATIONS** forebay is used to store the first flush of runoff from the site. **BFIRST FLUSH VOLUME & ORIFICE CALCULATIONS** forebay is a reasonable approximation to the average head as follows:	Top of riser/ overflow structure to be set at the flood control storage elevation. 2100 = Riser outlet pipe will have an upstream invert elevation at: Riser Orifice Sizing To gradually release the bank full flood storage volume over a period of 40 hours, the average release rate for the full 40 hour period is calculated as follows: QaveBF = VtBF / 144,000 = 24943 / 144,000 = 0.17 CFS However, since almost all of the forebay storage volume will be released at an average of 0.102 CFS during last 27.1 of the 40 hours, the remainder of the bank full flood storage volume must be released at a rate in excess of 0.17 CFS during the first 12.9 of the 40 hours. The desired average release rate for the remaind of the bank full flood volume is: CaveBF = (VtBF - VtFF) / [40 - Tff) x 3600] = (24943 - 8774) / [40 - 27.1) x 3,600 = CAVEBF = (VtBF - VtFF) / [40 - Tff) x 3600] = (24943 - 8774) / [40 - 27.1) x 3,600 = CAVEBF = (VtBF - VtFF) / [40 - Tff) x 3600] = (24943 - 8774) / [40 - 27.1) x 3,600 = A number holes will be drilled in the riser at elevation 674.5. The number and size of holes will be selected to convey the average release rate for the remainder of the bank full flood given the average head on the orifice as follows: A number holes will be drilled average release rate for the remainder of the bank full flood given the average head on the orifice as follows: h_ave_us = 2/3 (2bf - Zout) = 2/3 (875.03 - 674.5) = 3.5 FT Ao = QaveBF / (0.62/2 g h_ave_us)^A.5) = 0.35 / (0.62/2 x 32.2 x 0.35)^A.5) = 1.5 inch = Therefore, Ao = 1.5 inch = 1.5
0.71 0.95 0.87 1.91 0.95 1.81 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.17 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	To gradually release the bank full flood storage volume over a period of 40 hours, the average release rate for the full 40 hour period is calculated as follows: OuveBF = VIBF / 144,000 = 24943 / 144,000 = 0.17
1.91	To gradually release the bank full flood storage volume over a period of 40 hours, the average release rate for the full 40 hour period is calculated as follows: OuveBF = VIBF / 144,000 = 24943 / 144,000 = 0.17
oup A, <4%) s.00 0.15 11.79 4.86 m-off Coefficient, C: 0.41 8. FIRST FLUSH VOLUME & ORIFICE CALCULATIONS forebay volume required to store the first flush of runoif from the site. me to capture the first flush, VtFF: VtFF = 1815 x A x C = 1815 x 11.79 x 0.41 = 8774 CFT capacity calculations for incremental and cumulative storage volumes determining the total storage ed in the forebay and the water surface elevation corresponding to the first flush storage volume. elease the first flush storage volume over a period of 24 hours, the desired average release rate is: QaveFF = VtFF / 8400 = 8774 / 84400 = 0.102 GFS at pipe and orifice restrictor will be sized to convey the desired average release rate given ead in the forebay. Since the forebay has a trapezoidal cross section, 2/3 of the maximum rebay is a reasonable approximation to the average head as follows: h_ave = 2/3 (2f7 - Zout) tu = upstream crown elevation of riser outlet pipe (ft) assuming e outlet pipe is designed to flow full at 0.102 CFS. e equation to determine the required riser outlet pipe diameter which will yield the desired serate and holding time. assume 4 inches for calculating h_avg = 0.33 FT wided Cumulative Area Basin Volume Only Only (CFT) 12.619 13.699 5.264 5.264 16.556 15.128 20.391 n elevation from table, Zbottom: age elevation from table, Zbottom: age elevation from interpolation, Zff. Forestimater will be: Do = 2 (Aout/Pi)*0.5 = 2 (0.0458/Pi)*0.5 = 0.241 FT, or use 2.75 inches 2.75 inches 2.75 inches 3.50 calculation of h_ave is needed since the selected riser uals the evertical run of the outlet tee. No recalculation of h_ave is needed since the selected riser uals the assumed diameter used in accluating h_ave. Do = 2.75 inches 2.29 FT	However, since almost all of the forebay storage volume will be released at an average of 0.102 CFS during last 27.1 of the 40 hours, the remainder of the bank full flood storage volume must be released at a rate in excess of 0.17 CFS during the first 12.9 of the 40 hours. The desired average release rate for the remaind of the bank full flood volume is: QaveBF = (VtBF - VtFF) / [(40 - Tff) x 3600]
### SFIRST FLUSH VOLUME & ORIFICE CALCULATIONS In creating the first flush, ViFF: **VIFF = 1815 x A x C = 1815 x 11.79 x 0.41 = 8774 **OFT	last 27.1 of the 40 hours, the remainder of the bank full flood storage volume must be released at a rate in excess of 0.17 CFS during the first 12.9 of the 40 hours. The desired average release rate for the remaind of the bank full flood volume is: CaveBF = (VtBF - VtFF) / [(40 - 27.1) x 3,600]
The forebay volume required to store the first flush of runoff from the site. The first flush, VIFF: VtFF = 1815 x A x C = 1815 x 11.79 x 0.41 = 8774 CFT To capacity calculations for incremental and cumulative storage volumes determining the total storage and in the forebay and the water surface elevation corresponding to the first flush storage volume. The forebay and the water surface elevation corresponding to the first flush storage volume. The forebay and the water surface elevation corresponding to the first flush storage volume. The forebay and the water surface elevation corresponding to the first flush storage volume. The forebay and the water surface elevation corresponding to the first flush storage volume. The forebay is a reasonable approximation to the average head as follows: The forebay is a reasonable approximation to the average head as follows: The average head as follows: The average head as follows: The average release rate given ead in the forebay. Since the forebay has a trapezoidal cross section, 2/3 of the maximum rebay is a reasonable approximation to the average head as follows: The average release rate given ead in the forebay. Since the forebay has a trapezoidal cross section, 2/3 of the maximum rebay is a reasonable approximation to the average head as follows: The average release rate given ead in the forebay. Since the forebay has a trapezoidal cross section, 2/3 of the maximum rebay is a reasonable approximation to the average head as follows: The average release rate is: The average release	last 27.1 of the 40 hours, the remainder of the bank full flood storage volume must be released at a rate in excess of 0.17 CFS during the first 12.9 of the 40 hours. The desired average release rate for the remaind of the bank full flood volume is: CaveBF = (VtBF - VtFF) / [(40 - 27.1) x 3,600]
The forebay volume required to store the first flush of runoff from the site. The first flush, VIFF: VtFF = 1815 x A x C = 1815 x 11.79 x 0.41 = 8774 CFT To capacity calculations for incremental and cumulative storage volumes determining the total storage and in the forebay and the water surface elevation corresponding to the first flush storage volume. The forebay and the water surface elevation corresponding to the first flush storage volume. The forebay and the water surface elevation corresponding to the first flush storage volume. The forebay and the water surface elevation corresponding to the first flush storage volume. The forebay and the water surface elevation corresponding to the first flush storage volume. The forebay is a reasonable approximation to the average head as follows: The forebay is a reasonable approximation to the average head as follows: The average head as follows: The average head as follows: The average release rate given ead in the forebay. Since the forebay has a trapezoidal cross section, 2/3 of the maximum rebay is a reasonable approximation to the average head as follows: The average release rate given ead in the forebay. Since the forebay has a trapezoidal cross section, 2/3 of the maximum rebay is a reasonable approximation to the average head as follows: The average release rate given ead in the forebay. Since the forebay has a trapezoidal cross section, 2/3 of the maximum rebay is a reasonable approximation to the average head as follows: The average release rate is: The average release	of the bank full flood volume is: QaveBF = (VtBF - VtFF) / [(40 - Tff) x 3600] = (24943 - 8774) / [(40 - 27.1) x 3,600 = 0.35] A number holes will be drilled in the riser at elevation 674.5. The number and size of holes will be selected to convey the average release rate for the remainder of the bank full flood given the average he in the detention basin. Since the detention basin has a trapezoidal cross section, 2/3 of the maximum he on the orifice is a reasonable approximation for the average head on the orifice as follows: h_ave_us = 2/3 (Zbf - Zout) = 2/3 (675.03 - 674.5) = 0.35 f 7 Ao = QaveBF / (0.62(2 g h_ave_us)^0.5) = 0.35 / (0.62(2 x 32.2 x 0.35)^0.5) = 0.119 SF do = 1.5 inch = 0.125 FT Therefore, Ao = 0.0123 SFT The required number of 1.5 inch dia. holes is then 0.119 / 0.0123 = 9.7 holes Therefore, use 10 at elevation 674.5. The actual average release rate through the orifice is, Qave_bf: Qave_bf = 0.62 x Ao ((2 g h_ave_bf)^0.5) 0.62 x 10 x 0.0123((2 x 32.2 x 0.35)^0.5) = 0.362 CFS Actual holding time for the bank full flood excluding the forebay volume is, Tbf: Tff = (VtBF - VtFF) / (Qave_bf x 3600) = (24943 - 8774) / (0.362 x 3600) = 12.4 HRS Actual holding time for the bank full flood including the forebay volume is, T: T = Tff + Tbf = 27.1 + 12.4 = 39.5 HRS T < 40 HRS, OKI Check of Forebay Design Assumption In sizing the forebay outlet pipe and orifice restrictor it was assumed that the forebay riser outlet pipe was flowing full at the average release rate for the first flush storage volume. Therefore it is necessary to verify that the sizing of the bank full off on to conflict with this assumption. Therefore it is necessary to verify that the sizing of the bank full off to not conflict with this assumption. The nank full off must pass the actual average release rate for the forebay at a detention basin head that does not exceed the downstrean crown elevation of the forebay riser outlet pipe is 674.87 Use the orifice equation to determine the detention basin head for this condit
VtFF = 1815 x A x C = 1815 x 11.79 x 0.41 = 8774 CFT In capacity calculations for incremental and cumulative storage volumes determining the total storage and in the forebay and the water surface elevation corresponding to the first flush storage volume. elease the first flush storage volume over a period of 24 hours, the desired average release rate is: QaveFF = VtFF / 86400 = 8774 / 86400 = 0.102 CFS et pipe and orifice restrictor will be sized to convey the desired average release rate given leads in the forebay. Since the forebay has a trapezoidal cross section, 2/3 of the maximum rebay is a reasonable approximation to the average head as follows: h_ave = 2/3 (Zff - Zout) ut = upstream crown elevation of riser outlet pipe (ft) assuming e outlet pipe is designed to flow full at 0.102 CFS. et equation to determine the required riser outlet pipe diameter which will yield the desired are rate and holding time. assume 4 inches for calculating h_avg = 0.33 FT vided flood control storage volume required. Cumulative Area Basin Volume Only Only (CFT) 12,619 0 13,699 5,264 5,264 16,556 15,128 20,391 In elevation from table, Zbottom: 674.60 rage elevation from interpolation, Zff: 675.23 Tout = Zbottom + d_out = 674.6 + 0.33 = 674.93 FT e = 2/3 (Zff - Zout) = 2/3 (675.23 - 674.93) = 0.2 FT = QaveFF / (0.62(2 g H_ave)^0.5) = 0.102/(0.62(2 x 32.2 x 0.2)^0.5) = 0.0458 is it he minimum allowable riser outlet pipe size, a 2.75 inch diameter hole will be drilled in the evertical run of the outlet tee. No recalculation of h_ave is needed since the selected riser unals the assumed diameter used in calculating h_ave. Do = 2.75 inches = 0.229 FT	A number holes will be drilled in the riser at elevation 674.5. The number and size of holes will be selected to convey the average release rate for the remainder of the bank full flood given the average he in the detention basin has a trapezoidal cross section, 2/3 of the maximum he on the orifice is a reasonable approximation for the average head on the orifice as follows: h_ave_us = 2/3 (Zbr - Zout) = 2/3 (675.03 - 674.5) = 0.35 FT
VtFF = 1815 x A x C = 1815 x 11.79 x 0.41 = 8774 CFT In capacity calculations for incremental and cumulative storage volumes determining the total storage and in the forebay and the water surface elevation corresponding to the first flush storage volume. elease the first flush storage volume over a period of 24 hours, the desired average release rate is: QaveFF = VtFF / 86400 = 8774 / 86400 = 0.102 CFS et pipe and orifice restrictor will be sized to convey the desired average release rate given leads in the forebay. Since the forebay has a trapezoidal cross section, 2/3 of the maximum rebay is a reasonable approximation to the average head as follows: h_ave = 2/3 (Zff - Zout) ut = upstream crown elevation of riser outlet pipe (ft) assuming e outlet pipe is designed to flow full at 0.102 CFS. et equation to determine the required riser outlet pipe diameter which will yield the desired are rate and holding time. assume 4 inches for calculating h_avg = 0.33 FT vided flood control storage volume required. Cumulative Area Basin Volume Only Only (CFT) 12,619 0 13,699 5,264 5,264 16,556 15,128 20,391 In elevation from table, Zbottom: 674.60 rage elevation from interpolation, Zff: 675.23 Tout = Zbottom + d_out = 674.6 + 0.33 = 674.93 FT e = 2/3 (Zff - Zout) = 2/3 (675.23 - 674.93) = 0.2 FT = QaveFF / (0.62(2 g H_ave)^0.5) = 0.102/(0.62(2 x 32.2 x 0.2)^0.5) = 0.0458 is it he minimum allowable riser outlet pipe size, a 2.75 inch diameter hole will be drilled in the evertical run of the outlet tee. No recalculation of h_ave is needed since the selected riser unals the assumed diameter used in calculating h_ave. Do = 2.75 inches = 0.229 FT	A number holes will be drilled in the riser at elevation 674.5. The number and size of holes will be selected to convey the average release rate for the remainder of the bank full flood given the average in the detention basin. Since the detention basin has a trapezoidal cross section, 2/3 of the maximum he on the orifice is a reasonable approximation for the average head on the orifice as follows: h_ave_us = 2/3 (Zbf - Zout) = 2/3 (675.03 - 674.5) = 0.35 FT Ao = QaveBF / (0.62(2 g h_ave_us)^0.5) = 0.35 / (0.62(2 x 32.2 x 0.35)^0.5) = 0.119 SF do = 1.5 inch = 0.125 FT Therefore, Ao = 0.0123 SFT The required number of 1.5 inch dia. holes is then 0.119 / 0.0123 = 9.7 holes Therefore, use 10 at elevation 674.5. The actual average release rate through the orifice is, Qave_bf: Qave_bf = 0.62 x Ao ((2 g h_ave_bf^0.5)) 0.62 x 10 x 0.0123/(2 x 32.2 x 0.35)^0.5) = 0.362 CFS Actual holding time for the bank full flood excluding the forebay volume is, Tbf: Tbf = (V18F - V1FF) / (Qave_bf x 3600) = (24943 - 8774) / (0.362 x 3600) = 12.4 HRS Actual holding time for the bank full flood including the forebay volume is, T: T = Tff + Tbf = 27.1 + 12.4 = 39.5 HRS T < 40 HRS, OKI Check of Forebay Design Assumption In sizing the forebay outlet pipe and orifice restrictor it was assumed that the forebay riser outlet pipe was flowing full at the average release rate for the first flush storage volume. Therefore it is necessary to verify that the sizing of the bank full orifi do not conflict with this assumption. The bank full orifi must pass the actual average release rate for the first flush storage volume. Therefore it is necessary to verify that the sizing of the bank full orifi do not conflict with this assumption. The bank full orifi must pass the actual average release rate for the first flush storage volume. Therefore it is necessary to verify that the sizing of the bank full orifi do not conflict with this assumption. The bank full orifi must pass the actual average release rate for the first flush storage volume
ed in the forebay and the water surface elevation corresponding to the first flush storage volume. elease the first flush storage volume over a period of 24 hours, the desired average release rate is: QaveFF = VtFF / 86400 = 8774 / 86400 = 0.102 CFS at pipe and orifice restrictor will be sized to convey the desired average release rate given ead in the forebay. Since the forebay has a trapezoidal cross section, 2/3 of the maximum rebay is a reasonable approximation to the average head as follows: h_ave = 2/3 (Zff - Zout) but = upstream crown elevation of riser outlet pipe (ft) assuming e outlet pipe is designed to flow full at 0.102 CFS. elevation to determine the required riser outlet pipe diameter which will yield the desired ser ate and holding time. assume 4 inches for calculating h_avg = 0.33 FT wided Cumulative Complex Comple	be selected to convey the average release rate for the remainder of the bank full flood given the average he in the detention basin. Since the detention basin has a trapezoidal cross section, 2/3 of the maximum he on the orifice is a reasonable approximation for the average head on the orifice as follows: h_ave_us = 2/3 (Zbf - Zout) = 2/3 (675.03 - 674.5) = 0.35 FT
elease the first flush storage volume over a period of 24 hours, the desired average release rate is: QaveFF = VtFF / 86400 = 8774 / 86400 = 0.102 CFS et pipe and orifice restrictor will be sized to convey the desired average release rate given ead in the forebay. Since the forebay has a trapezoidal cross section, 2/3 of the maximum rebay is a reasonable approximation to the average head as follows: h_ave = 2/3 (Zff - Zout) but = upstream crown elevation of riser outlet pipe (ft) assuming et outlet pipe is designed to flow full at 0.102 CFS. et equation to determine the required riser outlet pipe diameter which will yield the desired ser rate and holding time. assume 4 inches for calculating h_avg = 0.33 FT wided flood control storage volume required. Cumulative Area Basin Volume Only Only (CFT) 12,619 0 0 13,699 5,264 5,264 16,556 15,128 20,391 nelevation from table, Zbottom: frage elevation from table, Zbottom: arge elevation from table, Zbottom: Frage elevation from interpolation, Zff: Cout = Zbottom + d_out = 674.6 + 0.33 = 674.93 FT et = 2/3 (Zff - Zout) = 2/3 (675.23 - 674.93) = 0.2 FT equivalent = Calculation for the couled tea. No recalculation of h_ave is needed since the selected riser unals the assumed diameter used in calculating h_ave. Do = 2.75 inches = 0.229 FT	on the orifice is a reasonable approximation for the average head on the orifice as follows: h_ave_us = 2/3 (Zbf - Zout) = 2/3 (675.03 - 674.5) = 0.35 FT Ao = QaveBF / (0.62/2 g h_ave_us)^0.5) = 0.35 / (0.62/2 x 32.2 x 0.35)^0.5) = 0.119 SF do = 1.5 inch = 0.125 FT Therefore, Ao = 0.0123 SFT The required number of 1.5 inch dia. holes is then 0.119 / 0.0123 = 9.7 holes Therefore, use 10 at elevation 674.5. The actual average release rate through the orifice is, Qave_bf: Qave_bf = 0.62 x Ao ((2 g h_ave_bf)^0.5) 0.62 x 10 x 0.0123((2 x 32.2 x 0.35)^0.5) 0.62 x 10 x 0.0123((2 x 32.2 x 0.35)^0.5) 0.62 x 10 x 0.0123((2 x 32.2 x 0.35)^0.5) Actual holding time for the bank full flood excluding the forebay volume is, Tbf: Tbf = (VtBF - VtFF) / (Qave_bf x 3600) 1
QaveFF = VtFF / 86400 = 8774 / 86400 = 0.102 CFS at pipe and orifice restrictor will be sized to convey the desired average release rate given ead in the forebay. Since the forebay has a trapezoidal cross section, 2/3 of the maximum rebay is a reasonable approximation to the average head as follows: h_ave = 2/3 (Zff - Zout) put = upstream crown elevation of riser outlet pipe (ft) assuming e outlet pipe is designed to flow full at 0.102 CFS. e equation to determine the required riser outlet pipe diameter which will yield the desired ser rate and holding time. assume 4 inches for calculating h_avg = 0.33 FT vided if lood control storage volume required. Cumulative Area Basin Volume Only Only (CFT) 12,619 0 0 13,699 5,264 5,264 16,556 15,128 20,391 nelevation from table, Zbottom: rage elevation from interpolation, Zff: 675.23 \ Zout = Zbottom + d_out = 674.6 + 0.33 = 674.93 FT = QaveFF / (0.62(2 g H_ave)^0.5) = 0.102/(0.62(2 x 32.2 x 0.2)^0.5) = 0.0458 orifice diameter will be: Do = 2 (Aout/Pi)^0.5 = 2 (0.0458/Pi)^0.5 = 0.241 FT, or 2.9 inches use 2.75 inches sis is the minimum allowable riser outlet pipe size, a 2.75 inch diameter hole will be drilled in the evertical run of the outlet tee. No recalculation of h_ave is needed since the selected riser usuals the assumed diameter used in calculating h_ave. Do = 2.75 inches 0.229 FT	h_ave_us = 2/3 (Zbf - Zout) = 2/3 (675.03 - 674.5) = 0.35 FT Ao = QaveBF / (0.62(2 g h_ave_us)^0.5) = 0.35 / (0.62(2 x 32.2 x 0.35)^0.5) = 0.119 SF do = 1.5 inch = 0.125 FT Therefore, Ao = 0.0123 SFT The required number of 1.5 inch dia. holes is then 0.119 / 0.0123 = 9.7 holes Therefore, use 10 at elevation 674.5. The actual average release rate through the orifice is, Qave_bf: Qave_bf = 0.62 x Ao ((2 g h_ave_bf)^0.5) 0.62 x 10 x 0.0123((2 x 32.2 x 0.35)^0.5) = 0.362 CFS Actual holding time for the bank full flood excluding the forebay volume is, Tbf: Tff = (VtBF - VtFF) / (Qave_bf x 3600) = (24943 - 8774) / (0.362 x 3600) = 12.4 HRS Actual holding time for the bank full flood including the forebay volume is, T: T = Tff + Tbf = 27.1 + 12.4 = 39.5 HRS Check of Forebay Design Assumption In sizing the forebay outlet pipe and orifice restrictor it was assumed that the forebay riser outlet pipe was flowing full at the average release rate for the first flush storage volume. Therefore it is necessary to verify that the sizing of the bank full orif do not conflict with this assumption. The bank full orif must pass the actual average release rate for the forebay at a detention basin head that does not exceed the downstrean crown elevation of the forebay riser outlet pipe. The downstream crown elevation of the forebay riser outlet pipe is 674.87 Use the orifice equation to determine the detention basin head for this condition. h = [Qave_ff /(0.62 x A)]^2 /(2 x g) h = [0.09 / (0.62 x 10 x 0.0123)]^2 /(2 x 32.2) h = 0.002 FT
et pipe and orifice restrictor will be sized to convey the desired average release rate given ead in the forebay. Since the forebay has a trapezoidal cross section, 2/3 of the maximum rebay is a reasonable approximation to the average head as follows: h_ave = 2/3 (Zff - Zout) but = upstream crown elevation of riser outlet pipe (ft) assuming et outlet pipe is designed to flow full at 0.102 CFS. et equation to determine the required riser outlet pipe diameter which will yield the desired serate and holding time. assume 4 inches for calculating h_avg = 0.33 FT vided flood control storage volume required. Cumulative Area Basin Volume Only Only (CFT) 12,619 13,699 5,264 5,264 16,556 15,128 20,391 In elevation from table, Zbottom: rage elevation from table, Zbottom: rage elevation from interpolation, Zff: 675,23 Zout = Zbottom + d_out = 674.6 + 0.33 = 674.93 FT = QaveFF / (0.62(2 g H_ave)^0.5) = 0.102/(0.62(2 x 32.2 x 0.2)^0.5) = 0.0458 orifice diameter will be: Do = 2 (Aout/Pl)^0.5 = 2 (0.0458/Pl)^0.5 = 0.241 FT, or 2.9 inches use 1.275 inches is is the minimum allowable riser outlet pipe size, a 2.75 inch diameter hole will be drilled in the evertical run of the outlet tee. No recalculation of h_ave. Do = 2.75 inches is use 1.229 FT	Ao = QaveBF / (0.62(2 g h_ave_us)^0.5) = 0.35 / (0.62(2 x 32.2 x 0.35)^0.5) = 0.119 SF do = 1.5 inch = 0.125 FT Therefore, Ao = 0.0123 SFT The required number of 1.5 inch dia. holes is then 0.119 / 0.0123 = 9.7 holes Therefore, use 10 at elevation 674.5. The actual average release rate through the orifice is, Qave_bf: Qave_bf = 0.62 x Ao ((2 g h_ave_bf)^0.5) 0.62 x 10 x 0.0123((2 x 32.2 x 0.35)^0.5) 0.62 x 10 x 0.0123((2 x 32.2 x 0.35)^0.5) 0.62 x 10 x 0.0123((2 x 32.2 x 0.35)^0.5) Actual holding time for the bank full flood excluding the forebay volume is, Tbf: Tbf = (VtBF - VtFF) / (Qave_bf x 3600) 1
ead in the forebay. Since the forebay has a trapezoidal cross section, 2/3 of the maximum rebay is a reasonable approximation to the average head as follows: h_ave = 2/3 (2ff - Zout) put = upstream crown elevation of riser outlet pipe (ft) assuming e outlet pipe is designed to flow full at 0.102 CFS. e equation to determine the required riser outlet pipe diameter which will yield the desired ser rate and holding time. assume 4 inches for calculating h_avg = 0.33 FT vided flood control storage volume required. Cumulative Area Basin Volume Only Only (CFT) 12,619 0 13,699 5,264 5,264 16,556 15,128 20,391 n elevation from table, Zbottom: rage elevation from interpolation, Zff: Cout = Zbottom + d_out = 674.6 + 0.33 = 674.93 FT = QaveFF / (0.62(2 g H_ave)^0.5) = 0.102/(0.62(2 x 32.2 x 0.2)^0.5) = 0.0458 orifice diameter will be: Do = 2 (Aout/Pi)^0.5 = 2 (0.0458/Pi)^0.5 = 0.241 FT, or 2.9 inches sis is the minimum allowable riser outlet pipe size, a 2.75 inch diameter hole will be drilled in the evertical run of the outlet tee. No recalculation of h_ave is needed since the selected riser usuals the assumed diameter used in calculating h_ave. Do = 2.75 inches = 0.229 FT	do = 1.5 inch = 0.125 FT Therefore, Ao = 0.0123 SFT The required number of 1.5 inch dia. holes is then 0.119 / 0.0123 = 9.7 holes Therefore, use 10 at elevation 674.5. The actual average release rate through the orifice is, Qave_bf: Qave_bf = 0.62 × Ao ((2 g h_ave_bf)*0.5) 0.62 × 10 × 0.0123(2 × 32.2 × 0.35)*0.5) = 0.362 CFS Actual holding time for the bank full flood excluding the forebay volume is, Tbf: Tbf = (VtBF - VtFF) / (Qave_bf × 3600) = (24943 - 8774) / (0.362 × 3600) = 12.4 HRS Actual holding time for the bank full flood including the forebay volume is, T: T = Tff + Tbf = 27.1 + 12.4 = 39.5 HRS T < 40 HRS, OKI Check of Forebay Design Assumption In sizing the forebay outlet pipe and orifice restrictor it was assumed that the forebay riser outlet pipe was flowing full at the average release rate for the first flush storage volume. Therefore it is necessary to verify that the sizing of the bank full orifi do not conflict with this assumption. The bank full orifi must pass the actual average release rate for the forebay at a detention basin head that does not exceed the downstrean crown elevation of the forebay riser outlet pipe. The downstream crown elevation of the forebay riser outlet pipe is 674.87 Use the orifice equation to determine the detention basin head for this condition. h = [Qave_ff /(0.62 × A)]^2 /(2 × g) h = [0.09 / (0.62 × 10 × 0.0123)]^2 /(2 × 32.2) h = 0.002 FT
rebay is a reasonable approximation to the average head as follows: h_ave = 2/3 (Zff - Zout) but = upstream crown elevation of riser outlet pipe (ft) assuming be outlet pipe is designed to flow full at 0.102 CFS. be equation to determine the required riser outlet pipe diameter which will yield the desired see rate and holding time. assume 4 inches for calculating h_avg = 0.33 FT wided b flood control storage volume required. Cumulative Area Basin Volume Only Only (CFT) 12,619 0 0 13,699 5,264 5,264 16,556 15,128 20,391 an elevation from table, Zbottom: rage elevation from interpolation, Zff: 675.23 Zout = Zbottom + d_out = 674.6 + 0.33 = 674.93 FT a equation from interpolation, Zff: 675.23 Zout = Zbottom + d_out = 674.6 + 0.33 = 674.93 FT a equation from table and the country of the coun	Therefore, Ao = 0.0123 SFT The required number of 1.5 inch dia. holes is then 0.119 / 0.0123 = 9.7 holes Therefore, use 10 at elevation 674.5. The actual average release rate through the orifice is, Qave_bf: Qave_bf = 0.62 x Ao ((2 g h_ave_bf)^0.5) 0.62 x 10 x 0.0123((2 x 32.2 x 0.35)^0.5) = 0.362 CFS Actual holding time for the bank full flood excluding the forebay volume is, Tbf: Tbf = (VtBF - VtFF) / (Qave_bf x 3600) = (24943 - 8774) / (0.362 x 3600) = 12.4 HRS Actual holding time for the bank full flood including the forebay volume is, T: T = Tff + Tbf = 27.1 + 12.4 = 39.5 HRS T < 40 HRS, OK! Check of Forebay Design Assumption In sizing the forebay outlet pipe and orifice restrictor it was assumed that the forebay riser outlet pipe was flowing full at the average release rate for the first flush storage volume. Therefore it is necessary to verify that the sizing of the bank full orifi do not conflict with this assumption. The bank full orifi must pass the actual average release rate for the forebay at a detention basin head that does not exceed the downstrean crown elevation of the forebay riser outlet pipe. The downstream crown elevation of the forebay riser outlet pipe is 674.87 Use the orifice equation to determine the detention basin head for this condition. h = [Qave_ff /(0.62 x A)]^2 /(2 x g) h = [0.09 / (0.62 x 10 x 0.0123)]^2 /(2 x 32.2) h = 0.02 FT
out = upstream crown elevation of riser outlet pipe (ft) assuming e outlet pipe is designed to flow full at 0.102 CFS. e equation to determine the required riser outlet pipe diameter which will yield the desired ser ate and holding time. assume 4 inches for calculating h_avg = 0.33 FT vided e flood control storage volume required. Cumulative	The required number of 1.5 inch dia. holes is then 0.119 / 0.0123 = 9.7 holes Therefore, use 10 at elevation 674.5. The actual average release rate through the orifice is, Qave_bf: Qave_bf = 0.62 x Ao ((2 g h_ave_bf)^0.5) 0.62 x 10 x 0.0123((2 x 32.2 x 0.35)^0.5) = 0.362 CFS Actual holding time for the bank full flood excluding the forebay volume is, Tbf: Tbf = (VtBF - VtFF) / (Qave_bf x 3600) = (24943 - 8774) / (0.362 x 3600) = 12.4 HRS Actual holding time for the bank full flood including the forebay volume is, T: T = Tff + Tbf = 27.1 + 12.4 = 39.5 HRS T < 40 HRS, OK! Check of Forebay Design Assumption In sizing the forebay outlet pipe and orifice restrictor it was assumed that the forebay riser outlet pipe was flowing full at the average release rate for the first flush storage volume. Therefore it is necessary to verify that the sizing of the bank full orifi do not conflict with this assumption. The bank full orifi must pass the actual average release rate for the forebay at a detention basin head that does not exceed the downstrean crown elevation of the forebay riser outlet pipe. The downstream crown elevation of the forebay riser outlet pipe is 674.87 Use the orifice equation to determine the detention basin head for this condition. h = [Qave_ff /(0.62 x A)]^2 /(2 x g) h = 0.02 FT
e outlet pipe is designed to flow full at 0.102 CFS. e equation to determine the required riser outlet pipe diameter which will yield the desired ser rate and holding time. assume 4 inches for calculating h_avg = 0.33 FT wided flood control storage volume required. Cumulative Area Basin Volume Only Only (CFT) 12,619 0 0 13,699 5,264 5,264 16,556 15,128 20,391 In elevation from table, Zbottom: rage elevation from interpolation, Zff: Caut = Zbottom + d_out = 674.6 + 0.33 = 674.93 FT E = 2/3 (Zff - Zout) = 2/3 (675.23 - 674.93) = 0.2 FT = QaveFF / (0.62(2 g H_ave)^0.5) = 0.102/(0.62(2 x 32.2 x 0.2)^0.5) = 0.0458 For inches is is the minimum allowable riser outlet pipe size, a 2.75 inch diameter hole will be drilled in the evertical run of the outlet tee. No recalculation of h_ave is needed since the selected riser uses the assumed diameter used in calculating h_ave. Do = 2.75 inches = 0.229 FT	Therefore, use 10 at elevation 674.5. The actual average release rate through the orifice is, Qave_bf: Qave_bf = 0.62 x Ao ((2 g h_ave_bf)^0.5) 0.62 x 10 x 0.0123((2 x 32.2 x 0.35)^0.5) = 0.362 CFS Actual holding time for the bank full flood excluding the forebay volume is, Tbf: Tbf = (VtBF - VtFF) / (Qave_bf x 3600) = (24943 - 8774) / (0.362 x 3600) = 12.4 HRS Actual holding time for the bank full flood including the forebay volume is, T: T = Tff + Tbf = 27.1 + 12.4 = 39.5 HRS T < 40 HRS, OKI Check of Forebay Design Assumption In sizing the forebay outlet pipe and orifice restrictor it was assumed that the forebay riser outlet pipe was flowing full at the average release rate for the first flush storage volume. Therefore it is necessary to verify that the sizing of the bank full orifi do not conflict with this assumption. The bank full orifi must pass the actual average release rate for the forebay at a detention basin head that does not exceed the downstrean crown elevation of the forebay riser outlet pipe. The downstream crown elevation of the forebay riser outlet pipe is 674.87 Use the orifice equation to determine the detention basin head for this condition. h = [Qave_ff /(0.62 x A)]^2 /(2 x g) h = [0.09 / (0.62 x 10 x 0.0123)]^2 /(2 x 32.2) h = 0.02 FT
see rate and holding time. assume 4 inches for calculating h_avg = 0.33 FT vided a flood control storage volume required. Cumulative Area Basin Volume Only Only (CFT) 12,619 0 13,699 5,264 5,264 16,556 15,128 20,391 In elevation from table, Zbottom: rage elevation from interpolation, Zff: Zout = Zbottom + d_out = 674.6 + 0.33 = 674.93 FT a = 2/3 (Zff - Zout) = 2/3 (675.23 - 674.93) = 0.2 FT = QaveFF / (0.62(2 g H_ave)^0.5) = 0.102/(0.62(2 x 32.2 x 0.2)^0.5) = 0.0458 orifice diameter will be: Do = 2 (Aout/Pi)^0.5 = 2 (0.0458/Pi)^0.5 = 0.241 FT, or 2.9 inches as is the minimum allowable riser outlet pipe size, a 2.75 inch diameter hole will be drilled in the evertical run of the outlet tee. No recalculation of h_ave is needed since the selected riser uses the assumed diameter used in calculating h_ave. Do = 2.75 inches = 0.229 FT	The actual average release rate through the orifice is, Qave_bf: Qave_bf = 0.62 x Ao ((2 g h_ave_bf)^0.5) 0.62 x 10 x 0.0123((2 x 32.2 x 0.35)^0.5) = 0.362 CFS Actual holding time for the bank full flood excluding the forebay volume is, Tbf: Tbf = (VtBF - VtFF) / (Qave_bf x 3600) = (24943 - 8774) / (0.362 x 3600) = 12.4 HRS Actual holding time for the bank full flood including the forebay volume is, T: T = Tff + Tbf = 27.1 + 12.4 = 39.5 HRS T < 40 HRS, OK! Check of Forebay Design Assumption In sizing the forebay outlet pipe and orifice restrictor it was assumed that the forebay riser outlet pipe was flowing full at the average release rate for the first flush storage volume. Therefore it is necessary to verify that the sizing of the bank full orifi do not conflict with this assumption. The bank full orifi must pass the actual average release rate for the forebay at a detention basin head that does not exceed the downstrean crown elevation of the forebay riser outlet pipe. The downstream crown elevation of the forebay riser outlet pipe is 674.87 Use the orifice equation to determine the detention basin head for this condition. h = [Qave_ff /(0.62 x A)]^2 /(2 x g) h = [0.09 / (0.62 x 10 x 0.0123)]^2 /(2 x 32.2) h = 0.02 FT
Area Basin Volume Only Only (CFT) Only Onl	Qave_bf = 0.62 x Ao ((2 g h_ave_bf)^0.5) 0.62 x 10 x 0.0123((2 x 32.2 x 0.35)^0.5) = 0.362 CFS Actual holding time for the bank full flood excluding the forebay volume is, Tbf: Tbf = (VtBF - VtFF) / (Qave_bf x 3600) = (24943 - 8774) / (0.362 x 3600) = 12.4 HRS Actual holding time for the bank full flood including the forebay volume is, T: T = Tff + Tbf = 27.1 + 12.4 = 39.5 HRS T < 40 HRS, OK! Check of Forebay Design Assumption In sizing the forebay outlet pipe and orifice restrictor it was assumed that the forebay riser outlet pipe was flowing full at the average release rate for the first flush storage volume. Therefore it is necessary to verify that the sizing of the bank full orifi do not conflict with this assumption. The bank full orifi must pass the actual average release rate for the forebay at a detention basin head that does not exceed the downstrean crown elevation of the forebay riser outlet pipe. The downstream crown elevation of the forebay riser outlet pipe is 674.87 Use the orifice equation to determine the detention basin head for this condition. h = [Qave_ff / (0.62 x A)]^2 / (2 x g) h = [0.09 / (0.62 x 10 x 0.0123)]^2 / (2 x 32.2) h = 0.02 FT
Cumulative Area Basin Volume Only Only (CFT) 12,619 0 13,699 5,264 5,264 16,556 15,128 20,391	Actual holding time for the bank full flood excluding the forebay volume is, Tbf: Tbf = (VtBF - VtFF) / (Qave_bf x 3600) = (24943 - 8774) / (0.362 x 3600) = 12.4 HRS Actual holding time for the bank full flood including the forebay volume is, T: T = Tff + Tbf = 27.1 + 12.4 = 39.5 HRS T < 40 HRS, OK! Check of Forebay Design Assumption In sizing the forebay outlet pipe and orifice restrictor it was assumed that the forebay riser outlet pipe was flowing full at the average release rate for the first flush storage volume. Therefore it is necessary to verify that the sizing of the bank full orifi do not conflict with this assumption. The bank full orifi must pass the actual average release rate for the forebay at a detention basin head that does not exceed the downstrean crown elevation of the forebay riser outlet pipe. The downstream crown elevation of the forebay riser outlet pipe is 674.87 Use the orifice equation to determine the detention basin head for this condition. h = [Qave_ff /(0.62 x A)]^2 /(2 x g) h = [0.09 / (0.62 x 10 x 0.0123)]^2 /(2 x 32.2) h = 0.02 FT
Cumulative	Actual holding time for the bank full flood excluding the forebay volume is, Tbf: Tbf = (VtBF - VtFF) / (Qave_bf x 3600)
Area Basin Volume Only Only (CFT) 12,619 13,699 13,699 5,264 5,264 16,556 15,128 20,391 In elevation from table, Zbottom: Irage elevation from interpolation, Zff: Zout = Zbottom + d_out = 674.6 + 0.33 = 674.93 FT Example = 2/3 (Zff - Zout) = 2/3 (675.23 - 674.93) = 0.2 FT = QaveFF / (0.62(2 g H_ave)^0.5) = 0.102/(0.62(2 x 32.2 x 0.2)^0.5) = 0.0458 For orifice diameter will be: Do = 2 (Aout/Pi)^0.5 = 2 (0.0458/Pi)^0.5 = 0.241 FT, or 2.9 inches is is the minimum allowable riser outlet pipe size, a 2.75 inch diameter hole will be drilled in the evertical run of the outlet tee. No recalculation of h_ave is needed since the selected riser unals the assumed diameter used in calculating h_ave. Do = 2.75 inches = 0.229 FT	Tbf = (VtBF - VtFF) / (Qave_bf x 3600) = (24943 - 8774) / (0.362 x 3600) = 12.4 HRS Actual holding time for the bank full flood including the forebay volume is, T: T = Tff + Tbf = 27.1 + 12.4 = 39.5 HRS T < 40 HRS, OK! Check of Forebay Design Assumption In sizing the forebay outlet pipe and orifice restrictor it was assumed that the forebay riser outlet pipe was flowing full at the average release rate for the first flush storage volume. Therefore it is necessary to verify that the sizing of the bank full orifi do not conflict with this assumption. The bank full orifi must pass the actual average release rate for the forebay at a detention basin head that does not exceed the downstrean crown elevation of the forebay riser outlet pipe. The downstream crown elevation of the forebay riser outlet pipe is 674.87 Use the orifice equation to determine the detention basin head for this condition. h = [Qave_ff /(0.62 x A)]^2 /(2 x g) h = [0.09 / (0.62 x 10 x 0.0123)]^2 /(2 x 32.2) h = 0.02 FT
Area Basin Volume Only Only (CFT) 12,619 13,699 13,699 5,264 5,264 16,556 15,128 20,391 In elevation from table, Zbottom: Irage elevation from interpolation, Zff: Zout = Zbottom + d_out = 674.6 + 0.33 = 674.93 FT Example = 2/3 (Zff - Zout) = 2/3 (675.23 - 674.93) = 0.2 FT = QaveFF / (0.62(2 g H_ave)^0.5) = 0.102/(0.62(2 x 32.2 x 0.2)^0.5) = 0.0458 For orifice diameter will be: Do = 2 (Aout/Pi)^0.5 = 2 (0.0458/Pi)^0.5 = 0.241 FT, or 2.9 inches is is the minimum allowable riser outlet pipe size, a 2.75 inch diameter hole will be drilled in the evertical run of the outlet tee. No recalculation of h_ave is needed since the selected riser unals the assumed diameter used in calculating h_ave. Do = 2.75 inches = 0.229 FT	Actual holding time for the bank full flood including the forebay volume is, T: T = Tff + Tbf = 27.1 + 12.4 = 39.5 HRS T < 40 HRS, OK! Check of Forebay Design Assumption In sizing the forebay outlet pipe and orifice restrictor it was assumed that the forebay riser outlet pipe was flowing full at the average release rate for the first flush storage volume. Therefore it is necessary to verify that the sizing of the bank full orifi do not conflict with this assumption. The bank full orifi must pass the actual average release rate for the forebay at a detention basin head that does not exceed the downstrean crown elevation of the forebay riser outlet pipe. The downstream crown elevation of the forebay riser outlet pipe is 674.87 Use the orifice equation to determine the detention basin head for this condition. h = [Qave_ff /(0.62 x A)]^2 /(2 x g) h = [0.09 / (0.62 x 10 x 0.0123)]^2 /(2 x 32.2) h = 0.02 FT
12,619 13,699 15,264 16,556 15,128 20,391 In elevation from table, Zbottom: In age elevation from interpolation, Zff: Zout = Zbottom + d_out = 674.6 + 0.33 = 674.93 FT Example = 2/3 (Zff - Zout) = 2/3 (675.23 - 674.93) = 0.2 FT = QaveFF / (0.62(2 g H_ave)^0.5) = 0.102/(0.62(2 x 32.2 x 0.2)^0.5) = 0.0458 For orifice diameter will be: Do = 2 (Aout/Pi)^0.5 = 2 (0.0458/Pi)^0.5 = 0.241 FT, or 2.9 inches is is the minimum allowable riser outlet pipe size, a 2.75 inch diameter hole will be drilled in the evertical run of the outlet tee. No recalculation of h_ave is needed since the selected riser uals the assumed diameter used in calculating h_ave. Do = 2.75 inches = 0.229 FT	T = Tff + Tbf
13,699 16,556 15,128 20,391 In elevation from table, Zbottom: In elevation from table, Zbottom: In elevation from interpolation, Zff: Zout = Zbottom + d_out = 674.6 + 0.33 = 674.93 FT Exercise = 2/3 (Zff - Zout) = 2/3 (675.23 - 674.93) = 0.2 FT = QaveFF / (0.62(2 g H_ave)^0.5) = 0.102/(0.62(2 x 32.2 x 0.2)^0.5) = 0.0458 Exercise diameter will be: Do = 2 (Aout/Pi)^0.5 = 2 (0.0458/Pi)^0.5 = 0.241 FT, or 2.9 inches is is the minimum allowable riser outlet pipe size, a 2.75 inch diameter hole will be drilled in the evertical run of the outlet tee. No recalculation of h_ave is needed since the selected riser unals the assumed diameter used in calculating h_ave. Do = 2.75 inches = 0.229 FT	Check of Forebay Design Assumption In sizing the forebay outlet pipe and orifice restrictor it was assumed that the forebay riser outlet pipe was flowing full at the average release rate for the first flush storage volume. Therefore it is necessary to verify that the sizing of the bank full orifi do not conflict with this assumption. The bank full orifi must pass the actual average release rate for the forebay at a detention basin head that does not exceed the downstrean crown elevation of the forebay riser outlet pipe. The downstream crown elevation of the forebay riser outlet pipe is 674.87 Use the orifice equation to determine the detention basin head for this condition. h = [Qave_ff /(0.62 x A)]^2 /(2 x g) h = [0.09 / (0.62 x 10 x 0.0123)]^2 /(2 x 32.2) h = 0.02 FT
16,556 15,128 20,391 n elevation from table, Zbottom: rage elevation from interpolation, Zff: 2out = Zbottom + d_out = 674.6 + 0.33 = 674.93 FT 2 = 2/3 (Zff - Zout) = 2/3 (675.23 - 674.93) = 0.2 FT = QaveFF / (0.62(2 g H_ave)^0.5) = 0.102/(0.62(2 x 32.2 x 0.2)^0.5) = 0.0458 2 orifice diameter will be: Do = 2 (Aout/Pi)^0.5 = 2 (0.0458/Pi)^0.5 = 0.241 FT, or 2.9 inches as is the minimum allowable riser outlet pipe size, a 2.75 inch diameter hole will be drilled in the evertical run of the outlet tee. No recalculation of h_ave is needed since the selected riser uses the assumed diameter used in calculating h_ave. Do = 2.75 inches = 0.229 FT	Check of Forebay Design Assumption In sizing the forebay outlet pipe and orifice restrictor it was assumed that the forebay riser outlet pipe was flowing full at the average release rate for the first flush storage volume. Therefore it is necessary to verify that the sizing of the bank full orifi do not conflict with this assumption. The bank full orifi must pass the actual average release rate for the forebay at a detention basin head that does not exceed the downstrean crown elevation of the forebay riser outlet pipe. The downstream crown elevation of the forebay riser outlet pipe is 674.87 Use the orifice equation to determine the detention basin head for this condition. h = [Qave_ff /(0.62 x A)]^2 /(2 x g) h = [0.09 / (0.62 x 10 x 0.0123)]^2 /(2 x 32.2) h = 0.02 FT
zout = Zbottom + d_out = 674.6 + 0.33 = 674.93 FT = 2/3 (Zff - Zout) = 2/3 (675.23 - 674.93) = 0.2 FT = QaveFF / (0.62(2 g H_ave)^0.5) = 0.102/(0.62(2 x 32.2 x 0.2)^0.5) = 0.0458 = orifice diameter will be: Do = 2 (Aout/Pi)^0.5 = 2 (0.0458/Pi)^0.5 = 0.241 FT, or 2.9 inches use 2.75 inches is is the minimum allowable riser outlet pipe size, a 2.75 inch diameter hole will be drilled in the evertical run of the outlet tee. No recalculation of h_ave is needed since the selected riser uals the assumed diameter used in calculating h_ave. Do = 2.75 inches = 0.229 FT	In sizing the forebay outlet pipe and orifice restrictor it was assumed that the forebay riser outlet pipe was flowing full at the average release rate for the first flush storage volume. Therefore it is necessary to verify that the sizing of the bank full orifi do not conflict with this assumption. The bank full orifi must pass the actual average release rate for the forebay at a detention basin head that does not exceed the downstrean crown elevation of the forebay riser outlet pipe. The downstream crown elevation of the forebay riser outlet pipe is 674.87 Use the orifice equation to determine the detention basin head for this condition. h = [Qave_ff /(0.62 x A)]^2 /(2 x g) h = [0.09 / (0.62 x 10 x 0.0123)]^2 /(2 x 32.2) h = 0.02 FT
zout = Zbottom + d_out = 674.6 + 0.33 = 674.93 FT = 2/3 (Zff - Zout) = 2/3 (675.23 - 674.93) = 0.2 FT = QaveFF / (0.62(2 g H_ave)^0.5) = 0.102/(0.62(2 x 32.2 x 0.2)^0.5) = 0.0458 = orifice diameter will be: Do = 2 (Aout/Pi)^0.5 = 2 (0.0458/Pi)^0.5 = 0.241 FT, or 2.9 inches use 2.75 inches is is the minimum allowable riser outlet pipe size, a 2.75 inch diameter hole will be drilled in the evertical run of the outlet tee. No recalculation of h_ave is needed since the selected riser uals the assumed diameter used in calculating h_ave. Do = 2.75 inches = 0.229 FT	flowing full at the average release rate for the first flush storage volume. Therefore it is necessary to verify that the sizing of the bank full orifi do not conflict with this assumption. The bank full orifi must pass the actual average release rate for the forebay at a detention basin head that does not exceed the downstrean crown elevation of the forebay riser outlet pipe. The downstream crown elevation of the forebay riser outlet pipe is 674.87 Use the orifice equation to determine the detention basin head for this condition. h = [Qave_ff /(0.62 x A)]^2 /(2 x g) h = [0.09 / (0.62 x 10 x 0.0123)]^2 /(2 x 32.2) h = 0.02 FT
e = 2/3 (Zff - Zout) = 2/3 (675.23 - 674.93) = 0.2 FT = QaveFF / (0.62(2 g H_ave)^0.5) = 0.102/(0.62(2 x 32.2 x 0.2)^0.5) = 0.0458 orifice diameter will be: Do = 2 (Aout/Pi)^0.5 = 2 (0.0458/Pi)^0.5 = 0.241 FT, or 2.9 inches use 2.75 inches s is the minimum allowable riser outlet pipe size, a 2.75 inch diameter hole will be drilled in the e vertical run of the outlet tee. No recalculation of h_ave is needed since the selected riser uals the assumed diameter used in calculating h_ave. Do = 2.75 inches = 0.229 FT	actual average release rate for the forebay at a detention basin head that does not exceed the downstrean crown elevation of the forebay riser outlet pipe. The downstream crown elevation of the forebay riser outlet pipe is 674.87 Use the orifice equation to determine the detention basin head for this condition. h = [Qave_ff /(0.62 x A)]^2 /(2 x g) h = [0.09 / (0.62 x 10 x 0.0123)]^2 /(2 x 32.2) h = 0.02 FT
e = 2/3 (Zff - Zout) = 2/3 (675.23 - 674.93) = 0.2 FT = QaveFF / (0.62(2 g H_ave)^0.5) = 0.102/(0.62(2 x 32.2 x 0.2)^0.5) = 0.0458 orifice diameter will be: Do = 2 (Aout/Pi)^0.5 = 2 (0.0458/Pi)^0.5 = 0.241 FT, or 2.9 inches use 2.75 inches s is the minimum allowable riser outlet pipe size, a 2.75 inch diameter hole will be drilled in the e vertical run of the outlet tee. No recalculation of h_ave is needed since the selected riser uals the assumed diameter used in calculating h_ave. Do = 2.75 inches = 0.229 FT	The downstream crown elevation of the forebay riser outlet pipe is 674.87 Use the orifice equation to determine the detention basin head for this condition. h = [Qave_ff /(0.62 x A)]^2 /(2 x g) h = [0.09 / (0.62 x 10 x 0.0123)]^2 /(2 x 32.2) h = 0.02 FT
= QaveFF / (0.62(2 g H_ave)^0.5) = 0.102/(0.62(2 x 32.2 x 0.2)^0.5) = 0.0458 orifice diameter will be: Do = 2 (Aout/Pi)^0.5 = 2 (0.0458/Pi)^0.5 = 0.241 FT, or 2.9 inches use 2.75 inches s is the minimum allowable riser outlet pipe size, a 2.75 inch diameter hole will be drilled in the e vertical run of the outlet tee. No recalculation of h_ave is needed since the selected riser uals the assumed diameter used in calculating h_ave. Do = 2.75 inches = 0.229 FT	Use the orifice equation to determine the detention basin head for this condition. h = [Qave_ff /(0.62 x A)]^2 /(2 x g) h = [0.09 / (0.62 x 10 x 0.0123)]^2 /(2 x 32.2) h = 0.02 FT
orifice diameter will be: Do = 2 (Aout/Pi)^0.5 = 2 (0.0458/Pi)^0.5 = 0.241 FT, or 2.9 inches use 2.75 inches is is the minimum allowable riser outlet pipe size, a 2.75 inch diameter hole will be drilled in the e vertical run of the outlet tee. No recalculation of h_ave is needed since the selected riser uals the assumed diameter used in calculating h_ave. Do = 2.75 inches = 0.229 FT	h = [Qave_ff /(0.62 x A)]^2 /(2 x g) h = [0.09 / (0.62 x 10 x 0.0123)]^2 /(2 x 32.2) h = 0.02 FT
Do = 2 (Aout/Pi)^0.5 = 2 (0.0458/Pi)^0.5 = 0.241 FT, or use 2.75 inches s is the minimum allowable riser outlet pipe size, a 2.75 inch diameter hole will be drilled in the evertical run of the outlet tee. No recalculation of h_ave is needed since the selected riser uals the assumed diameter used in calculating h_ave. Do = 2.75 inches = 0.229 FT	h = [Qave_ff /(0.62 x A)]^2 /(2 x g) h = [0.09 / (0.62 x 10 x 0.0123)]^2 /(2 x 32.2) h = 0.02 FT
use 2.75 inches s is the minimum allowable riser outlet pipe size, a 2.75 inch diameter hole will be drilled in the e vertical run of the outlet tee. No recalculation of h_ave is needed since the selected riser uals the assumed diameter used in calculating h_ave. Do = 2.75 inches = 0.229 FT	h = [0.09 / (0.62 x 10 x 0.0123)]^2 /(2 x 32.2) h = 0.02 FT
s is the minimum allowable riser outlet pipe size, a 2.75 inch diameter hole will be drilled in the e vertical run of the outlet tee. No recalculation of h_ave is needed since the selected riser uals the assumed diameter used in calculating h_ave. Do = 2.75 inches = 0.229 FT	
uals the assumed diameter used in calculating h_ave. Do = 2.75 inches = 0.229 FT	Reced on the bank full crift as designed the water surface elevation in the detention basin is:
	674.52 < 674.87 therefore, OK.
David Alimbra 2000 FT	Riser Outlet Pipe and Orifice Restrictor Sizing The riser outlet pipe and orifice restrictor will be sized to convey the desired maximum allowable release
Dout = 4 inches = 0.333 FT	rate (for the 100 year flood) at the flood control storage elevation in the detention basin. A number of orifi
erage release rate through the orifice restrictor and outlet pipe is:	placed in the riser above the bank full flood elevation but will not serve as a restrictor for the maximum rele
Qave_ff = 0.62 (Ao) ((2 g h_ave)^0.5)	Qmax = Qa = 1.77 CFS (from storage volume calculations)
= 0.62(0.0412)((2x32.2x0.2)^0.5) = 0.090 CFS	h_max = Z100 - Zout
09 CFS < desired rate of 0.102 CFS, therefore OK.	where: Zout = upstream crown elevation of riser outlet pipe (ft) assuming the outlet pipe is designed to flow full at 1.77 CFS.
g time is:	
Tff = VtFF/Qff_actual = 8774 / 0.09 / 60 min / 60 sec = 27.1 HRS	Determine the riser outlet pipe diameter to achieve the maximum release rate. Assume an outlet pipe diameter of: 10 inches
Tff > 24 HRS, OK!	Then, d_out = 0.83 FT
Pipe Slope	Zout = 674.5 + 0.83 = 675.33 FT
er outlet pipe slope to be consistent with earlier assumption that it is flowing full at the actual se rate. Use Manning's equation with n = 0.012 for PVC pipe.	h_max = 675.71 - 675.33 = 0.38 FT
	Aout = Qmax / (0.62(2 g h_max)^0.5) = 1.77/(0.62(2 x 32.2 x 0.38)^0.5) = 0.577 SF
[(Qave_ff x n)/(1.486 x Aout x R^2/3)]^2	
R = Dout / 4 = 0.333 / 4 = 0.083 FT Slope (ft/ft) = [(0.09 x 0.012)/(1.486 x 0.0871 x 0.083^2/3)]^2	Therefore, the orifice diameter will be: Do = 2 (Aout/Pi)^0.5 = 2 (0.577/Pi)^0.5 = 0.86 FT, or 10 Inc
Slope = 0.0019 FT/FT	
= 0.2 % herefore, use a 4 inch PVC pipe at 0.2% slope.	Do = 10 inches = 0.833 FT Which has an orifice area of: Ao = 0.545 SFT
y at full flow condition against maximum allowable closed conduit velocity.	Dout = 10 inches = 0.833 FT
ve_ff / Aout = 0.09 / 0.0871 = 1.03 FPS	Which has an orifice area of: Aout = 0.545 SFT
03 < Vmax of 8 FPS therefore, OK.	The actual maximum release rate through the orifice restrictor and outlet pipe is:
DETENTION BASIN VOLUME CALCULATIONS	Qmax = 0.62 (Ao) ((2 g h_max)^0.5) = 0.62 (0.545) ((2 x 32.2 x 0.38)^0.5)
is larger than 5 acres, the maximum allowable outflow from this site is 0.15 cfs/acre for the m. The detention basin will be designed with a permanent pool, but we must verify that it is	= 1.67 CFS
vnstream invert of the forebay riser outlet pipe.	Qave_ff of 1.67 CFS < desired rate of 1.77 CFS, therefore OK.
Length of riser outlet pipe, per plan = 34 FT elevation of permanent pool, per plan = 674.50	Riser Outlet Pipe Slope Determine riser outlet pipe slope to be consistent with earlier assumption that it is flowing full at the actual
D.S. Invert = 674.6 - (0.0019 x 34) = 674.54	maximum release rate. Use Manning's equation with n = 0.012 for PVC pipe.
74.54 > 674.5 therefore, OK.	Slope (ft/ft) = [(Qmax x n)/(1.486 x Aout x R^2/3)]^2
lume	
e flood control storage volume required.	where, R = Dout / 4 = 0.833 / 4 = 0.208 FT So, Slope (ft/ft) = [(1.67 x 0.012)/(1.486 x 0.545 x 0.208^2/3)]^2
Discharge Rate per Acre, q: 0.15 CFS/Ac	Slope = 0.005 FT/FT = 0.5 %
owable release rate from the flood control storage volume, Qa:	Therefore, use a 10 inch PVC pipe at 0.5% slope.
Qa = q x A = 0.15 x 11.79 = 1.77 CFS	Check velocity at full pipe flow condition against minimum and maximum allowable closed conduit velocities
flow rate per acre imperviousness, Qo:	V = Qmax / Aout = 1.67 / 0.545 = 3.06 FPS 3.06 < Vmax of 8 FPS therefore, OK.
D = Qa / (A x C) = 1.77 / (11.79 x 0.41) = 0.37 CFS/acre*imperviousness	3.06 < Vmax of 8 FPS therefore, OK. 3.06 > Vmin of 2.5 FPS therefore, OK.
- the instant storage begins until peak storage is attained, T100:	
00 = -45 + sqrt(19,845 / Qo) = -45 + sqrt(19,845 / 0.37) = 186.59 minutes	Emergency Overflow Weir
ume of water stored in the detention basin per acre of imperviousness, Vs100:	
Vs100 = [(17,649 x T100) / (T100+45)] - 40 x Qo x T100 6.59) / (186.59 + 45) - 40 x 0.37 x 186.59 = 11458	Determine unrestricted flow over site from a 10-Year storm event using the rational method:
	Area of the site: 11.79 Acres
ume of water stored in the detention basin (required), Vt100: Vt100 = Vs10 x A x C = 11458 x 11.79 x 0.41 = 55387 CFT	Overall site C factor: 0.41 Time of concentration, t (from storm calcs): 20.19 minutes
nk full flood storage volume, Vtbf:	Assumed minimum initial time: 20.19 minutes minutes
tBF = 5160 x A x C = 5160 x 11.79 x 0.41 = 24,943 CFT	
vided	Rainfall Intensity, I=151.8/(t+15) = 4.31 in/hr
e flood control storage volume required.	Flow, Q10 = C A = 0.41 x 4.31 x 11.79 = 20.83 CFS
Incremental	Equation for transported Weig Designs
Area (SFT) Volumes (CFT) Forebay Forebay Cumulative	Equation for trapazoidal Weir Design:
(But only Volume	Q10 = 3.367 x b x h ² (3/2)
Basin above Basin above (CFT) Only elev. Zff) Only elev. Zff)	Solve above equation for the bottom width his
	Solve above equation for the bottom width, b:
28,763 0 0 31,467 0 15,058 15,058 15,058	b = Q10 / (3.367 x h^(3/2))
32,674 14,308 7,376 22,434	Accume don't of flow controls to the door of
37,044 16,556 26,841 11,883 61,158	Assume depth of flow over weir, h = 1.00 ft
	Therefore, minimum bottom width of Weir is:
the bank full flood to be captured in the detention basin is determined by subracting the age volume provided in the forebay.	b= 6.19 ft
VtBF(adj) = VtBF - VtFF = 24943 - 8774 = 16,169 CFT	
elevation from table, Zbottom: 674.50	
storage elevation from interpolation, Zbf. 675.03	مرمرمرم
the flood control storage volume to be captured in the detention basin is also determined by	صرمرم.

Flood control storage elevation from interpolation, Z100:

(Design Water Level for the Basin)

PROPOSED ECDC SITE - STORM SEWER DRAINAGE CALCULATIONS - BRANCH "C"

(REFER TO SHEET C3.6 FOR DRAINAGE MAP)

(User)		(User)	(User)	,	, ,	(Calc)	, ,	, ,	, ,	(Calc)	(User)	(Calc)	(Calc)	(User)	(Calc)	(Calc)	(Calc)	(User)	(Calc)	Jump	Invert	Invert	HG	HG						
MANHOLE		Area	Area	Accm	Imperv.	Equiv.	Accm.		(" ")	("Q")	D	Min HG	HG for	Pipe	Actual	"V" fps	Cap.	L	Time of	at	Elev. at	Elev. at	Elev. at	Elev. at						
		Name	Added	Area		Area	Equiv.		Inten.	Runoff	Diam.	based	2.5 fps	Slope	HG	Vel.@	Prov.	Pipe	Flow	MH (dn)	Up	Down	Up	Down	Up MH	Depth	DN MH	Depth	H.G. TO	H.G. TO
From	То		("A")		("C")	(AxC)	Area	("T")	ln./Hr	(CFS)	(in.)	on Q %	given D	(%)	(%)	HG	(CFS)	Length	(min)	?	MH	MH	MH	MH	Rim	RIM-T/P	Rim	RIM-T/P	RIM(Up)	RIM(Dn)
ROOF	MH C4	ROOF	0.71	0.71	0.95	0.67	0.67	15.00	4.35	2.93	10	1.79	0.42	0.50	1.79	5.38	2.93	105	0.33	2.88	674.50	673.97	676.84	674.96	678.50	3.17	677.35	2.55	1.66	2.39
		1																												
MAIN BRAN	CH																													
FCB C9	FCB C8	C9	0.27	0.27	0.50	0.14	0.14	15.00	4.35	0.59	12	0.03	0.32	0.32	0.32	2.57	2.02	90	0.58		672.20	671.91	676.20	675.91	676.70	3.50	676.70	3.79	0.50	0.79
FCB C8	FCB C7	C8	0.16	0.43	0.57	0.09	0.23	15.58	4.28	0.97	12	0.07	0.32	0.32	0.32	2.57	2.02	118	0.77		671.91	671.53	675.91	675.53	676.70	3.79	676.70	4.17	0.79	1.17
FCB C7	CB C6	C7	0.21	0.64	0.60	0.13	0.35	16.35	4.19	1.47	15	0.05	0.24	0.24	0.24	2.58	3.16	122	0.79		671.33	671.04	675.53	675.24	676.70	4.12	676.70	4.41	1.17	1.46
CB C6	CB C5	C6	0.80	1.44	0.75	0.60	0.95	17.14	4.10	3.90	18	0.14	0.18	0.18	0.18	2.52	4.46	120	0.79		670.84	670.62	675.24	675.02	676.70	4.36	676.70	4.58	1.46	1.68
CB C5	MH C4	C5	1.02	2.46	0.48	0.49	1.44	17.93	4.01	5.79	21	0.13	0.14	0.14	0.14	2.46	5.93	45	0.30		670.42	670.36	675.02	674.96	676.70	4.53	677.35	5.24	1.68	2.39
MH C4	FCB C3	- 7	0.00	3.17	0.00	0.00	2.12	18.24	3.98	8.42	27	0.07	0.10	0.10	0.10	2.46	9.79	195	1.32		669.96	669.76	674.96	674.76	677.35	5.14	676.20	4.19	2.39	1.44
FCB C3	FCB C2	C3	1.56	4.73	0.15	0.23	2.35	19.56	3.85	9.04	27	0.09	0.10	0.10	0.10	2.46	9.79	94	0.64		669.76	669.67	674.76	674.67	676.20	4.19	676.20	4.28	1.44	1.53
FCB C2	ES C1	C2	0.98	5.71	0.15	0.15	2.50	20.19	3.79	9.46	27	0.09	0.10	0.10	0.10	2.46	9.79	166	1.12		669.67	669.50	674.67	674.50	676.20	4.28	674.50	2.75	1.53	

PROPOSED ECDC SITE - STORM SEWER DRAINAGE CALCULATIONS - BRANCH "D"

(REFER TO SHEET C3.6 FOR DRAINAGE MAP)

(User)		(User)	(User)	(Calc)				(User)	(Calc)	(Calc)	(User)	(Calc)	, ,	(User)	(Calc)	(Calc)	(Calc)	(User)	(Calc)	Jump	Invert	Invert	HG	HG						
MANHOLE		Area	Area	Accm	Imperv.	Equiv.	Accm.		("I")	("Q")	D	Min HG	HG for	Pipe	Actual	"V" fps	Cap.	L	Time of	at	Elev. at	Elev. at	Elev. at	Elev. at						
		Name	Added	Area		Area	Equiv.		Inten.	Runoff	Diam.	based	2.5 fps	Slope	HG	Vel.@	Prov.	Pipe	Flow	MH (dn)	Up	Down	Up	Down	Up MH	Depth	DN MH	Depth	H.G. TO	H.G. TO
From	То		("A")		("C")	(AxC)	Area	("T")	In./Hr	(CFS)	(in.)	on Q %	given D	(%)	(%)	HG	(CFS)	Length	(min)	?	MH	MH	MH	MH	Rim	RIM-T/P	Rim	RIM-T/P	RIM(Up)	RIM(Dn)
FCB D3.2	FCB D3.1	D3.2	0.44	0.44	0.23	0.10	0.10	15.00	4.35	0.44	12	0.02	0.32	0.32	0.32	2.57	2.02	97	0.63		671.98	671.67	675.58	675.27	676.20	3.22	676.10	3.43	0.62	0.83
FCB D3.1	FCB D3	D3.1	0.45	0.89	0.18	0.08	0.18	15.63	4.27	0.78	12	0.05	0.32	0.32	0.32	2.57	2.02	97	0.63		671.67	671.36	675.27	674.96	676.10	3.43	676.10	3.74	0.83	1.14
MAIN BRAN	CH																													
FCB D6	FCB D5	D6	0.52	0.52	0.52	0.27	0.27	15.00	4.35	1.18	12	0.11	0.32	0.32	0.32	2.57	2.02	88	0.57		672.19	671.91	675.79	675.51	676.50	3.31	676.50	3.59	0.71	0.99
FCB D5	MH D4	D5	0.49	1.01	0.59	0.29	0.56	15.57	4.28	2.39	15	0.14	0.24	0.24	0.24	2.58	3.16	112	0.72		671.71	671.44	675.51	675.24	676.50	3.54	677.44	4.75	0.99	2.20
MH D4	FCB D3	-	0.00	1.01	0.00	0.00	0.56	16.30	4.19	2.35	15	0.13	0.24	0.24	0.24	2.58	3.16	115	0.74		671.44	671.16	675.24	674.96	677.44	4.75	676.10	3.69	2.20	1.14
FCB D3	FCB D2	D3	0.74	2.64	0.16	0.12	0.86	17.04	4.11	3.53	18	0.11	0.18	0.18	0.18	2.52	4.46	123	0.81		670.96	670.74	674.96	674.74	676.10	3.64	677.00	4.76	1.14	2.26
FCB D2	ES D1	D2	0.10	2.74	0.15	0.02	0.88	17.85	4.02	3.52	18	0.11	0.18	0.18	0.18	2.52	4.46	135	0.89		670.74	670.50	674.74	674.50	677.00	4.76	674.50	2.50	2.26	

EXISTING BELLEVILLE HIGH SCHOOL SITE - STORM SEWER DRAINAGE CALCULATIONS

CALCULATIONS PROVIDED TO CONFIRM EFFECT OF NEW ECDC STORM SEWER SYSTEM FLOW ON EXISTING HIGH SCHOOL SYSTEM. ORIGINAL STORM CALCULATIONS WERE RECREATED USING ORIGINAL HIGH SCHOOL PROJECT PLANS FOR STORM SEWER INFORMATION (PIPE SIZE, SLOPES, INVERT, ETC.) AS WELL AS LIMITED FIELD SURVEY INFORMATION COLLECTED ON THE HIGH SCHOOL'S SYSTEM AS PART OF THE CURRENT ECDC PROJECT. REFER TO BELLEVILLE HIGH SCHOOL REFERENCE SHEETS FOR INFORMATION ON EXISTING STORM SEWER SYSTEM USED IN THESE CALCULATIONS.

				(0.1.)		(0.1.)	L (O L)	(11)	L (0 L)	(0.1.)	(1.1)	(0.1.)	(0.1.)		(0.1.)	(0.1.)	_ (O)		_ (O)												3
(User)		(User)	(User)	(Calc)	(User)	(Calc)		(User)	(Calc)	(Calc)	(User)	(Calc)	(Calc)	(User)	(Calc)	(Calc)	(Calc)	(User)	(Calc)	Jump	Invert	Invert	HG	HG ,							}
MANHOLE		Area	Area	Accm	Imperv.	Equiv.	Accm.		(" ")	("Q") 	_ D	Min HG		Pipe	Actual	"V" fps	Cap.	L	Time of	at	Elev. at	Elev. at	Elev. at	Elev. at			5				Į .
		Name	Added	Area		Area	Equiv.		Inten.	Runoff		based		Slope	HG	Vel.@	Prov.	Pipe	Flow	MH (dn)	Up	Down	Up	Down	Up MH	Depth	DN MH	Depth	H.G. TO	H.G. TO	}
From	То		("A")		("C")	(AxC)	Area	("T")	In./Hr	(CFS)	(ın.)	on Q %	given D	(%)	(%)	HG	(CFS)	Length	(min)	?	MH	MH	MH	MH	Rim	RIM-T/P	Rim	RIM-T/P	RIM(Up)	RIM(Dn)	}
																															3
CB 3	CB 4	3	0.66	0.66	0.25	0.17	0.17	15.00	4.35	0.72	12	0.04	0.32	0.45	0.04	0.91	0.72	154	2.80		673.77	673.08	674.27	674.21	676.50	1.73	676.50	2.42	2.23	2.29	} -
																															3
CB 6	CB 7	6	0.78	0.78	0.48	0.37	0.37	15.00	4.35	1.63	12	0.21	0.32	1.00	0.21	2.07	1.63	66	0.53		673.17	672.50	674.05	673.91	677.00	2.83	677.25	3.75	2.95	3.34	}
																															{ -
ECDC	CB 9	NEW	0.65	0.65	0.50					1.60	10	0.53	0.42	0.46	0.53	2.93	1.60	159	0.90	1.02	674.50	673.77	675.29	674.44		0.35	676.88	2.28	0.39	2.44	}
CB 9	CB 10	9	0.27	0.92	0.28	0.08	0.40	15.90	4.24	1.69	12	0.22	0.32	0.23	0.23	2.18	1.71	133	1.02		672.62	672.31	674.09	673.78	676.88	3.26	677.25	3.94	2.79	3.47	} _
																															3
CB 14	CB 15	14	0.22	0.22	0.25	0.06	0.06	15.00	4.35	0.24	12	0.00	0.32	1.25	0.00	0.30	0.24	103	5.61		673.05	671.76	673.08	673.08	676.25	2.20	676.25	3.49	3.17	3.17	}
																															\{ -
CB 16	CB 17	16	0.39	0.39	0.82	0.32	0.32	15.00	4.35	1.39	12	0.15	0.32	1.30	0.15	1.77	1.39	107	1.00		673.05	671.67	673.10	672.94	676.25	2.20	676.25	3.58	3.15	3.31	3
														=																	} _
CB 18	CB 19	18	0.63	0.63	0.85	0.54	0.54	15.00	4.35	2.33	12	0.43	0.32	1.15	0.43	2.97	2.33	148	0.83		673.05	671.36	673.15	672.52	676.25	2.20	676.25	3.89	3.10	3.73	3
																															}
CB 24	CB 25	24	0.28	0.28	0.81	0.23	0.23	15.00	4.35	0.99	12	0.08	0.32	1.50	0.08	1.26	0.99	66	0.88		673.54	672.55	673.59	673.54	676.75	2.21	676.75	3.20	3.16	3.21	\ -
																															}
CB 26	CB 27	26	0.26	0.26	0.95	0.25	0.25	15.00	4.35	1.07	12	0.09	0.32	2.00	0.09	1.37	1.07	64	0.78		673.50	672.22	673.08	673.02	676.75	2.25	676.75	3.53	3.67	3.73	}
																			L												} -
CB 21	CB 22	21	0.25	0.25	0.62			15.00		0.67	12	0.04	0.32	0.30	0.04	0.86	0.67	63	1.23		673.56	673.37	674.19	674.17		2.19	676.75	2.38	2.56	2.58	}
CB 22	CB 23	22	0.13	0.38	0.74		0.25	16.23		1.06	12	0.09	0.32	0.30	0.09	1.34	1.06	125	1.55		673.37	672.99	673.90	673.79	676.75	2.38	676.75	2.76	2.85	2.96	\ _
CB 23	CB 25	23	0.12	0.50	0.76	0.09	0.34	17.78		1.38	12	0.15	0.32	0.30	0.15	1.76	1.38	147	1.40		672.99	672.55	673.76	673.54	676.75	2.76	676.75	3.20	2.99	3.21	} -
CB 25	CB 27	25	0.34	1.12	0.87	0.30	0.87	19.18		3.36	15	0.27	0.24	0.28	0.27	2.74	3.36	117	0.71		672.55	672.22	673.54	673.22	676.75	2.95	676.75	3.28	3.21	3.53	{
CB 27	CB 28	27	0.28	1.66	0.95	0.27	1.38	19.89	3.81	5.26	15	0.66	0.24	1.25	0.66	4.28	5.26	117	0.46		672.22	670.76	672.95	672.18	676.75	3.28	676.75	4.74	3.80	4.57	3
																															} _
CB 1	CB 2	1	0.58	0.58	0.25	0.15	0.15	15.00		0.63	12	0.03	0.32	0.30	0.03	0.80	0.63	111	2.31		673.80	673.47	674.33	674.30	676.50	1.70	677.00	2.53	2.17	2.70	\
CB 2	CB 4	2	0.13	0.71	0.61	0.08	0.22	17.31		0.92	12	0.07	0.32	0.30	0.07	1.17	0.92	130	1.85		673.47	673.08	674.30	674.21		2.53	676.50	2.42	2.70	2.29	} -
CB 4	CB 5	4	0.56	1.93	0.35	0.20	0.59	19.16		2.27	15	0.12	0.24	0.28	0.12	1.85	2.27	161	1.44		673.08	672.63	674.21	674.01	676.50	2.17	676.50	2.62	2.29	2.49	{ -
CB 5	CB 7	5	1.22	3.15	0.44	0.54	1.12	20.61		4.21	18	0.16	0.18	1.00	0.16	2.38	4.21	62	0.44		672.63	672.00		673.91		2.37	677.25	3.75	2.49	3.34	3
CB 7	CB 8	7	0.27	4.20	0.56	0.15		21.04		6.11	24	0.07	0.12	0.11	0.07	1.94	6.11	104	0.89		671.50	671.39	673.91	673.83	677.25	3.75	678.65	5.26	3.34	4.82	} -
CB 8	CB 10	8	0.07	4.27	0.45	0.03	1.68	21.93		6.09	24	0.07	0.12	0.11	0.07	1.94	6.09	69	0.59		671.39	671.31	673.83	673.78	678.65	5.26	677.25	3.94	4.82	3.47	\ -
CB 10	CB 11	10	0.49	5.68	0.34	0.17	2.24	22.52		8.03	24	0.13	0.12	0.11	0.13	2.56	8.03	178	1.16		671.31	671.12	673.78	673.56	677.25	3.94	677.75	4.63	3.47	4.19	}
CB 11	CB 12	11	0.54	6.22	0.32	0.17	2.42	23.69		8.42	24	0.14	0.12	0.11	0.14	2.68	8.42	93	0.58		671.12	671.01	673.56	673.43	677.75	4.63	677.60	4.59	4.19	4.17	} -
CB 12	CB 13	12	0.34	6.56	0.29	0.10	2.52	24.27	3.44	8.64	24	0.15	0.12	0.11	0.15	2.75	8.65	85	0.51		671.01	670.92	673.43	673.31	677.60	4.59	677.00	4.08	4.17	3.69) –
CB 13	CB 15	13	0.48	7.04	0.28			24.78		9.00	24	0.16	0.12	0.11	0.16	2.87	9.00	142	0.83		670.92	670.76	673.31	673.08	677.00	4.08	676.25	3.49	3.69	3.17	}
CB 15	CB 17	15	0.32				2.91			9.71	24	0.18	0.12	0.13	0.18	3.09	9.71	74	0.40				673.08			3.49	676.25	3.58	3.17	3.31	\ -
CB 17	CB 19	17	0.40	8.37	0.83			26.01		11.78	24	0.27	0.12	0.20	0.27	3.75	11.78	157	0.70		670.67	670.36		672.52		3.58	676.25	3.89	3.31	3.73	3 -
CB 19	CB 20	19	0.73							15.41	30	0.14	0.09	0.15	0.14	3.14	15.41	168	0.89			669.60				3.89	676.75	4.65	3.73	4.47	}
CB 20	CB 28	20	0.39	10.12					3.20		30	0.16	0.09	0.15	0.16	3.30	16.22	64	0.32		669.60	669.51				4.65	676.75	4.74	4.47	4.57	ξ -
CB 28	ES	28	0.39	12.17	0.88	0.34	6.80	27.92	3.17	21.57	30	0.28	0.09	0.15	0.28	4.40	21.57	138	0.52		669.51	669.30	672.18	6/1.80	676.75	4.74	673.80	2.00	4.57	2.00	} -
																														سررررر	/
																											متتنير	تتتمين	٠٠٠٠٠		
																							_	برزر	سررر		-				_
																					سررر.	منتند	مرزرر								
																		مبير	مرزر	سررر	, ·										
															سيرير	مررر	بررر														_
											مدي .	برزر	مررر	تبرر																	
							هيد	مبرر	مرزر	سررر																					
				منترر	تترير	سممر																									_
	برز	سمير	مررر	J																										,,,,,,,,,	
<i>ر</i> .	- سرر																														
مرر																															_



INTEGRATED design SOLUTIONS architecture engineering interiors & technology

1441 west long lake, suite 200 troy, michigan 48098

troy, michigan 48098
5211 cascade road SE, suite 300
grand rapids, michigan 49546
248.823.2100
www.ids-michigan.com

CIVIL ENGINEER
SPALDING DeDECKER
905 south blvd. E
rochester hills, michigan 48307

800.598.1600 www.sda-eng.com STRUCTURAL ENGINEER

SDI Structures
275 east liberty

ann arbor, michigan 48104 734.213.6091

www.sdistructures.com

Project Title



Van Buren Public Schools

The Early Childhood Development Center

Davis St. Belleville, MI 48111

	Project Administrator
	V. Grant
	Project Designer
	J. Ensley
	Project Architect / Engineer
	J. Ensley
	Drawn By
	C. Yang
	Q.M. Review
	T. Sovel
	Approved
	T. Sovel
	Drawing Scale
	As Noted
Issued for	Issue Date
Issued for Design Development	
	06-19-2020
Design Development	06-19-2020 08-14-2020
Design Development	06-19-2020 08-14-2020 09-08-2020
Design Development Bid Package 1 Addendum No. 3	06-19-2020 08-14-2020 09-08-2020 11-02-2020
Design Development Bid Package 1 Addendum No. 3 City Engineering Review No. 2	06-19-2020 08-14-2020 09-08-2020 11-02-2020 11-04-2020
Design Development Bid Package 1 Addendum No. 3 City Engineering Review No. 2 Bulletin No. 1	06-19-2020 08-14-2020 09-08-2020 11-02-2020 11-04-2020 11-18-2020
Design Development Bid Package 1 Addendum No. 3 City Engineering Review No. 2 Bulletin No. 1 City Engineering Review No. 3	06-19-2020 08-14-2020 09-08-2020 11-02-2020 11-04-2020 11-18-2020 12-07-2020
Design Development Bid Package 1 Addendum No. 3 City Engineering Review No. 2 Bulletin No. 1 City Engineering Review No. 3 City Engineering Review No. 3	06-19-2020 08-14-2020 09-08-2020 11-02-2020 11-04-2020 11-18-2020 12-07-2020
Design Development Bid Package 1 Addendum No. 3 City Engineering Review No. 2 Bulletin No. 1 City Engineering Review No. 3 City Engineering Review No. 3 EGLE Water Supply Permit	06-19-2020 08-14-2020 09-08-2020 11-02-2020 11-04-2020 11-18-2020 12-07-2020

© 2020 INTEGRATED design solutions, LLC IDS Drawing Title

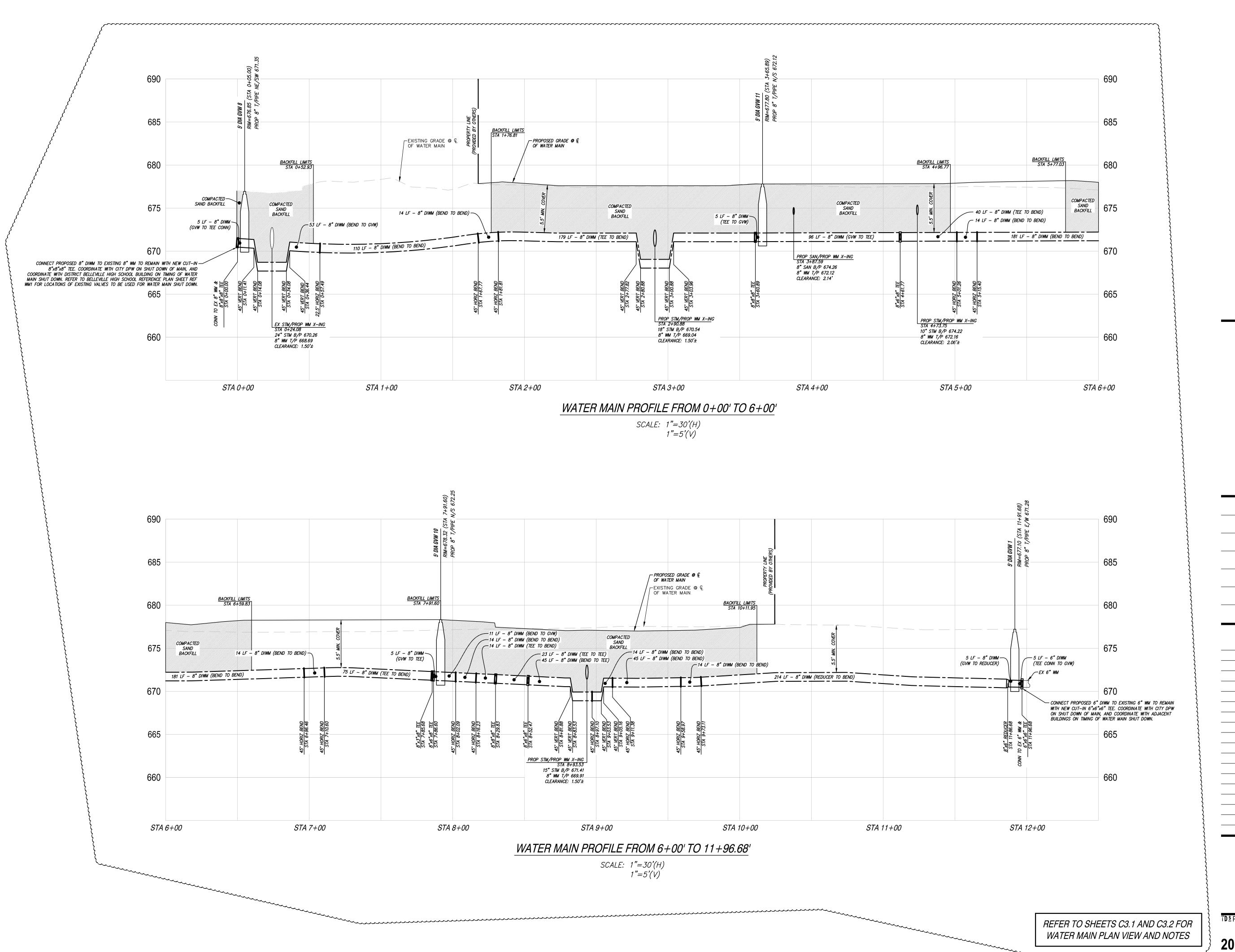
Sewer and Detention

Storm Sewer and Detention Calculations

ī**D**§ Project Number

Drawing Number





INTEGRATED design SOLUTIONS architecture engineering interiors & technology 1441 west long lake, suite 200

troy, michigan 48098
5211 cascade road SE, suite 300
grand rapids, michigan 49546
248.823.2100

www.ids-michigan.com

CIVIL ENGINEER

SPALDING DeDECKER 905 south blvd. E rochester hills, michigan 48307 800.598.1600 www.sda-eng.com

STRUCTURAL ENGINEER
SDI Structures
275 east liberty

275 east liberty ann arbor, michigan 48104 734.213.6091 www.sdistructures.com

Project Title



Van Buren Public Schools

The Early Childhood Development Center

Davis St.
Belleville, MI 48111

Project Adn	ninistrator
V	/. Grant
•	Designer
	Ensley
Project Architect /	•
	Ensley
	Drawn By
	C. Yang
	M. Review
	Γ. Sovel
	Approved Γ. Sovel
	ving Scale
	s Noted
Issued for Issu	ue Date
Design Development 06-1	19-2020
Bid Package 1 08-1	14-2020
Addendum No. 3 09-0	8-2020
City Engineering Review No. 2 11-0	2-2020
Bulletin No. 1 11-0	04-2020
City Engineering Review No. 3 11-1	8-2020
City Engineering Revisions 12-0	7-2020
EGLE Water Supply Permit 12-0	7-2020
<u> </u>	08-2020

 \circ 2020 Integrated design solutions, LLC IDS Drawing Title

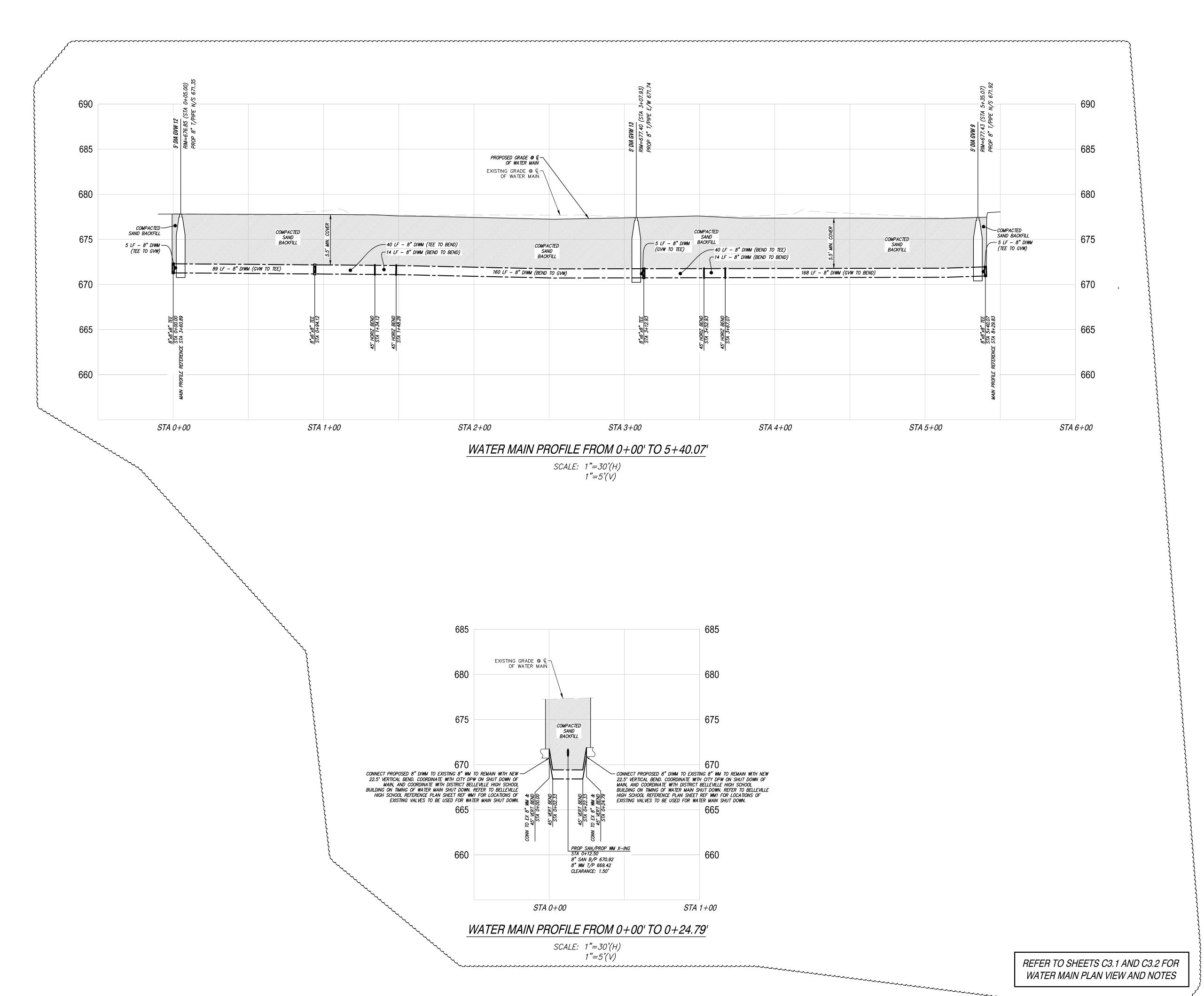
Water Main Profiles

ī**D** § Project Number

Drawing Number

20111-1000SDA Project No. NP20062

C3.8



INTEGRATED design solutions architecture engineering interiors & technology

1441 west long lake, suite 200 troy, michigan 48098 5211 cascade road SE, suite 300 grand rapids, michigan 49546

www.ids-michigan.com

CIVIL ENGINEER SPALDING DeDECKER 905 south blvd. E

rochester hills, michigan 48307 800.598.1600 www.sda-eng.com

STRUCTURAL ENGINEER SDI Structures 275 east liberty ann arbor, michigan 48104 734.213.6091 www.sdistructures.com



Van Buren Public Schools

The Early Childhood **Development Center**

Davis St. Belleville, MI 48111

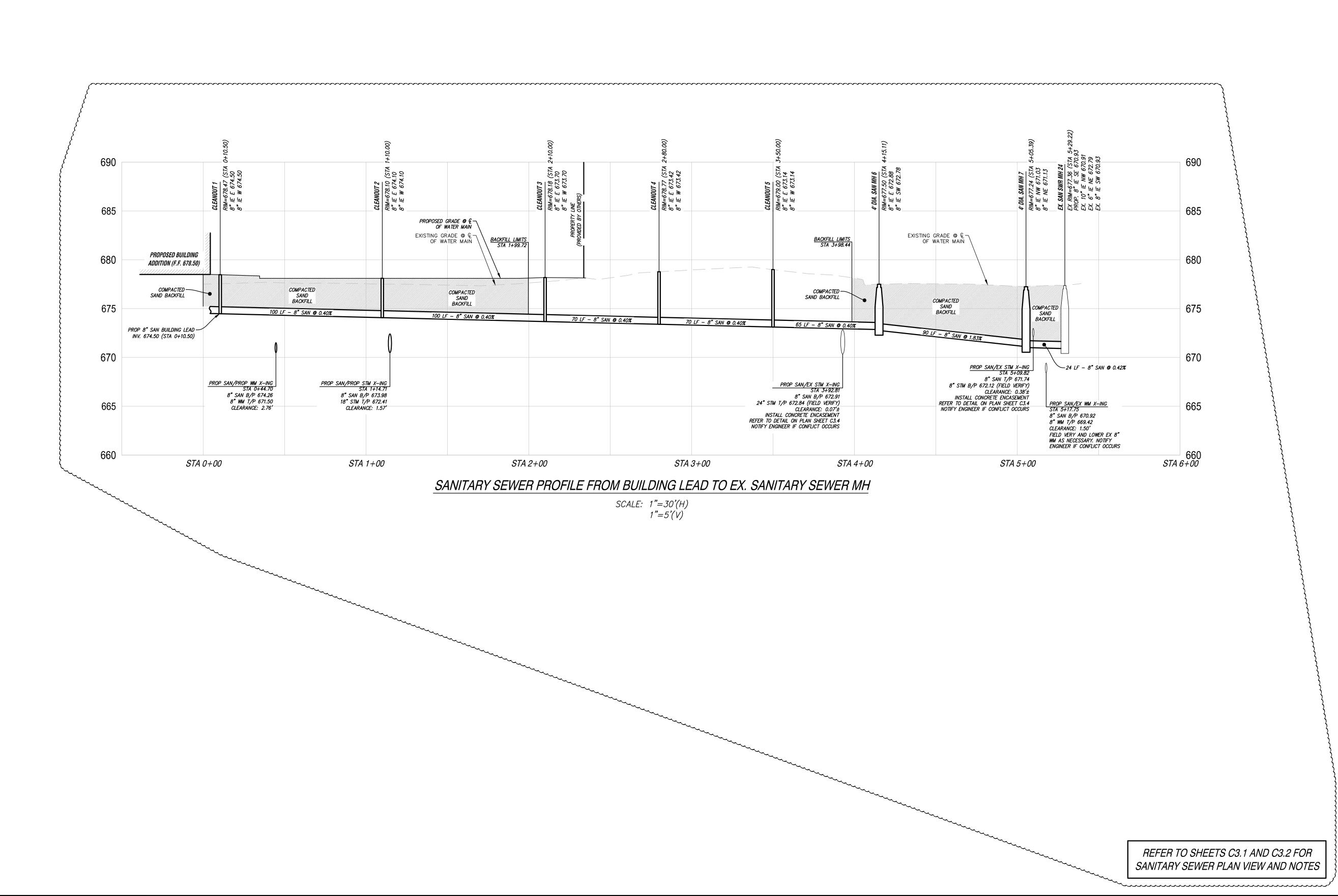
Project Administrator	
V. Grant	
Project Designer	
J. Ensley	
ect Architect / Engineer	P
J. Ensley	
Drawn By	
C. Yang	
Q.M. Review	
T. Sovel	
Approved	
T. Sovel	
Drawing Scale	
As Noted	
Issue Date	Issued for
06-19-2020	Design Development
08-14-2020	Bid Package 1
	Addendum No. 3
09-08-2020	/ tadendam No. 0
09-08-2020 11-02-2020	City Engineering Review No. 2
11-02-2020	City Engineering Review No. 2
11-02-2020 11-04-2020	City Engineering Review No. 2 Bulletin No. 1
11-02-2020 11-04-2020 11-18-2020	City Engineering Review No. 2 Bulletin No. 1 City Engineering Review No. 3

 \circ 2020 Integrated design solutions, LLC **IDS Drawing Title**

Water Main Profiles

ī**D** § Project Number

Drawing Number



INTEGRATED design SOLUTIONS architecture engineering interiors & technology

1441 west long lake, suite 200 troy, michigan 48098
5211 cascade road SE, suite 300 grand rapids, michigan 49546
248.823.2100
www.ids-michigan.com

CIVIL ENGINEER SPALDING DeDECKER 905 south blvd. E

rochester hills, michigan 48307 800.598.1600 www.sda-eng.com

STRUCTURAL ENGINEER
SDI Structures
275 east liberty
ann arbor, michigan 48104
734.213.6091
www.sdistructures.com

Project Title



Van Buren Public Schools

The Early Childhood Development Center

Davis St. Belleville, MI 48111

Project Administrator

	V. Grant
	Project Designer J. Ensley
	Project Architect / Engineer J. Ensley
	Drawn By C. Yang
	Q.M. Review
	T. Sovel
	Approved T. Sovel
	Drawing Scale
	As Noted
Issued for	Issue Date
Design Development	06-19-2020
Bid Package 1	08-14-2020
Addendum No. 3	09-08-2020
City Engineering Review No. 2	11-02-2020
Bulletin No. 1	11-04-2020
City Engineering Review No. 3	11-18-2020
City Engineering Revisions	12-07-2020
EGLE Water Supply Permit	12-07-2020
Bulletin No. 1 Revised	12-08-2020

© 2020 INTEGRATED design solutions, LLC IDS Drawing Title

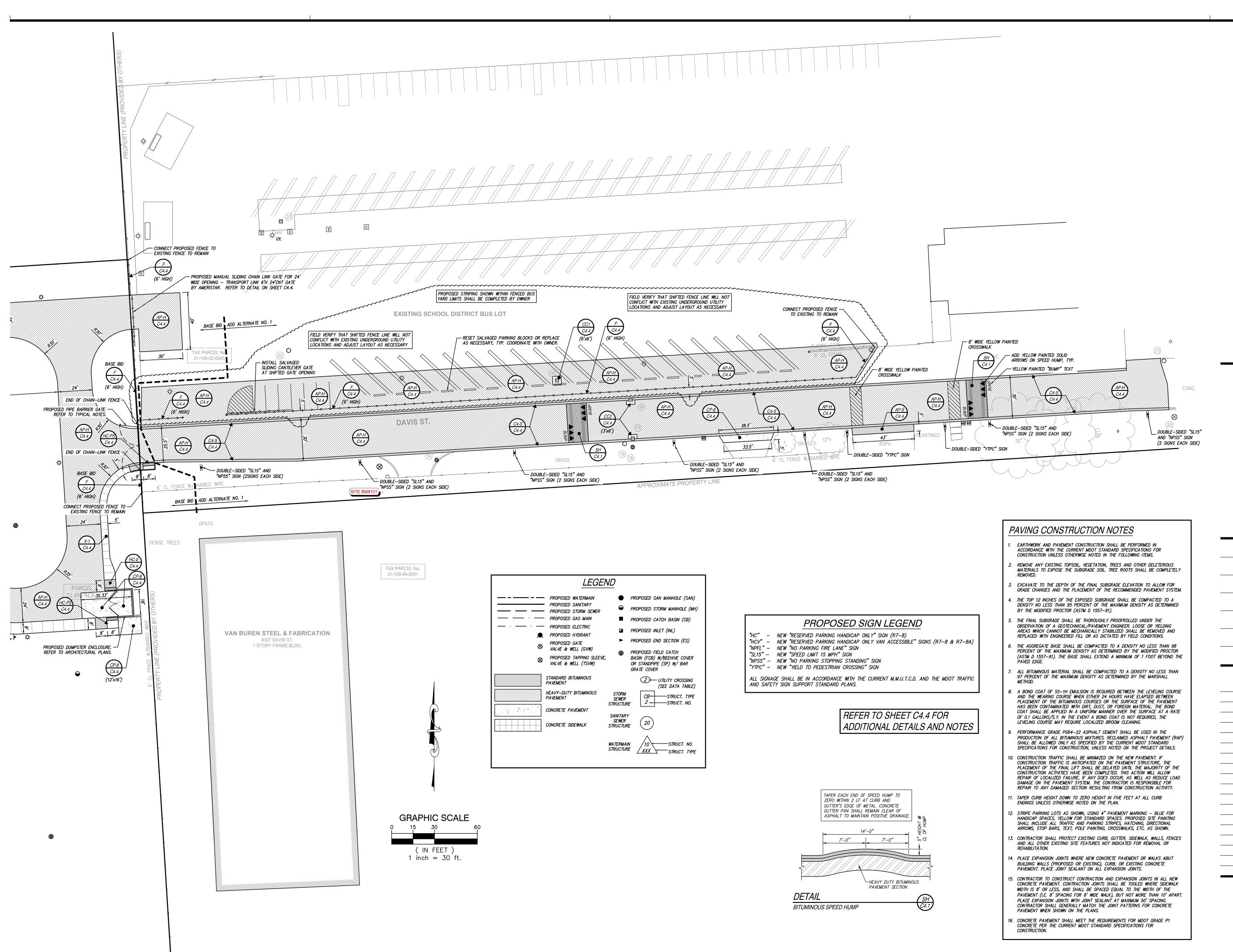
Sanitary Sewer Profiles

ī**D** § Project Number

Drawing Number

20111-1000SDA Project No. NP20062

000 (C3.10)



INTEGRATED design SOLUTIONS architecture engineering interiors & technology

1441 west long lake, suite 200 troy, michigan 48098
5211 cascade road SE, suite 300 grand rapids, michigan 49546
248.823.2100

www.ids-michigan.com

CIVIL ENGINEER

SPALDING DeDECKER

905 south blvd. E rochester hills, michigan 48307 800.598.1600 www.sda-eng.com

STRUCTURAL ENGINEER
SDI Structures
275 east liberty

ann arbor, michigan 48104 734.213.6091 www.sdistructures.com

Project Title



Van Buren Public Schools

The Early Childhood Development Center

Davis St. Belleville, MI 48111

Project Administrator

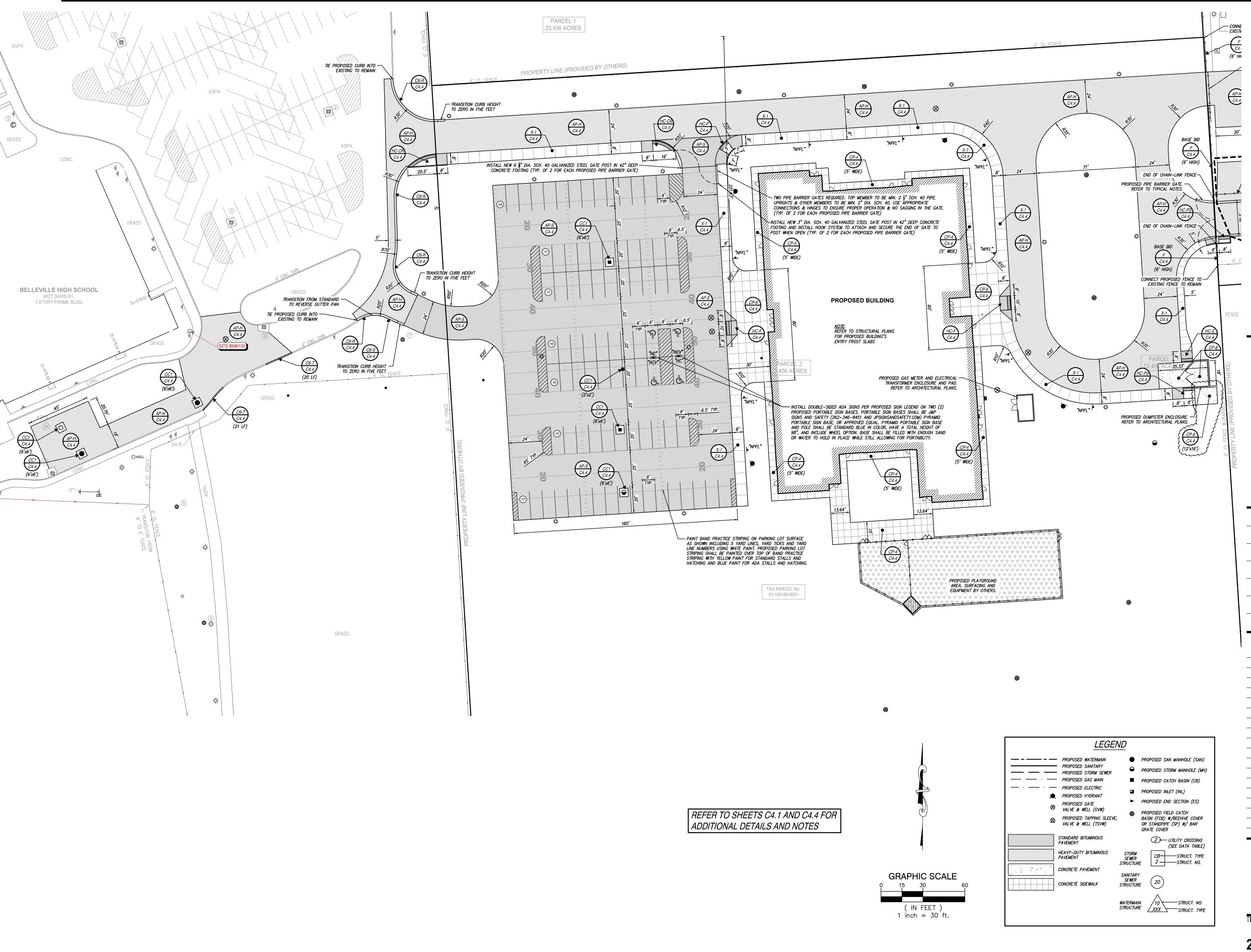
V. Grant	
Project Designer	
J. Ensley	
ect Architect / Engineer	Proj
J. Ensley	
Drawn By	
C. Yang	
Q.M. Review	
T. Sovel	
Approved T. Sovel	
Drawing Scale	
As Noted	
Issue Date	Issued for
00.40.000	D : D 1 (
06-19-2020	Design Development
06-19-2020 08-14-2020	Bid Package 1
	<u> </u>
08-14-2020	Bid Package 1
08-14-2020 09-08-2020	Bid Package 1 Addendum No. 3
08-14-2020 09-08-2020 11-02-2020	Bid Package 1 Addendum No. 3 City Engineering Review No. 2
08-14-2020 09-08-2020 11-02-2020 11-04-2020	Bid Package 1 Addendum No. 3 City Engineering Review No. 2 Bulletin No. 1
08-14-2020 09-08-2020 11-02-2020 11-04-2020 11-18-2020	Bid Package 1 Addendum No. 3 City Engineering Review No. 2 Bulletin No. 1 City Engineering Review No. 3
08-14-2020 09-08-2020 11-02-2020 11-04-2020 11-18-2020 12-07-2020	Bid Package 1 Addendum No. 3 City Engineering Review No. 2 Bulletin No. 1 City Engineering Review No. 3 City Engineering Revisions
08-14-2020 09-08-2020 11-02-2020 11-04-2020 11-18-2020 12-07-2020 12-07-2020	Bid Package 1 Addendum No. 3 City Engineering Review No. 2 Bulletin No. 1 City Engineering Review No. 3 City Engineering Revisions EGLE Water Supply Permit

 \circ 2020 Integrated design solutions, LLC IDS Drawing Title

Paving and Layout Plan
Area "A"

ī D § Project Number

Drawing Number



INTEGRATED design SOLUTIONS architecture engineering interiors & technology 1441 west long lake, suite 200

troy, michigan 48098
5211 cascade road SE, suite 300
grand rapids, michigan 49546
248.823.2100

CIVIL ENGINEER

www.ids-michigan.com

SPALDING DeDECKER 905 south blvd. E rochester hills, michigan 48307 800.598.1600 www.sda-eng.com

STRUCTURAL ENGINEER
SDI Structures

SDI Structures 275 east liberty ann arbor, michigan 48104 734.213.6091 www.sdistructures.com

Project Title



Van Buren Public Schools

The Early Childhood Development Center

Davis St. Belleville, MI 48111

Project Administrator

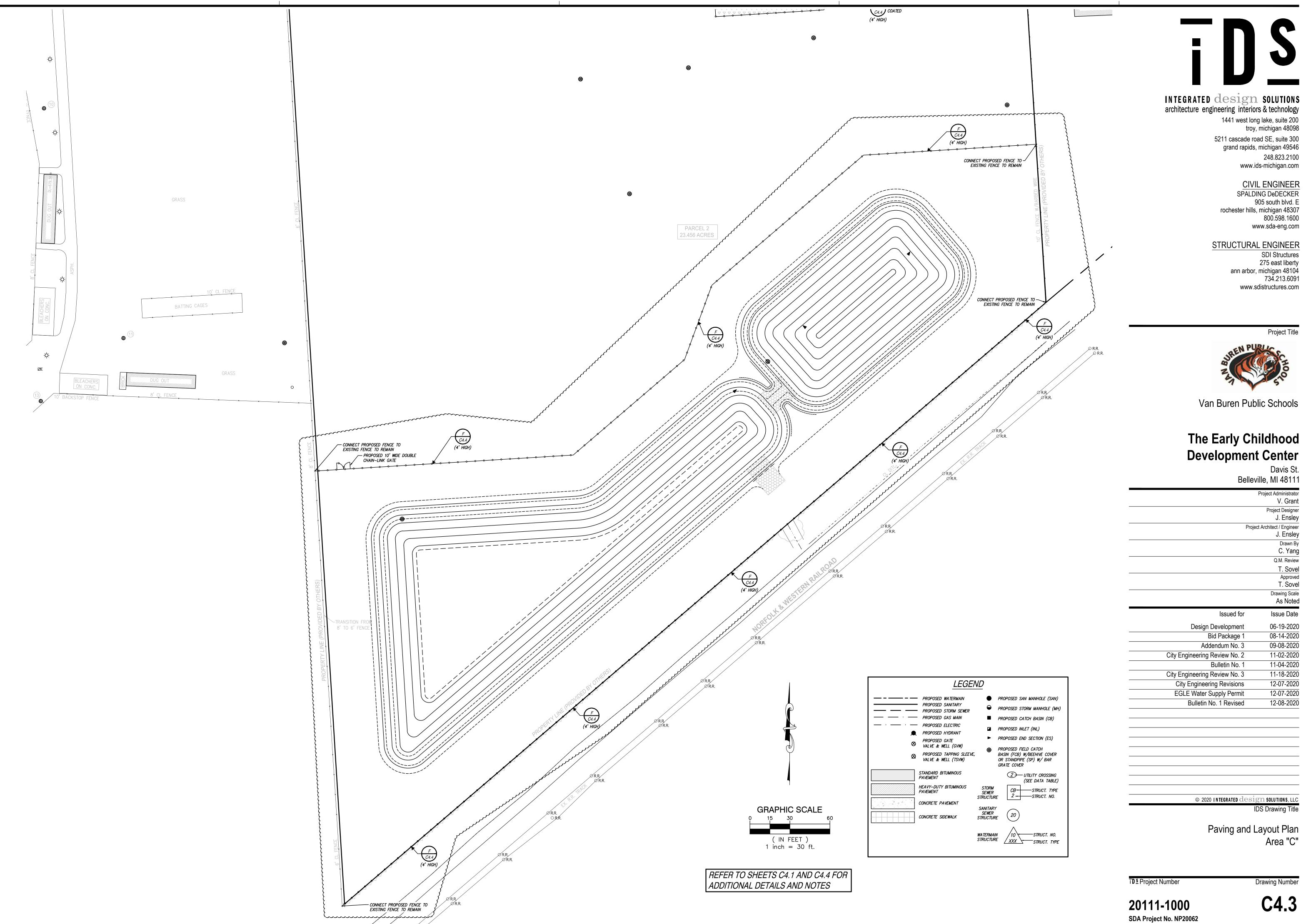
	V. Grant
	Project Designer
	J. Ensley
Project	ct Architect / Engineer
	J. Ensley
	Drawn By
	C. Yang
	Q.M. Review
	T. Sovel Approved
	T. Sovel
	Drawing Scale
	As Noted
Issued for	Issue Date
133000 101	
Danieus Danielaus aut	
Design Development	06-19-2020
Bid Package 1	06-19-2020 08-14-2020
<u> </u>	
Bid Package 1	08-14-2020
Bid Package 1 Addendum No. 3	08-14-2020 09-08-2020
Bid Package 1 Addendum No. 3 City Engineering Review No. 2	08-14-2020 09-08-2020 11-02-2020
Bid Package 1 Addendum No. 3 City Engineering Review No. 2 Bulletin No. 1	08-14-2020 09-08-2020 11-02-2020 11-04-2020
Bid Package 1 Addendum No. 3 City Engineering Review No. 2 Bulletin No. 1 City Engineering Review No. 3	08-14-2020 09-08-2020 11-02-2020 11-04-2020 11-18-2020
Bid Package 1 Addendum No. 3 City Engineering Review No. 2 Bulletin No. 1 City Engineering Review No. 3 City Engineering Revisions	08-14-2020 09-08-2020 11-02-2020 11-04-2020 11-18-2020 12-07-2020
Bid Package 1 Addendum No. 3 City Engineering Review No. 2 Bulletin No. 1 City Engineering Review No. 3 City Engineering Revisions EGLE Water Supply Permit	08-14-2020 09-08-2020 11-02-2020 11-04-2020 11-18-2020 12-07-2020 12-07-2020

 \circ 2020 Integrated design solutions, LLC IDS Drawing Title

Paving and Layout Plan
Area "B"

ī **D** <u>s</u> Project Number

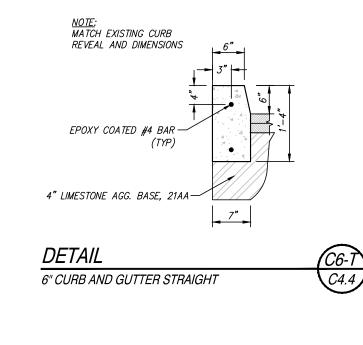
Drawing Number

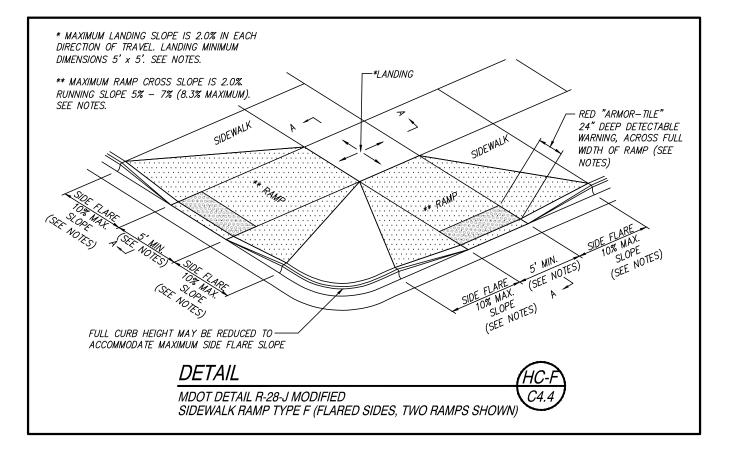


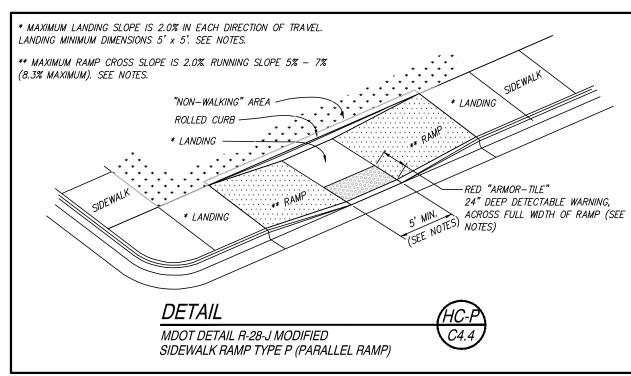
	Project Designer
	J. Ensley
Pr	oject Architect / Engineer
	J. Ensley
	Drawn By
	C. Yang
	Q.M. Review
	T. Sovel
	Approved
	T. Sovel
	Drawing Scale
	As Noted
Issued for	Issue Date
Design Development	06-19-2020
Bid Package 1	08-14-2020
Addendum No. 3	09-08-2020
City Engineering Review No. 2	11-02-2020
Bulletin No. 1	11-04-2020
City Engineering Review No. 3	11-18-2020
City Engineering Revisions	12-07-2020
EGLE Water Supply Permit	12-07-2020
Bulletin No. 1 Revised	12-08-2020
	•

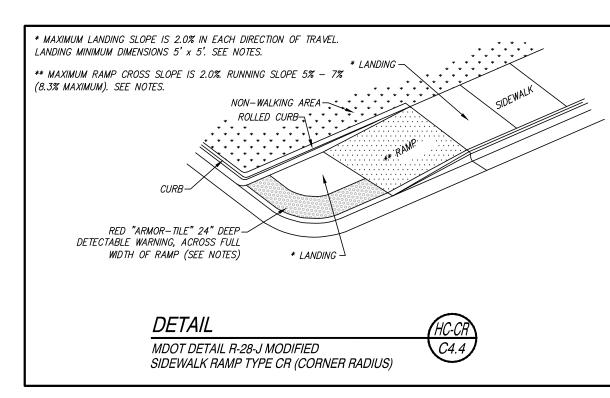
SIDEWALK RAMP NOTES (MDOT DETAIL R-28-J MODIFIED)

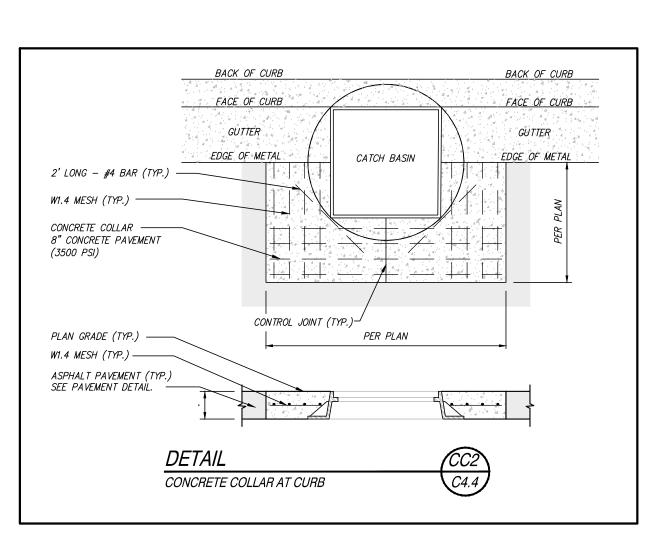
- . DETAILS SPECIFIED ON THIS PLAN APPLY TO ALL CONSTRUCTION, RECONSTRUCTION, OR ALTERATION OF STREETS, CURBS, OR SIDEWALKS BY ALL PUBLIC AGENCIES AND BY ALL PRIVATE ORGANIZATIONS CONSTRUCTING FACILITIES FOR PUBLIC USE.
- 2. SIDEWALK RAMPS ARE TO BE LOCATED AS SPECIFIED ON THE PLANS OR AS DIRECTED BY THE ENGINEER.
- 3. SURFACE TEXTURE OF THE RAMP SHALL BE THAT OBTAINED BY A COARSE BROOMING, TRANSVERSE TO THE RUNNING SLOPE.
- 1. CARE SHALL BE TAKEN TO ASSURE A UNIFORM GRADE ON THE RAMP. WHERE CONDITIONS PERMIT, IT IS DESIRABLE THAT THE SLOPE OF THE RAMP BE IN ONLY ONE DIRECTION, PARALLEL TO THE DIRECTION OF TRAVEL. 5. PROVIDE TURNING SPACES WHERE PEDESTRIAN TURNING MOVEMENTS ARE REQUIRED.
- 6. CURB RAMPS WITH RUNNING SLOPE EQUAL TO OR LESS THAN 5% DO NOT REQUIRE A TOP LANDING. HOWEVER, ANY CONTINUOUS SIDEWALK OR PEDESTRIAN ROUTE CROSSING THROUGH OR INTERSECTING THE CURB RAMP MUST INDEPENDENTLY MAINTAIN A CROSS SLOPE NOT GREATER THAN 2% PERPENDICULAR TO ITS OWN DIRECTION(S) OF TRAVEL.
- 7. DETECTABLE WARNING SURFACE COVERAGE IS 24" MINIMUM IN THE DIRECTION OF RAMP/PATH TRAVEL AND THE FULL WIDTH OF THE RAMP/PATH OPENING EXCLUDING CURBED OR FLARED CURB TRANSITION AREAS. A BORDER OFFSET NOT GREATER THAN 2" MEASURED ALONG THE EDGES OF THE DETECTABLE WARNING IS ALLOWABLE. FOR RADIAL CURB THE OFFSET IS MEASURED FROM THE ENDS OF THE RADIUS.
- 3. THE MAXIMUM RUNNING SLOPE OF 8.3% IS RELATIVE TO A FLAT (0%) REFERENCE. HOWEVER, IT SHALL NOT REQUIRE ANY RAMP OR SERIES OF RAMPS TO EXCEED 15 FEET IN LENGTH INCLUDING LANDINGS OR TRANSITIONS. 9. THE TOP OF THE JOINT FILLER FOR ALL RAMP TYPES SHALL BE FLUSH WITH THE ADJACENT CONCRETE.
- 10. FLARED SIDES WITH A SLOPE OF 10% MAXIMUM, MEASURED ALONG THE ROADSIDE CURB LINE, SHALL BE PROVIDED WHERE AN UNOBSTRUCTED CIRCULATION PATH LATERALLY CROSSES THE SIDEWALK RAMP. FLARED SIDES ARE NOT REQUIRED WHERE THE RAMP IS BORDERED BY LANDSCAPING, UNPAVED SURFACE OR PERMANENT FIXED OBJECTS. WHERE THEY ARE NOT REQUIRED, FLARED SIDES CAN BE CONSIDERED IN ORDER TO AVOID SHARP CURB RETURNS AT RAMP OPENINGS.
- . DETECTABLE WARNING PLATES MUST BE INSTALLED USING FABRICATED OR FIELD CUT UNITS CAST AND/OR ANCHORED IN THE PAVEMENT TO RESIST SHIFTING OR HEAVING. DETECTABLE WARNING PLATES TO BE RED CAST-IN-PLACE "ARMOR-TILE", OR APPROVED EQUAL, IN ACCORDANCE WITH ANSI SECTIONS 406.13 AND 705, AND ADA CODE OF REGULATION A4.29.

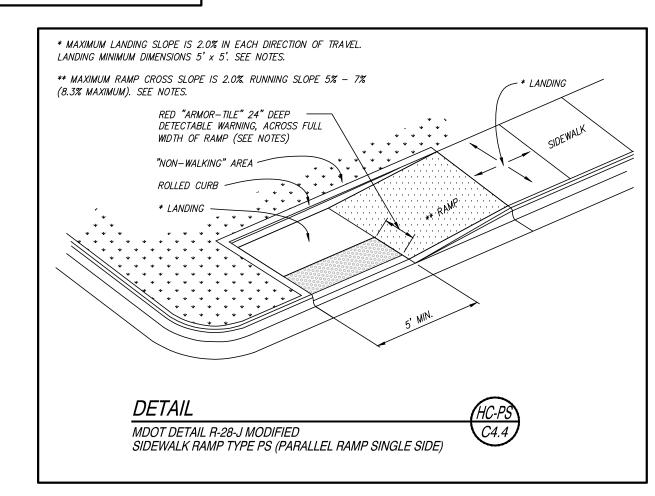


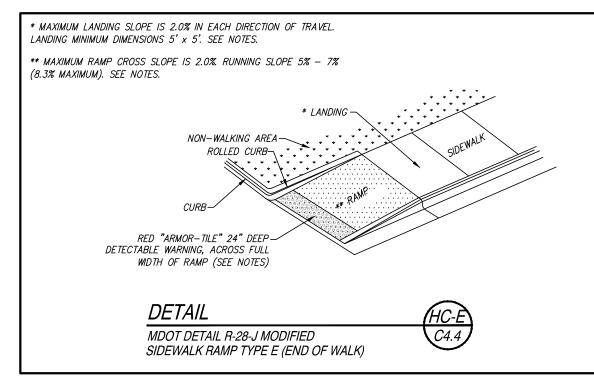


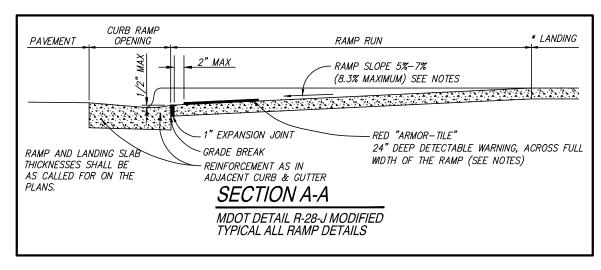


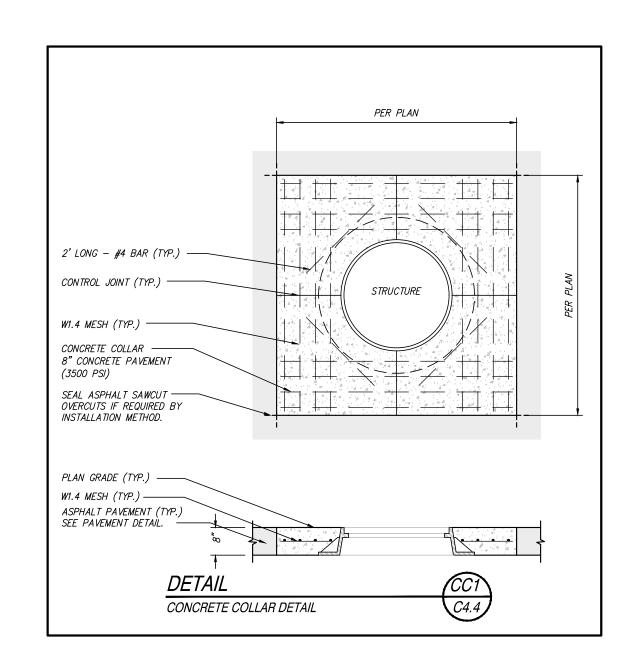


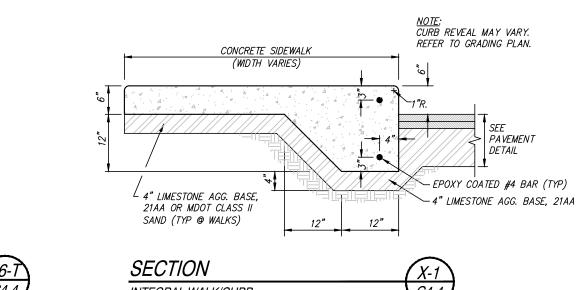


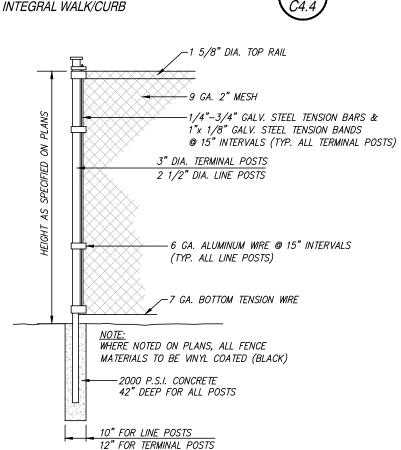


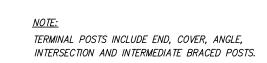












PART 1 - GENERAL 1.01 WORK INCLUDED

1.02 RELATED WORK

Section 31 2000 – Earth Moving 1.03 SYSTEM DESCRIPTION

1.04 QUALITY ASSURANCE

submitted prior to installation.

PART 2 - MATERIALS

2.01 MANUFACTURER

materials and techniques specified.

ASTM B117 - Practice for Operating Salt-Spray (Fog) Apparatus.

ASTM D3359 - Test Method for Measuring Adhesion by Tape Test.

ASTM F1184 – Industrial & Commercial Horizontal Slide Gates

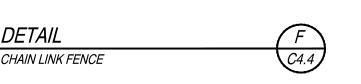
ASTM B221 - Aluminum and Aluminum-Alloy

ASTM D523 - Test Method for Specular Gloss.

Carbon-Arc Light and Water Exposure Apparatus

1.07 PRODUCT HANDLING AND STORAGE

system defined herein at the project site.



GATE RECEIVER POST

AMERISTAR FENCE PRODUCTS

TRANSPORT LINK – Enclosed Track Industrial Aluminum Cantilever Gate System

Construction Specification – SECTION 32 31 00

The manufacturer shall supply a total industrial ornamental aluminum cantilever gate system of the Ameristar® TransPort LINK design. Extended uprights for barb-wire are not required. The system shall include all components (i.e., tracks,

uprights, bracing, pickets, hardware, fittings and fasteners) required. NOTE: CHAIN LINK FABRIC AND BARB-WIRE

ruded Bars, Rods, Wire, Profiles and Tubes.

ARE NOT PROVIDED BY AMERISTAR. Contractor to provide chain link fabric to match adjacent proposed fencing.

ASTM D822 - Practice for Conducting Tests on Paint and Related Coatings and Materials using Filtered Open-Flame

ASTM D1654 - Test Method for Evaluation of Painted or Coated Specimens Subjected to Corrosive Environments.

ASTM D2244 - Test Method for Calculation of Color Differences from Instrumentally Measured Color Coordinates.

ASTM D2794 - Test Method for Resistance of Organic Coatings to the Effects of Rapid Deformation (Impact).

The manufacturer's submittal package consisting of gate elevations, hardware details, and installation details, shall be

Upon receipt at the job site, all materials shall be checked to ensure that no damage occurred during shipping or handling.

Materials shall be stored in such a manner to ensure proper ventilation and drainage, and to protect against damage, weather,

All industrial ornamental aluminum cantilever gates shall conform to the Ameristar® TransPort LINK gate system, without

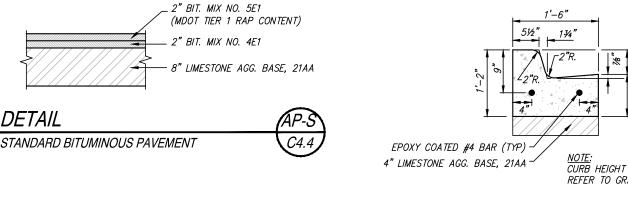
extended uprights, manufactured by Ameristar Fence Products, Inc., in Tulsa, Oklahoma. The project gate schedule shall

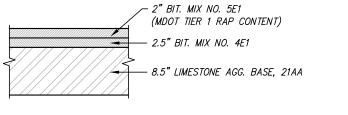
22'-24' OPENING

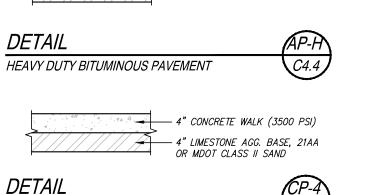
- 421½" — **ELEVATION VIEW**

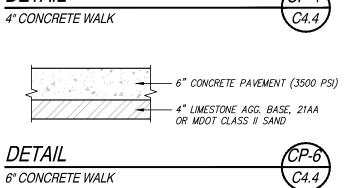
FENCE -

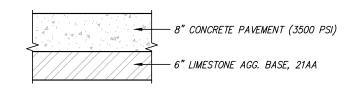
LINE FENCE







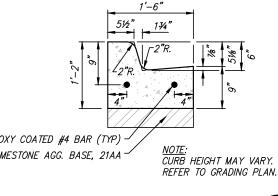




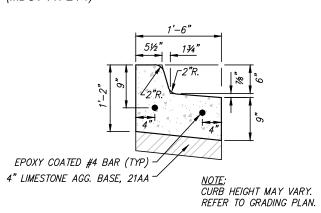


FENCE LINE

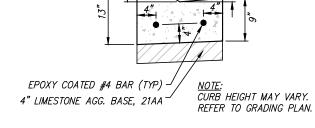
FENCE POST





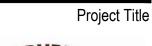


DETAIL C4.4 6" CURB & GUTTER REVERSE PAN



C4.4

DETAIL 4" MOUNTABLE CURB & GUTTER STANDARD PAN



ann arbor, michigan 48104

www.sdistructures.com



Van Buren Public Schools

The Early Childhood **Development Center**

INTEGRATED design solutions

architecture engineering interiors & technology

1441 west long lake, suite 200

5211 cascade road SE, suite 300 grand rapids, michigan 49546

troy, michigan 48098

www.ids-michigan.com

CIVIL ENGINEER

905 south blvd. E

www.sda-eng.com

800.598.1600

SDI Structures 275 east liberty

734.213.6091

SPALDING DeDECKER

rochester hills, michigan 48307

STRUCTURAL ENGINEER

248.823.2100

Belleville, MI 48111

Project Administrator

V. Grant

	Project Designer
	J. Ensley
	Project Architect / Engineer
	J. Ensley
	Drawn By
	C. Yang
	Q.M. Review
	T. Sovel
	Approved
	T. Sovel
	Drawing Scale
	As Noted
Issued fo	r Issue Date
Design Developmer	t 06-19-2020
Bid Package	1 08-14-2020
Did i ackaye	
Addendum No.	
	3 09-08-2020
Addendum No.	3 09-08-2020 2 11-02-2020
Addendum No. : City Engineering Review No. :	3 09-08-2020 2 11-02-2020 1 11-04-2020
Addendum No. City Engineering Review No. Bulletin No.	3 09-08-2020 2 11-02-2020 1 11-04-2020 3 11-18-2020
Addendum No. City Engineering Review No. Bulletin No. City Engineering Review No.	3 09-08-2020 2 11-02-2020 1 11-04-2020 3 11-18-2020

© 2020 INTEGRATED design solutions, LLC IDS Drawing Title

Paving Details and Notes

īDs Project Number

Drawing Number

20111-1000 SDA Project No. NP20062

include the following additional information for each cantilever gate included in the project scope: 24 wide gate opening,

and gate posts. A. The materials used for cantilever gate framing (i.e., uprights, diagonal braces and pickets or pales) shall be manufactured from ASTM B221 aluminum (designation 6063-T-6) with a yield strength of 25,000 PSI, a tensile strength of 30,000 PSI and a standard mill finish. The TransPort® Fast-Trak™ rails shall be manufactured from ASTM B221 aluminum (designation 6063-T-6) with minimum yield strength of 25,000 PSI, a tensile strength of 30,000 PSI and a standard mill finish.

B. Material for diagonal bracing and uprights shall be 2" sq. x ¼" aluminum. The design of the top and bottom enclosed track shall conform to the manufacturers 5" x 2" Fast-Trak system. Material for chain link infill shall be per specification C. Internal roller truck assembly shall be self-aligning swivel ball-and-socket type running on four bearing wheels. Internal roller truck assembly shall be affixed to the hanger bracket by means of a 5/8" diameter industrial-grade rod end/center bolt, with a minimum static load rating of 10,000 pounds. Attachment of the center bolt to the truck body shall be by means of a swivel joint to ensure equivalent and consistent loading on all bearing wheels and internal track surfaces throughout the travel 2.03 FABRICATION

SIDE VIEW

The contractor shall provide all labor, materials, and appurtenances necessary for installation of the industrial cantilever gate

A. Enclosed track, uprights and diagonal bracing shall be pre-drilled and labeled for easy assembly. All components shall be precut to specified lengths.

GATE MOUNTING POST

GATE MOUNTING POST

FENCE MOUNTING POST

B. Top and bottom rail extrusions shall be mechanically fastened to vertical uprights and reinforced with diagonal braces, as C. Color coating is not required. All materials shall be galvanized.

- 125½" MIN.

PART 3 - EXECUTION 3.01 PREPARATION

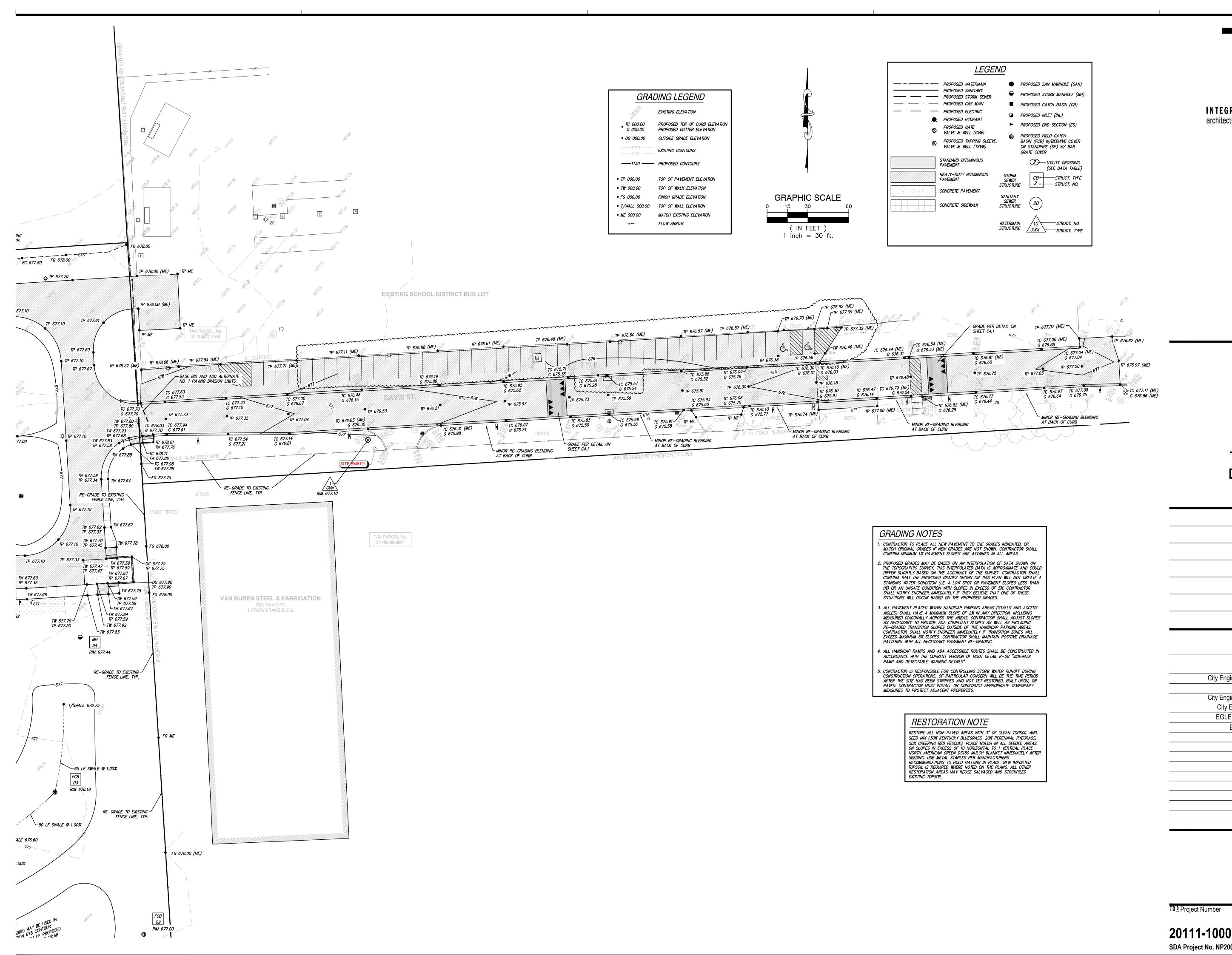
A. All new gate installations shall be laid out by the contractor in accordance with the construction plans. B. All hardware shall be installed in accordance with the Transport installation instructions. Transport cantilever gates shall The contractor shall provide laborers and supervisors who are thoroughly familiar with the type of construction involved and be installed so they comply with current ASTM F2200 & UL325 standards.

C. Gate stops shall be installed on each track in a way that conforms to current ASTM F2200 standards.

shown by engineering analysis to be sufficient in strength for the intended application.

3.02 GATE INSTALLATION Gate post shall be spaced according to specified gate elevation. Posts shall be set in concrete footers having a minimum depth of 48" with a minimum diameter of 12" (Note: In some cases, local restrictions of freezing weather conditions may require a greater depth). The "Earthwork" and "Concrete" sections of this specification shall govern material requirements for the concrete footer. Posts setting by other methods such as plated posts or grouted core-drilled footers are permissible only if

The contractor shall clean the jobsite of excess materials; post-hole excavations shall be scattered uniformly away from posts.



INTEGRATED design solutions architecture engineering interiors & technology

1441 west long lake, suite 200 troy, michigan 48098

5211 cascade road SE, suite 300 grand rapids, michigan 49546 248.823.2100 www.ids-michigan.com

CIVIL ENGINEER SPALDING DeDECKER 905 south blvd. E rochester hills, michigan 48307

800.598.1600 www.sda-eng.com STRUCTURAL ENGINEER

SDI Structures 275 east liberty ann arbor, michigan 48104 734.213.6091 www.sdistructures.com



Van Buren Public Schools

The Early Childhood **Development Center**

Belleville, MI 48111

Project Administrator

	V. Grant
	Project Designer
	J. Ensley
	Project Architect / Engineer
	J. Ensley
	Drawn By
	C. Yang
	Q.M. Review
	T. Sovel
	Approved T. Sovel
	Drawing Scale
	As Noted
Issued for	Issue Date
Design Development	06-19-2020
Bid Package 1	08-14-2020
Addendum No. 3	09-08-2020
City Engineering Review No. 2	11-02-2020
Bulletin No. 1	11-04-2020
City Engineering Review No. 3	11-18-2020
City Engineering Revisions	12-07-2020
EGLE Water Supply Permit	12-07-2020
Bulletin No. 1 Revised	12-08-2020
Bulletin No. 6	06-16-2021
	_

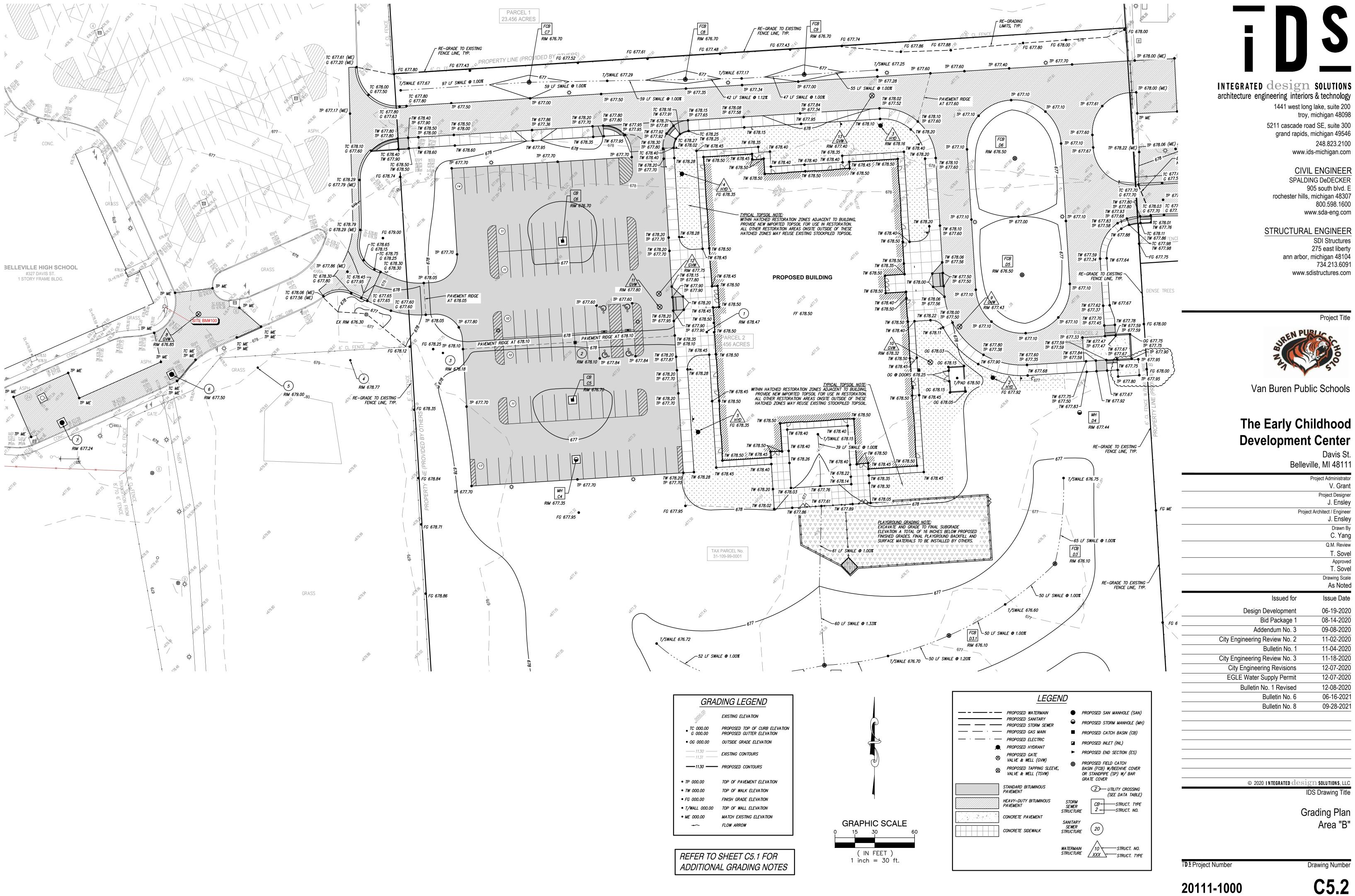
 \odot 2020 Integrated design solutions, LLC IDS Drawing Title

> Grading Plan Area "A"

ī**D** § Project Number

Drawing Number

SDA Project No. NP20062

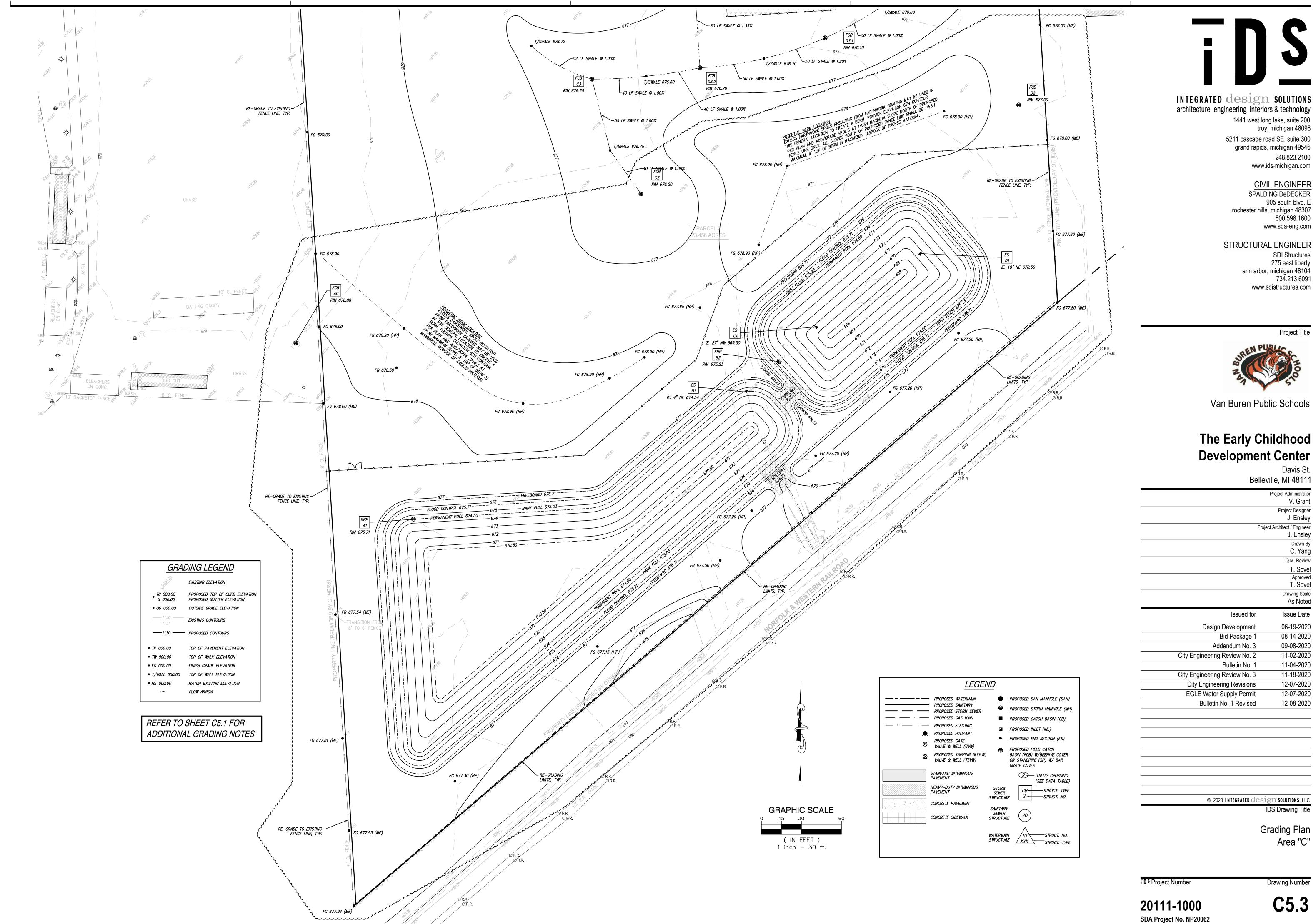


905 south blvd. E 800.598.1600 www.sda-eng.com



	Project Administrator
	V. Grant
	Project Designer
	J. Ensley
	Project Architect / Engineer
	J. Ensley
	Drawn By
	C. Yang
	Q.M. Review
	T. Sovel
	Approved
	T. Sovel
	Drawing Scale
	As Noted
Issued for	Issue Date
Design Development	06-19-2020
Bid Package 1	08-14-2020
Addendum No. 3	09-08-2020
City Engineering Review No. 2	11-02-2020
Bulletin No. 1	11-04-2020
City Engineering Review No. 3	11-18-2020
City Engineering Revisions	12-07-2020
EGLE Water Supply Permit	12-07-2020
Bulletin No. 1 Revised	12-08-2020
Bulletin No. 6	06-16-2021
Bulletin No. 8	09-28-2021

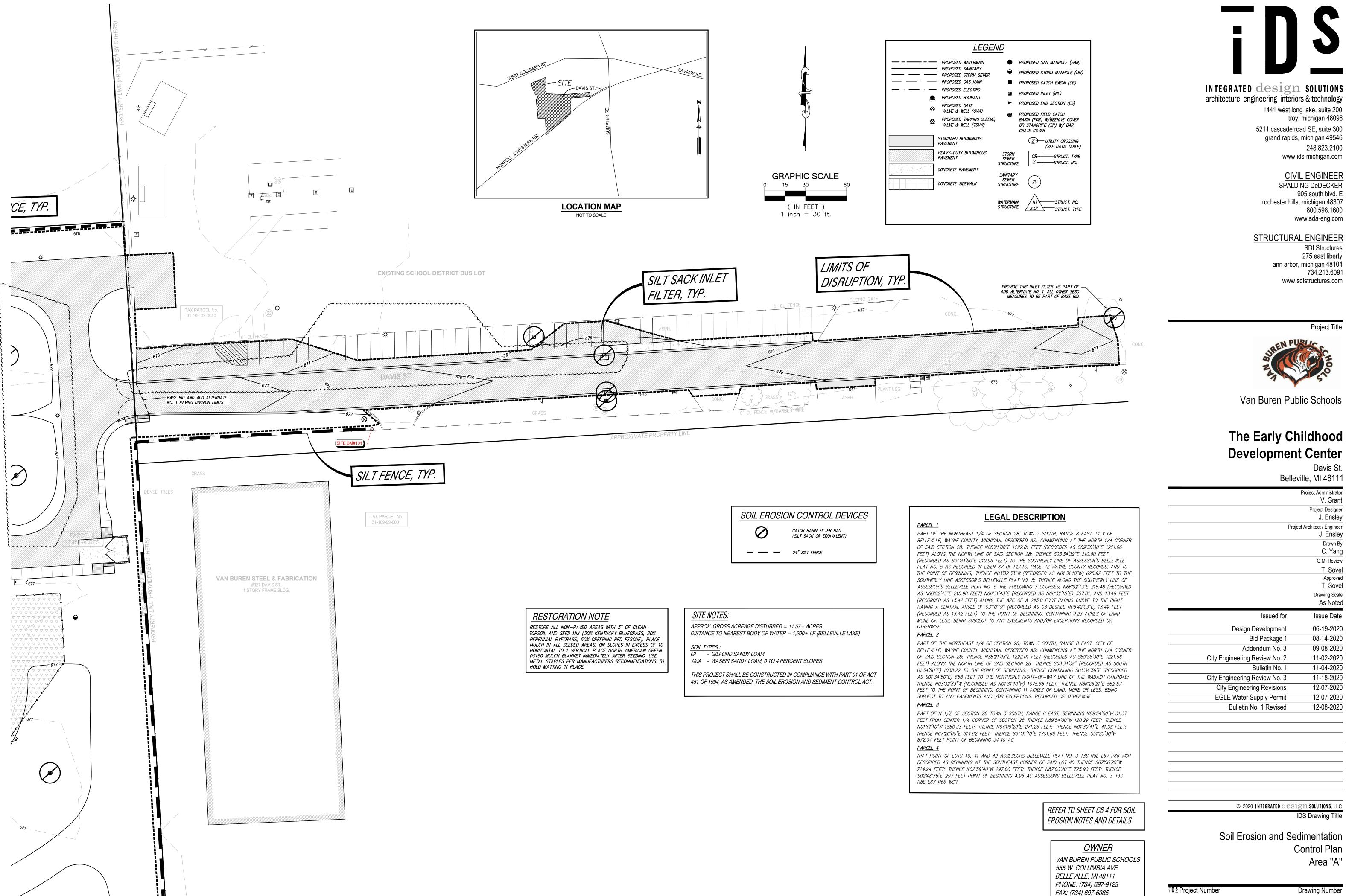
SDA Project No. NP20062



905 south blvd. E www.sda-eng.com

Belleville, MI 48111

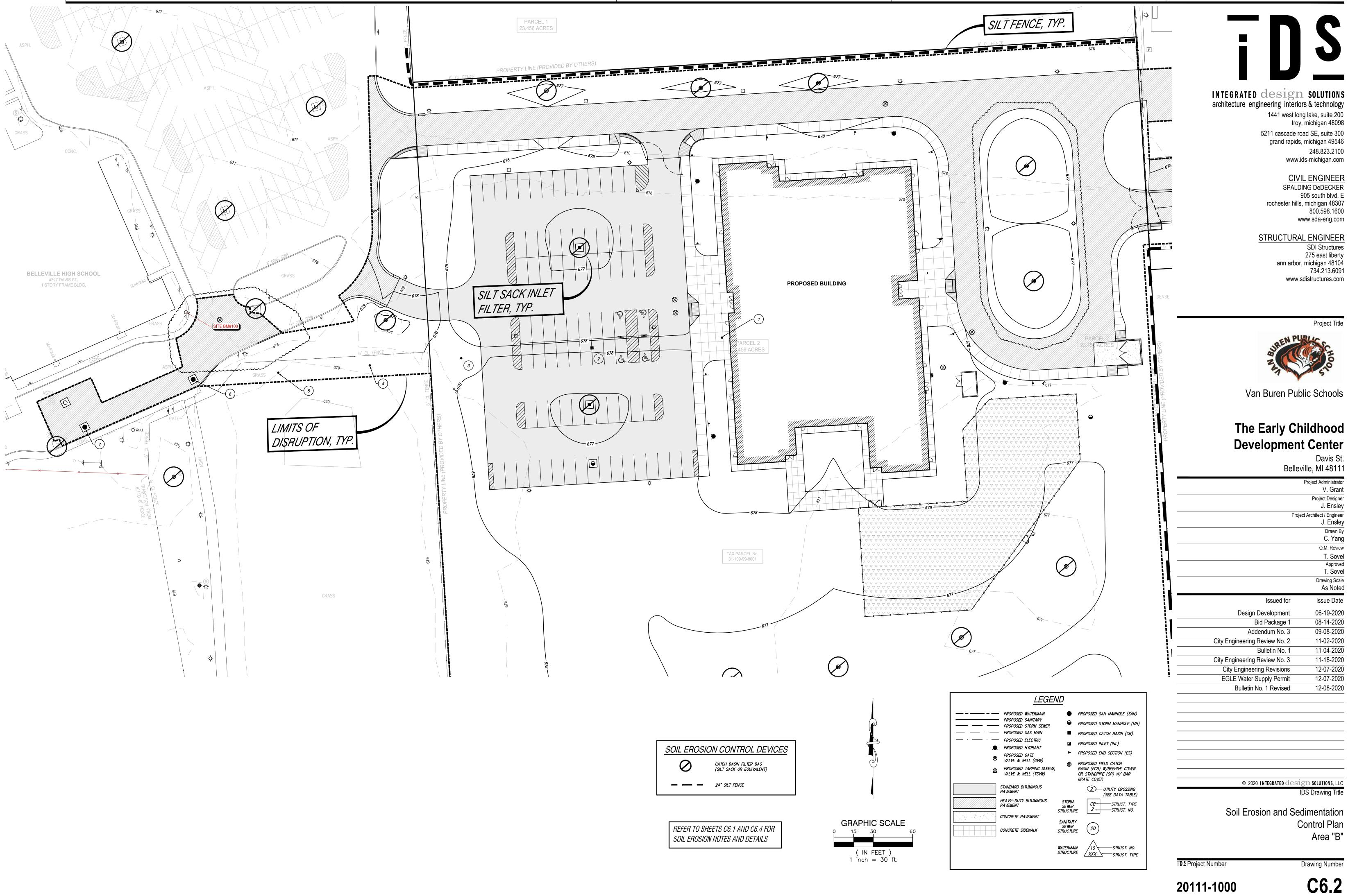
. – .
J. Ensley
ect Architect / Engineer
J. Ensley
Drawn By
C. Yang
Q.M. Review
T. Sovel
Approved
T. Sovel
Drawing Scale
As Noted
Issue Date
06-19-2020
08-14-2020
09-08-2020
11-02-2020
11-04-2020
11-04-2020 11-18-2020
11-18-2020
11-18-2020 12-07-2020
11-18-2020 12-07-2020 12-07-2020
11-18-2020 12-07-2020 12-07-2020





	Project Administrator
	V. Grant
	Project Designer
	J. Ensley
	Project Architect / Engineer
	J. Ensley
	Drawn By
	C. Yang
	Q.M. Review
	T. Sovel
	Approved
	T. Sovel
	Drawing Scale
	As Noted
Issued for	Issue Date
Design Development	06-19-2020
Bid Package 1	08-14-2020
Addendum No. 3	09-08-2020
City Engineering Review No. 2	11-02-2020
Bulletin No. 1	11-04-2020
City Engineering Review No. 3	11-18-2020
City Engineering Revisions	12-07-2020
EGLE Water Supply Permit	12-07-2020
Bulletin No. 1 Revised	12-08-2020

ī **D** § Project Number



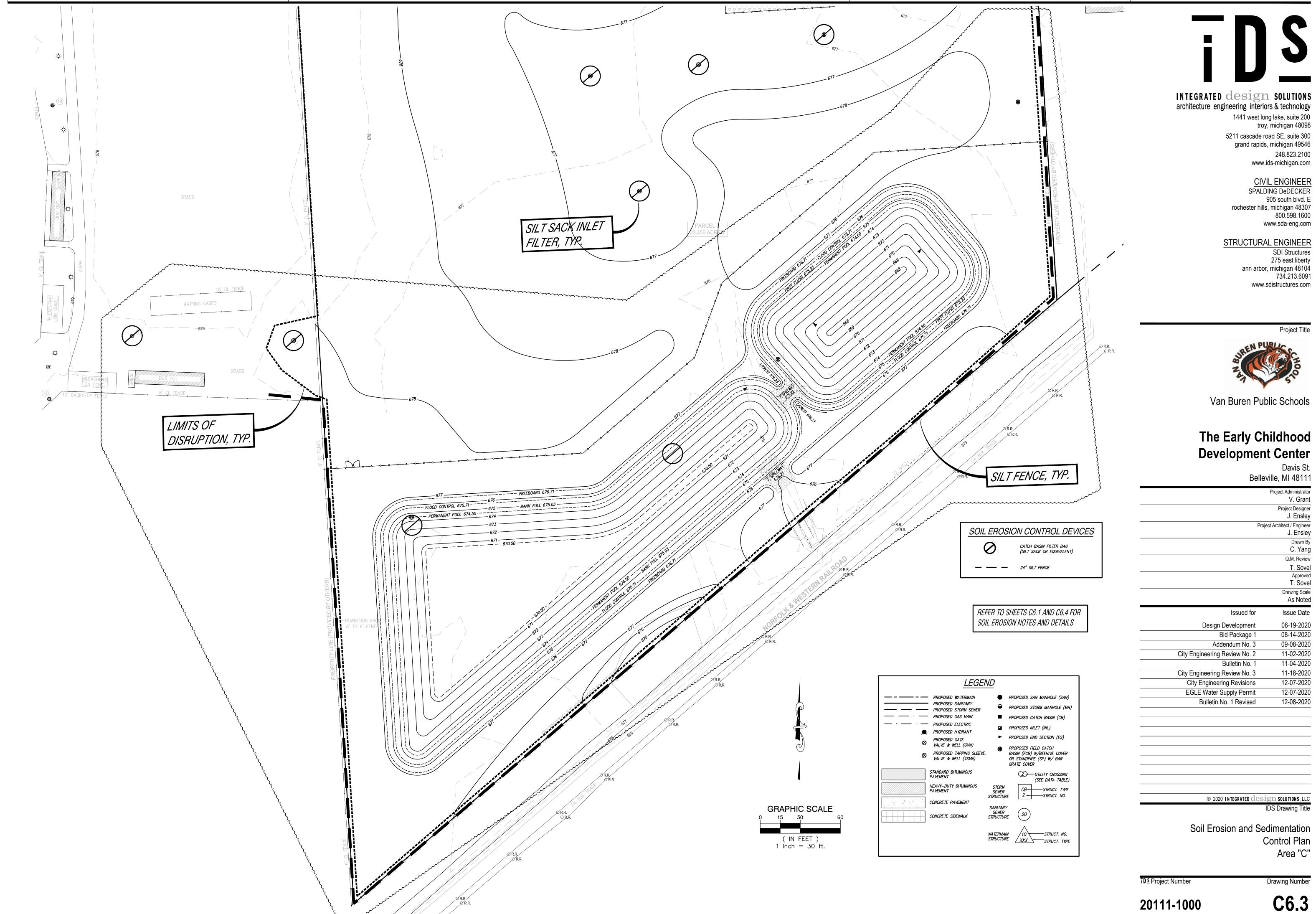
905 south blvd. E www.sda-eng.com



	V. Grant
	Project Designer J. Ensley
	Project Architect / Engineer J. Ensley
	Drawn By C. Yang
	Q.M. Review
	T. Sovel
	Approved T. Sovel
	Drawing Scale As Noted
Issued for	Issue Date
Issued for Design Development	
	06-19-2020
Design Development	06-19-2020 08-14-2020
Design Development Bid Package 1	06-19-2020 08-14-2020 09-08-2020
Design Development Bid Package 1 Addendum No. 3	06-19-2020 08-14-2020 09-08-2020 11-02-2020
Design Development Bid Package 1 Addendum No. 3 City Engineering Review No. 2	06-19-2020 08-14-2020 09-08-2020 11-02-2020 11-04-2020
Design Development Bid Package 1 Addendum No. 3 City Engineering Review No. 2 Bulletin No. 1	06-19-2020 08-14-2020 09-08-2020 11-02-2020 11-04-2020 11-18-2020
Design Development Bid Package 1 Addendum No. 3 City Engineering Review No. 2 Bulletin No. 1 City Engineering Review No. 3	06-19-2020 08-14-2020 09-08-2020 11-02-2020 11-04-2020 11-18-2020 12-07-2020
Design Development Bid Package 1 Addendum No. 3 City Engineering Review No. 2 Bulletin No. 1 City Engineering Review No. 3 City Engineering Revisions	06-19-2020 08-14-2020 09-08-2020 11-02-2020 11-04-2020 11-18-2020 12-07-2020

Control Plan

SDA Project No. NP20062



CIVIL ENGINEER SPALDING DeDECKER

905 south blvd. E www.sda-eng.com

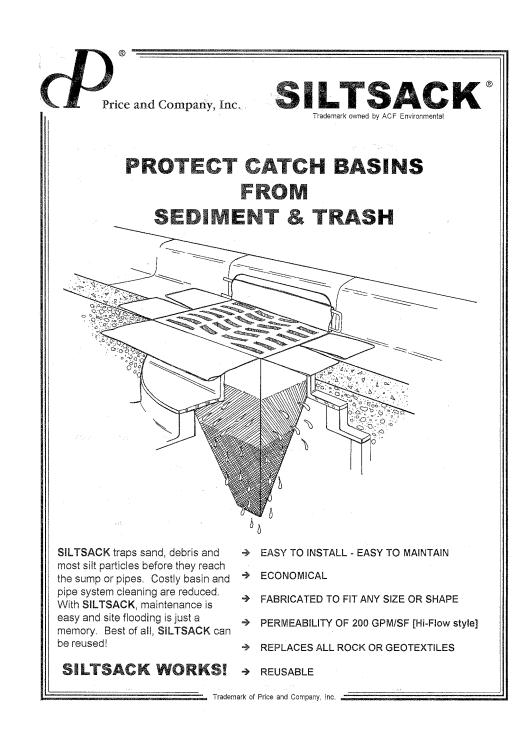
SDI Structures

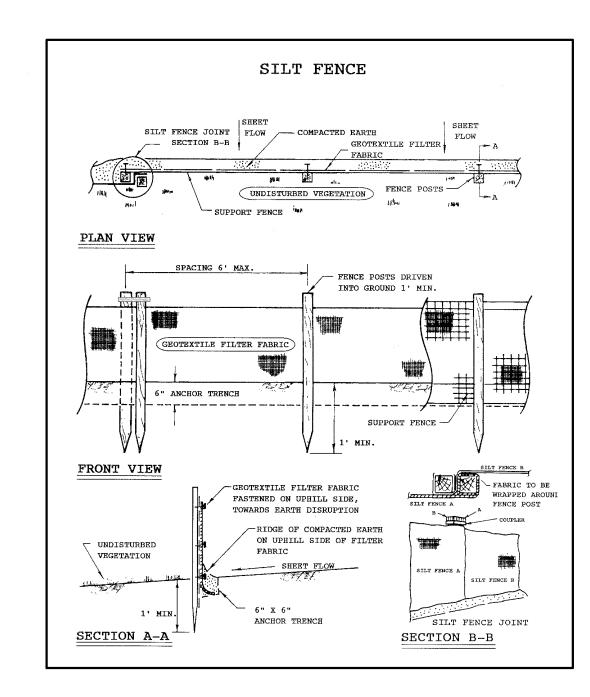


Project Designer
, ,
J. Ensley
ect Architect / Engineer
J. Ensley
Drawn By
C. Yang
Q.M. Review
T. Sovel
Approved
T. Sovel
Drawing Scale
As Noted
Issue Date
00.40.0000
06-19-2020
06-19-2020
08-14-2020
08-14-2020 09-08-2020
08-14-2020 09-08-2020 11-02-2020
08-14-2020 09-08-2020 11-02-2020 11-04-2020
08-14-2020 09-08-2020 11-02-2020 11-04-2020 11-18-2020
08-14-2020 09-08-2020 11-02-2020 11-04-2020 11-18-2020 12-07-2020
08-14-2020 09-08-2020 11-02-2020 11-04-2020 11-18-2020 12-07-2020

Control Plan

SDA Project No. NP20062





SOIL EROSION/SEDIMENTATION CONTROL NOTES

- ALL EROSION AND SEDIMENT CONTROL WORK SHALL CONFORM TO THE STANDARDS AND SPECIFICATIONS OF THE CITY OF BELLEVILLE. 2. DAILY INSPECTIONS SHALL BE MADE BY THE CONTRACTOR TO DETERMINE EFFECTIVENESS OF EROSION AND SEDIMENTATION CONTROL DEVICES, AND ANY NECESSARY REPAIRS SHALL BE PERFORMED WITHOUT DELAY.
- EROSION AND ANY SEDIMENT FROM WORK ON THIS SITE SHALL BE CONTAINED ON THE SITE AND NOT ALLOWED TO COLLECT ON ANY OFF-SITE AREAS OR IN WATER WAYS. WATERWAYS INCLUDE BOTH NATURAL AND MANMADE OPEN DITCHES, STREAMS, STORM DRAINS,
- P. EROSION AND SEDIMENT CONTROL DEVICES ARE TO BE PLACED PRIOR TO OR AS THE FIRST STEP IN CONSTRUCTION; SEDIMENT CONTROL PRACTICES WILL BE APPLIED AS A PERIMETER DEFENSE AGAINST ANY TRANSPORTING OF SILT OFF THE SITE.
- CONTRACTOR SHALL APPLY TEMPORARY EROSION AND SEDIMENTATION CONTROL DEVICES AS REQUIRED AND AS DIRECTED ON THESE PLANS. HE SHALL REMOVE TEMPORARY DEVICES AS SOON AS PERMANENT STABILIZATION OF SLOPES, DITCHES, AND OTHER EARTH CHANGES HAVE BEEN ACCOMPLISHED AND APPROVED BY THE CITY OF BELLEVILLE.
- DEBRIS FROM PROJECT WILL BE LEFT ON THE SITE BY DELIVERY OR CONSTRUCTION VEHICLES THROUGH THE USE OF CLEAN STONE EXITS. SHOULD THE STONE BECOME LESS EFFECTIVE IT WILL BE REPLACED. ALL CONSTRUCTION TRAFFIC WILL USE THE CLEAN STONE EXIT.
- . DUST CONTROL WILL BE EXERCISED AT ALL TIMES WITHIN THE PROJECT BY THE CONTRACTORS. SPRINKLING TANK TRUCKS WILL BE AVAILABLE AT ALL TIMES TO BE USED ON HAUL ROUTES OR OTHER PLACES WHERE DUST BECOMES A PROBLEM.
- 3. IMMEDIATELY AFTER SEEDING, MULCH ALL SEEDED AREAS WITH UNWEATHERED SMALL GRAIN STRAW OR HAY. SPREAD UNIFORMLY AT A RATE OF 1 1/2 TO 2 TONS PER ACRE OR 0.10 POUNDS PER SQUARE FEET. ANCHOR MULCH WITH DISC TYPE MULCH ANCHORING
- ALL MUD, DIRT, AND DEBRIS TRACKED ONTO EXISTING ROADS FROM THIS SITE SHALL BE PROMPTLY REMOVED BY THE CONTRACTOR OR BUILDER. ALL MUD, DIRT, AND DEBRIS TRACKED OR SPILLED ONTO PAVED SURFACES WITHIN THIS SITE SHALL BE PROMPTLY REMOVED BY THE CONTRACTOR.
- O. PERMANENT SOIL EROSION CONTROL DEVICES FOR ALL SLOPES, CHANNELS, DITCHES OR ANY DISTURBED LAND AREA SHALL BE COMPLETED WITHIN 15 CALENDAR DAYS AFTER FINAL GRADING OR FINAL EARTH CHANGES HAVE BEEN COMPLETED. WHEN IT IS NOT POSSIBLE TO PERMANENTLY STABILIZE A DISTURBED AREA AFTER AN EARTH CHANGE HAS BEEN COMPLETED OR WHERE SIGNIFICANT EARTH CHANGE ACTIVITY CEASES TEMPORARY SOIL EROSION CONTROL DEVICES SHALL BE IMPLEMENTED WITHIN 30 CALENDAR DAYS.
 ALL TEMPORARY SOIL EROSION CONTROL DEVICES SHALL BE MAINTAINED UNTIL PERMANENT SOIL EROSION DEVICES ARE IMPLEMENTED AND/OR ESTABLISHED. ALL PERMANENT SOIL EROSION CONTROL DEVICES WILL BE IMPLEMENTED AND ESTABLISHED BEFORE A CERTIFICATE OF INSURANCE IS ISSUED.
- 1. ALL CONTRACTORS ARE TO KEEP EXCAVATED MATERIAL ON SITE. PARTICULAR CARE SHOULD BE TAKEN WHEN WORKING ALONG THE PERIMETER OF THE SITE. IN NO EVENT SHALL THE WORK AREA EXTEND BEYOND THE LIMITS INDICATED ON THE PLANS.
- 12. THE SOIL EROSION CONTROLS WILL BE MAINTAINED WEEKLY AND AFTER EVERY STORM EVENT BY THE CONTRACTOR.

SOIL EROSION/SEDIMENTATION CONTROL

CONSTRUCTION SEQUENCE

- INSTALL SILT FENCE AROUND DEFINED PERIMETER AND INLET FILTERS IN EXISTING STRUCTURES
- CLEAR, GRUB AND STRIP TOPSOIL IN AREAS OF EARTH DISRUPTION. DEMOLISH EXISTING PAVEMENT.
- COMPLETE LAND BALANCING OPERATIONS.
- INSTALL UNDERGROUND UTILITIES AND PLACE NEW INLET FILTERS WHERE INDICATED.
- INSTALL PROPOSED BUILDING.
- PERFORM FINE GRADING, PAVING OPERATIONS, LANDSCAPING.
- EROSION CONTROL MEASURES ARE NOT TO BE REMOVED UNTIL THE CITY OF BELLEVILLE GRANTS ITS APPROVAL. INLET FILTERS SHALL BE PERIODICALLY INSPECTED AND CLEANED/REPLACED AS NECESSARY.
- ALL EROSION CONTROL MEASURES SHALL BE INSTALLED APPROXIMATELY ACCORDING TO THE FOLLOWING SEQUENCE OF CONSTRUCTION.

PROJECT COMMENCEMENT ON OR ABOUT SEPTEMBER 2020.

- . INSTALL SILT FENCE AND INLET FILTERS AS SHOWN ON PLANS. 1-2 DAYS STRIP AND STOCKPILE TOPSOIL, DEMOLISH PAVEMENT AND ROUGH GRADE SITE. 3-4 WEEKS
- INSTALL UNDERGROUND UTILITIES. 3-4 WEEKS D. CONSTRUCT PROPOSED BUILDING. 48-56 WEEKS FINE GRADE SITE, PAVE, INSTALL LANDSCAPING AND ESTABLISH VEGETATION. 3-4 WEEKS
- CLEAN PAVEMENTS, WALKS, CULVERTS, AND WATERCOURSES OF ALL ACCUMULATED SEDIMENT IN CONJUNCTION WITH REMOVING ALL TEMPORARY DEVICES.

PROJECT COMPLETION ON OR ABOUT DECEMBER 2021.

INTEGRATED design solutions architecture engineering interiors & technology

1441 west long lake, suite 200 troy, michigan 48098 5211 cascade road SE, suite 300

grand rapids, michigan 49546 248.823.2100 www.ids-michigan.com

CIVIL ENGINEER SPALDING DeDECKER

905 south blvd. E rochester hills, michigan 48307 800.598.1600 www.sda-eng.com

STRUCTURAL ENGINEER SDI Structures

275 east liberty ann arbor, michigan 48104 734.213.6091 www.sdistructures.com



Van Buren Public Schools

The Early Childhood **Development Center**

Belleville, MI 48111 Project Administrator

V. Grant

Project Designer J. Ensley Project Architect / Engineer J. Ensley Drawn By C. Yang Q.M. Review T. Sovel Approved T. Sovel Drawing Scale As Noted Issued for Issue Date Design Development Design Development Design Development O6-19-2020 Bid Package 1 Addendum No. 3 O9-08-2020 City Engineering Review No. 2 11-04-2020 City Engineering Review No. 3 11-18-2020 City Engineering Review No. 3 11-18-2020 City Engineering Review No. 3 11-18-2020		
Project Architect / Engineer J. Ensley Drawn By C. Yang Q.M. Review T. Sovel Approved T. Sovel Drawing Scale As Noted Issued for Issue Date Design Development Design Development O6-19-2020 Bid Package 1 Addendum No. 3 O9-08-2020 City Engineering Review No. 2 11-02-2020 Bulletin No. 1 11-04-2020 City Engineering Review No. 3 11-18-2020		Project Designer
J. Ensley Drawn By C. Yang Q.M. Review T. Sovel Approved T. Sovel Drawing Scale As Noted Issued for Issue Date Design Development 06-19-2020 Bid Package 1 08-14-2020 Addendum No. 3 09-08-2020 City Engineering Review No. 2 11-02-2020 Bulletin No. 1 11-04-2020 City Engineering Review No. 3 11-18-2020		J. Ensley
Drawn By C. Yang Q.M. Review T. Sovel Approved T. Sovel Drawing Scale As Noted Issued for Issue Date Design Development 06-19-2020 Bid Package 1 08-14-2020 Addendum No. 3 09-08-2020 City Engineering Review No. 2 11-02-2020 Bulletin No. 1 11-04-2020 City Engineering Review No. 3 11-18-2020		Project Architect / Engineer
C. Yang Q.M. Review T. Sovel Approved T. Sovel Drawing Scale As Noted Issued for Issue Date Design Development 06-19-2020 Bid Package 1 08-14-2020 Addendum No. 3 09-08-2020 City Engineering Review No. 2 11-02-2020 Bulletin No. 1 11-04-2020 City Engineering Review No. 3 11-18-2020		J. Ensley
Q.M. Review T. Sovel Approved T. Sovel Drawing Scale As Noted Issued for Issue Date Design Development 06-19-2020 Bid Package 1 08-14-2020 Addendum No. 3 09-08-2020 City Engineering Review No. 2 11-02-2020 Bulletin No. 1 11-04-2020 City Engineering Review No. 3 11-18-2020		•
T. Sovel		C. Yang
Approved T. Sovel Drawing Scale As Noted Issued for Issue Date Design Development 06-19-2020 Bid Package 1 08-14-2020 Addendum No. 3 09-08-2020 City Engineering Review No. 2 11-02-2020 Bulletin No. 1 11-04-2020 City Engineering Review No. 3 11-18-2020		Q.M. Review
T. Sovel Drawing Scale As Noted Issued for Issue Date Design Development 06-19-2020 Bid Package 1 08-14-2020 Addendum No. 3 09-08-2020 City Engineering Review No. 2 11-02-2020 Bulletin No. 1 11-04-2020 City Engineering Review No. 3 11-18-2020		T. Sovel
Drawing Scale As Noted		
As Noted Issued for Issue Date Design Development 06-19-2020 Bid Package 1 08-14-2020 Addendum No. 3 09-08-2020 City Engineering Review No. 2 11-02-2020 Bulletin No. 1 11-04-2020 City Engineering Review No. 3 11-18-2020		
Issued for Issue Date Design Development 06-19-2020 Bid Package 1 08-14-2020 Addendum No. 3 09-08-2020 City Engineering Review No. 2 11-02-2020 Bulletin No. 1 11-04-2020 City Engineering Review No. 3 11-18-2020		~
Design Development 06-19-2020 Bid Package 1 08-14-2020 Addendum No. 3 09-08-2020 City Engineering Review No. 2 11-02-2020 Bulletin No. 1 11-04-2020 City Engineering Review No. 3 11-18-2020		As Noted
Bid Package 1 08-14-2020 Addendum No. 3 09-08-2020 City Engineering Review No. 2 11-02-2020 Bulletin No. 1 11-04-2020 City Engineering Review No. 3 11-18-2020	Issued f	or Issue Date
Addendum No. 3 09-08-2020 City Engineering Review No. 2 11-02-2020 Bulletin No. 1 11-04-2020 City Engineering Review No. 3 11-18-2020	Design Developme	nt 06-19-2020
City Engineering Review No. 2 11-02-2020 Bulletin No. 1 11-04-2020 City Engineering Review No. 3 11-18-2020	Bid Package	1 08-14-2020
Bulletin No. 1 11-04-2020 City Engineering Review No. 3 11-18-2020	Addendum No.	3 09-08-2020
City Engineering Review No. 3 11-18-2020	City Engineering Review No.	2 11-02-2020
City Engineering Revisions 12-07-2020	, , ,	1 11-04-2020
	Bulletin No.	
	Bulletin No. City Engineering Review No.	3 11-18-2020
	Bulletin No. City Engineering Review No.	3 11-18-2020

© 2020 INTEGRATED design solutions, LLC IDS Drawing Title

Soil Erosion and Sedimentation Control **Details and Notes**

ī**D** § Project Number

Drawing Number C6.4

CITY OF BELLEVILLE STANDARD GENERAL NOTES

- 1. All workmanship and materials shall be in accordance with the current standards and specifications of the City of Belleville.
- 2. The contractor and his subcontractors shall attend a pre-construction meeting at a time and place arranged by the engineer in which various utility companies and governmental agency representatives will be present.
- 3. After a pre-construction meeting is held, the contractor shall notify Hennessev Engineers, Inc. a minimum of 3 working days prior to the start of construction.
- 4. Contractor shall notify Miss Dig for existing utility stake out 3 working days in advance of construction. The project will be billed for excessive stakeouts.
- 5. Locations and elevations of existing underground utilities as shown on the plans are approximate. No guarantee is either expressed or implied as to the completeness or accuracy thereof. The contractor shall be exclusively responsible for determining and verifying the location, depth, and elevation of existing utilities, and proposed utilities crossing the construction area prior to start of construction. Contractor shall notify engineer if any conflicts are apparent or if locations and depth differ significantly from the plans.
- 6. All elevations refer to current N.G.V.D. datum.
- 7. All properties or facilities in the surrounding areas, public or private, destroyed or otherwise damaged by the contractors operations shall be replaced or repaired to the satisfaction of the authority having jurisdiction of the property or facility by the contractor at his own expense.
- 8. Contractor shall provide and maintain all necessary barricades and traffic control devices required by the current standards and specifications of the City of Belleville, other agencies having jurisdiction, and the Michigan Manual of Uniform Traffic Control Devices (MMUTCD).
- 9. All required soil erosion and sedimentation control measures must be in place prior to starting construction, including stripping and grubbing.
- 10. All trenches under or within three feet of existing or proposed pavement, curb, sidewalks, and driveways shall be backfilled with 21A crushed limestone (Trench B) and compacted in one foot layers to a minimum 95 percent maximum unit weight.
- 11. All trenches within or parallel and adjacent to right-of-way, except where 21A crushed limestone (Trench B) backfill is required, shall be backfilled with suitable excavated material (excluding blue clay) compacted in one foot layers to a minimum of 90 percent maximum unit weight. This trench shall be designated Trench "A".
- 12. Four inches of compacted approved bedding shall be placed under all utilities and to one foot above the top of the pipe.
- 13. A recording detector tape, approved by the engineer, shall be installed two feet above the top of all non-metal sewer and water lines.
- 14. All public improvements and private improvements shall be field staked under the supervision of a professional engineer or land surveyor licensed to practice in the State of Michigan. If Hennessey Engineers, Inc. is not performing the field staking, a copy of the surveying cut sheet must be sent to Hennessey Engineers, Inc., one (1) working day prior to any construction starting.
- 15. All work within Wayne County and State of Michigan right-of-way shall be in accordance with their specifications. A copy of the required permit(s) must be on file with Hennessey Engineers and the City of Belleville prior to any construction starting.
- 16. All disturbed lawn areas shall be restored with 3 inches of topsoil and Class "A" sod. The Contractor will be responsible for watering and maintaining the sod until it is firmly knitted in place and in a vigorous growing condition. Areas designated by the City Engineer as non-lawn areas, but grass areas, shall have placed 3 inches of topsoil, a chemical fertilizer, a Michigan Department of Environmental Quality roadside mixture of seed sowed, and a mulch applied in accordance with City of Woodhaven Standard Specifications.
- 17. For isolated road cuts, all trenches shall be backfilled with "K-Krete" or an approved equal flowable fill. This shall be designated as Trench "C".

CITY OF BELLEVILLE STANDARD WATERMAIN NOTES

- 1. All construction shall conform to current Belleville Detailed Specifications for watermain and any other agency having jurisdiction of the construction
- 2. Slip—on joints may be used except at tees, bends, and hydrants, where mechanical joints will be used.
- 3. All watermain shall be placed on approved bedding as shown on the City Belleville Standard Watermain Details.
- 4. All watermains shall be installed a minimum of 5.5 feet below proposed finished grade. Seven (7) foot minimums when in County Right-of-Way. When a watermain must dip to pass under a storm sewer or sanitary sewer, the sections which are deeper than normal shall have a minimum of 18" clearance between utilities and be in accordance with the standard
- 5. No pipe shall be deflected more than 3 degrees. Where deflections greater than 3 degrees are required, bends, vertical or horizontal, will be required in accordance with the details.
- 6. A thrust block is required on the opposite side of each hydrant, tee, cap and bend.
- 7. Connections to existing watermains shall not be made until after hydrostatic/bacteriological tests have been successfully completed and reviewed by the Engineer.
- 8. The watermain shall be pressure tested at 150 psi for 2 hours with an allowable leakage of 1 gallon per inch diameter per mile of pipe in the 2 hour period. Test sections shall not exceed 1,000 feet. Testing against valves is not allowed.
- 9. Fire hydrants shall be East Jordan Iron Works Water Master 5BR250 equipped with 2- 4.5" pumper nozzles in commercial, industrial, and residential areas. Opening shall be in a counter-clockwise direction. Threads shall be Detroit Standard Threads with 1-1/8 pentagonal nut.
- 10. All hydrants shall be properly orientated and approved by the Department of Public Services prior to the pressure test.
- 11. All hydrants not in service shall be covered with black plastic until such time as they are put in service or removed.
- 12. All gate valves shall be left hand open E.J.I.W. Flow Master Resilient
- 13. Water gatewells shall not be located in driveways, sidewalks or streets.
- 14. Gate valves and curb stops shall only be operated by City of Belleville Water/Sewer Department personnel except in an emergency.
- 15. Contractor shall compact <u>all</u> trenches and excavated areas in one—foot lifts by vibratory means during the backfilling operations to the required percent per the City of Belleville Standards.
- 16. The City of Detroit Water and Sewer Department, the City of Belleville, and Hennessey Engineers, Inc. shall be notified at least 72 hours (three (3) working days) prior to any watermain construction.
- 17. All saddles for water services shall be bronze with double stainless steel
- 18. For isolated road cuts, all trenches shall be backfilled with "K-Krete" or an approved equal flowable fill. This shall be designated as Trench "C".

STANDARD STORM SEWER NOTES

- 1. All construction shall conform to current City of Belleville Standard Specifications for Storm Sewer and any other agency having jurisdiction of the construction area.
- 2. All road catchbasins and inlets shall have underdrains as shown on the City of Belleville Standard Storm Sewer Details. All parking lot catchbasins and inlets shall have underdrains as shown on the City of Belleville Standard Storm Sewer Details.
- 3. All storm sewer shall be placed on approved bedding as shown on the City of Belleville Standard Storm Sewer Details.
- 4. Contractor shall compact <u>all</u> trenches and excavated areas in one-foot lifts by vibratory means during backfilling operations to the required percent per the City of Belleville Standards.
- 5. For isolated road cuts, all trenches shall be backfilled with "K-Krete" or an approved equal flowable fill. This shall be designated as Trench "C".

STANDARD SANITARY SEWER NOTES

- 1. All construction shall conform to current City of Belleville Standard and General Specifications for Sanitary Sewer and other agencies having iurisdiction over the construction area.
- 2. All sanitary sewer wye openings shall contain factory installed premium
- 3. No connection receiving stormwater, surface water, or groundwater shall be made to the public sanitary sewers or the building service lead.
- 4. Infiltration for any section of sewer between manholes shall not exceed 100 gallons per inch diameter, per mile, per 24 hours.
- 5. Each wye or end of building lead to be capped shall have a cap with the same type of material as the lead and shall have a solvent weld joint. Cleanouts shall have J.R. Smith # 4240U4 or approved equal covers with 24"x24" x6" thick concrete pad surround. See detail on sheet S.D.1.
- 6. Sanitary sewer leads shall be installed to a minimum of 1 foot past the right-of-way or easement line as shown on these plans. Risers are required where a sanitary sewer is over 10' in depth. Risers shall be installed to a depth of 10 feet.
- 7. A bulkhead shall be installed at each outlet to an existing system and shall not be removed until the new sewer system has been accepted by the City of Belleville.
- 8. All sewers shall be subjected to an air filtration, or exfiltration test or a combination of same prior to acceptance. All sewers over 24 inch diameter shall be subjected to infiltration tests. All sewers of 24 inch diameter of smaller, where the groundwater level above the top of the sewer is over 2 feet, shall be subjected to infiltration tests. All sewers of 24" diameter or less, where the groundwater level above the top of the sewer is 2 feet or less, shall be subjected to air tests or exfiltration
- 9. All sewers shall be televised by the contractor, at no additional cost to the City of Belleville, with test results approved and the city provided a copy of the video tape of the sewer prior to placing the sewer in service.
- 10. Manhole casting shall be watertight, bolt down type with an approved external chimney seal.
- 11. Contractor shall notify Wayne County and the City of Belleville Water/Sewer Department at least 48 hours two (2) working days prior to start of construction.
- 12. Differential excavation around the existing manhole shall not exceed 6
- 13. All stubs shall have a water and air—tight bulkhead approved by the
- 14. Wherever existing manholes or sewer pipe are to be tapped, core manhole with a coring machine and install a rubber boot with stainless steel bands. Use Kor-N-Seal with Korband external contraction bands or approved equal.
- 15. All manhole steps shall be placed toward the property lines unless otherwise noted.
- 16. No footing drains or downspouts shall be connected to the building
- 17. Deflection Tests:
- a. Deflection tests shall be performed on all flexible pipe. The test shall be conducted after the final backfill has been in place at least 30 days.
- b. No pipe shall exceed a deflection of 5%
- c. If the deflection test is to be run using a rigid ball or mandrel, it shall have a diameter equal to 95% of the inside diameter of the pipe. The test shall be performed without mechanical pulling devices.
- 18. Contractor shall compact <u>all</u> trenches and excavated area in one—foot lifts by vibratory means during backfilling operations to the required percent per the City of Belleville Standards
- 19. For isolated road cuts, all trenches shall be backfilled with "K-Krete" or an approved equal flowable fill. This shall be designated as Trench "C".

STANDARD PAVING AND PAVEMENT REPLACEMENT NOTES

- 1. All construction shall conform to current City of Belleville Standards and General Specifications for Pavina and any other gaency having jurisdiction over the construction area.
- 2. Compaction of all pavement subbase shall be to a minimum of 95% maximum unit weight prior to placement of pavement. No paving shall take place prior to the successful testing of the compaction of the backfill and/or subbase.
- 3. All fill required to meet final subgrade elevations shall be select material approved by the City Engineer free from organic material or extraneous matter, and shall be placed in layers not exceeding 6 inches and compacted to a minimum of 95% of its maximum unit weight. The subgrade must be proof rolled prior to the placement on pavement base.
- 4. All radii at intersections are to be 25 feet unless otherwise noted.
- 5. The contractor shall submit, prior to the pre-construction meeting, a concrete and bituminous mix design from the supplier and a 21A crushed limestone sample for approval by the city engineer.
- 6. New pavement shall be as described in the plans and specifications.
- 7. All curb and gutter, new or replacement, shall be placed on a minimum of 4 inch 21A crushed limestone base. The base shall be placed one foot behind the back of curb.
- 8. Existing concrete pavement and curb sections shall be saw cut the full depth of the pavement prior to their removal.
- 9. Any excavation necessary to install replacement pavement at the proposed grades shall be performed by the contractor.
- 10. If the pavement is being replaced, the minimum thickness of replacement concrete allowed for roadways is 8 inches, and the minimum thickness of asphalt pavement for roadways is 5 inches.
- 11. If the drive approach or sidewalk located in the approach is being replaced, the minimum thickness of replacement concrete is 6 inches. No asphalt drive approaches are allowed. If the sidewalk is located outside the approach, the minimum thickness of concrete allowed is 4 inches. New driveway pavement shall be a minimum of 6" thick concrete with thickened edges unless otherwise noted.
- 12. All replacement pavement for roadways be placed on 21A crushed limestone per the City of Belleville standard specifications.
- 13. If an asphalt cap is required to match the existing payement, the thickness of the existing asphalt shall be matched. This cap shall be placed on a minimum of 8 inches of replacement concrete.
- 14. Before placing the replacement pavement, the contractor shall install 1/2" diameter hook bolts with Philip Red Heads into the existing pavement. These bolts shall be install at 40 inches on center.
- 15. 21A crushed limestone, compacted in place to a minimum of 95 percent maximum unit weight shall be placed where additional base is required to meet proposed pavement grades.
- 16. The contractor shall remove unsatisfactory subgrade as determined by the engineer and replace the unsatisfactory subgrade with 21A crushed limestone compacted to a minimum of 95 percent maximum unit weight.
- 17. All joints in concrete pavement areas, including curb and gutter, shall be sealed with a hot-poured, elastic-type compound, approved by the city engineer.
- 18. Contractor shall protect all trees and shall be responsible for replacing any trees damaged by his operations.
- 19. Surface restoration shall include replacement of existing sod between the sidewalk and curb. Three inches of topsoil shall be placed prior to placing Class "A" sod. Contractor shall keep the sodded area continuously moist until a good growth is indicated.
- 20. It shall be the responsibility of the paving contractor to adjust the top of all existing structures (sewers, manholes, catchbasins, inlets, gatewells, etc.. except hydrants) within the street right-of-way or within 10 feet adjacent to the street right-of-way to the final grade as required by the City of Belleville. All such adjustments will be incidental to the paving
- 21. The contractor shall install all required permanent pavement striping upon completion of the pavement replacement. This work shall be performed in accordance with the "Michigan Manual of Uniform Traffic Control Devices" (MMUTCD) and as directed by the Engineer.
- 22. All existing sidewalk that is cracked, uneven, and/or creates a trip hazard shall be removed and replaced as determined by the Engineer and Department of Public Services.

DRAWN BY: ESCHECKED BY:

DESIGNED BY: ES

NTS

APPROVED BY:

REVISIONS

03/29/05

PER ENGINEER

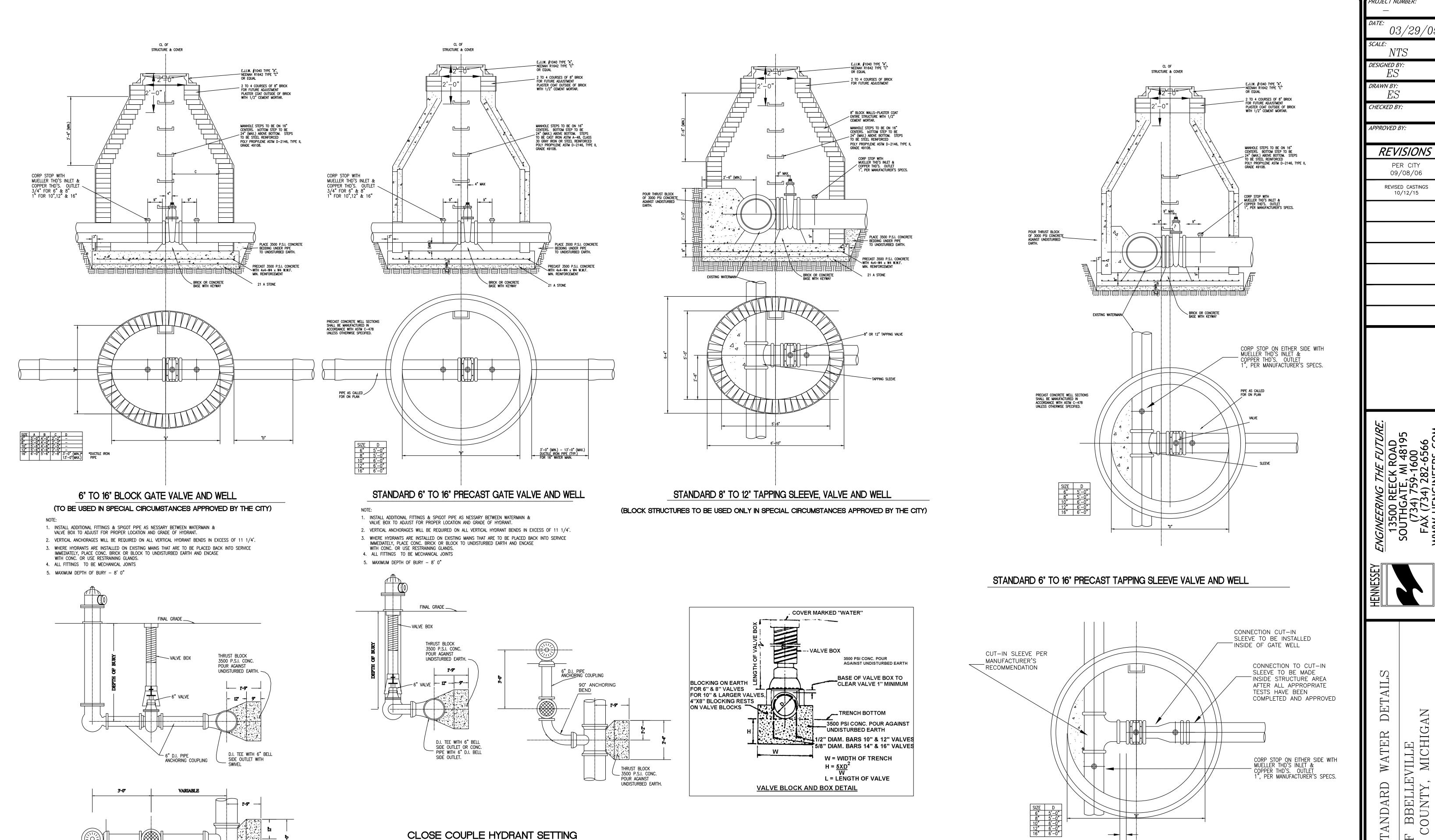
PER CITY

K ROAD MI 48195 -1600 82-6566 IEERS.COM 00 RI THGA 734) (734 HEN



Z HIG, NOTES LLE ARD SELLEV $STAND_{\lambda}$ B. I O 日

SHEET C7.



THRUST BLOCK

_ 3500 P.S.I. CONC. POUR AGAINST UNDISTURBED EARTH.

STANDARD HYDRANT SETTING

MECHANICAL JOINT FITTINGS FOR ALL HYDRANT INSTALLATIONS SHALL BE SWIVEL FITTINGS AS MANUFACTURED BY TYLER PIPE OR APPROVED EQUAL

STANDARD BBELLI CITY WAYI

2' MIN, 20' MAX

CUT-IN SLEEVE, VALVE, AND WELL

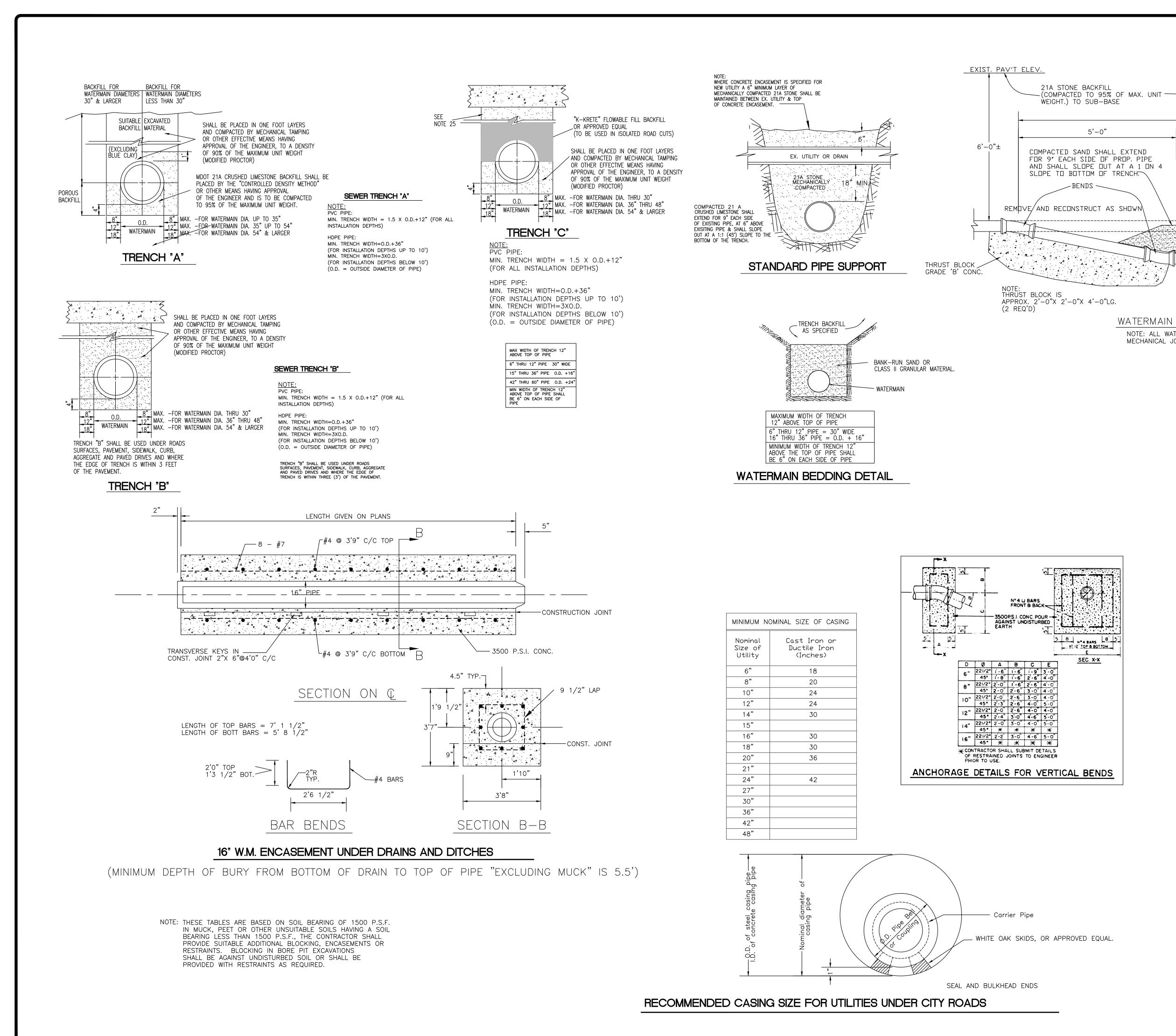
VILLE MICHIGA

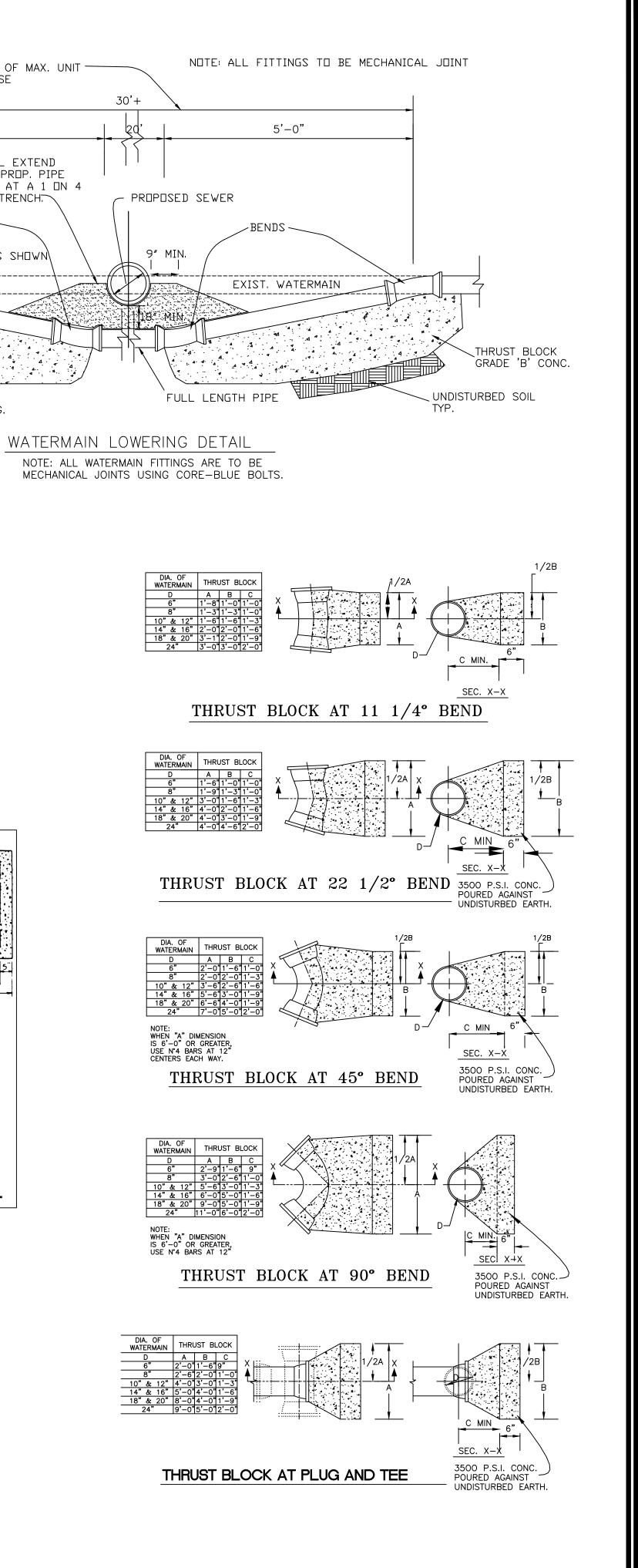
03/29/05

PER CITY 09/08/06

10/12/15

SHEET





DATE: 03/29/05

SCALE: NTS

DESIGNED BY: ES

DRAWN BY: ES

CHECKED BY:

APPROVED BY:

PER CITY 09/08/06

REVISED CASTINGS 10/12/15

ROJECT NUMBER:

13500 REECK ROAD SOUTHGATE, MI 48195 (734) 759-1600 FAX (734) 282-6566

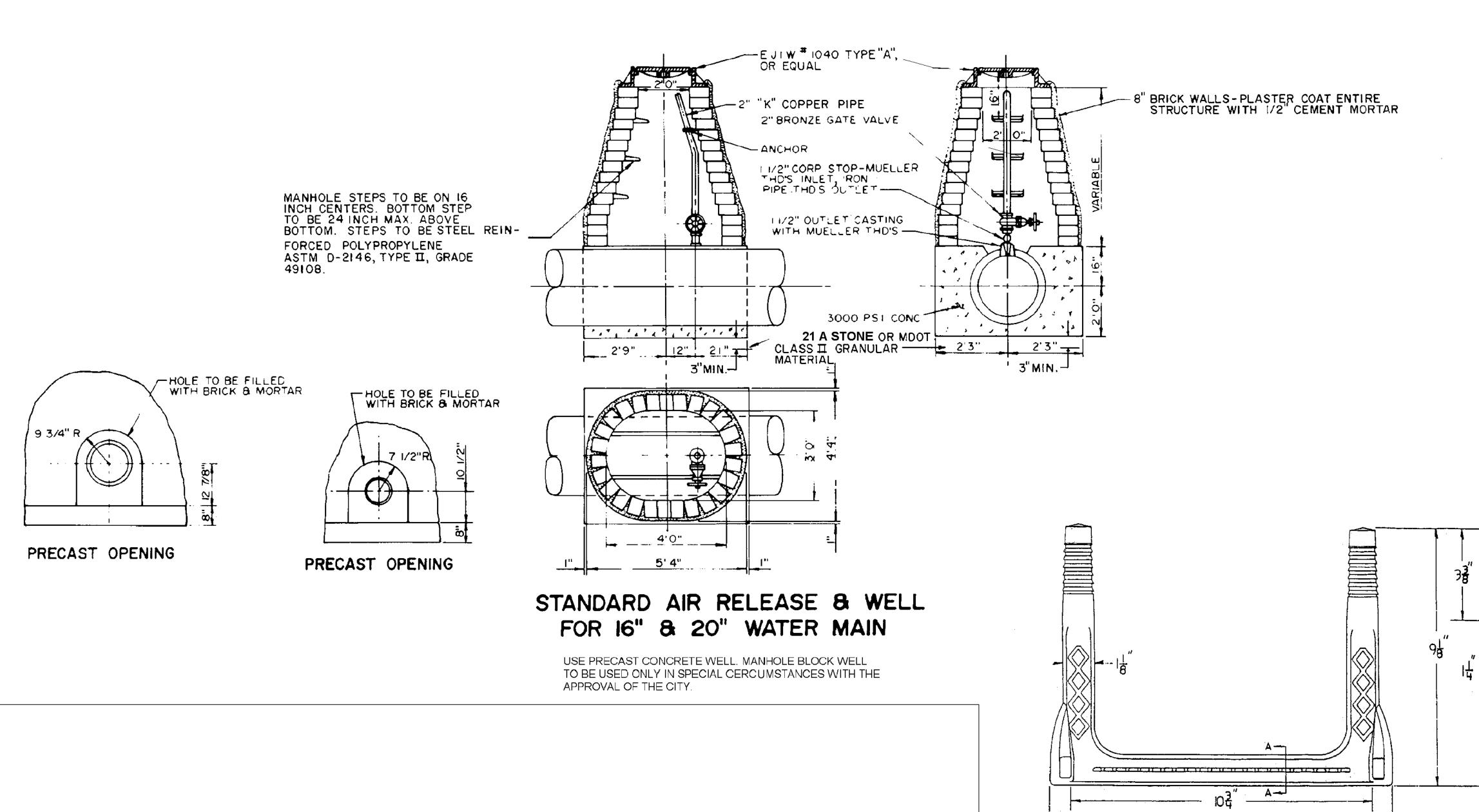
HENNESSE Y

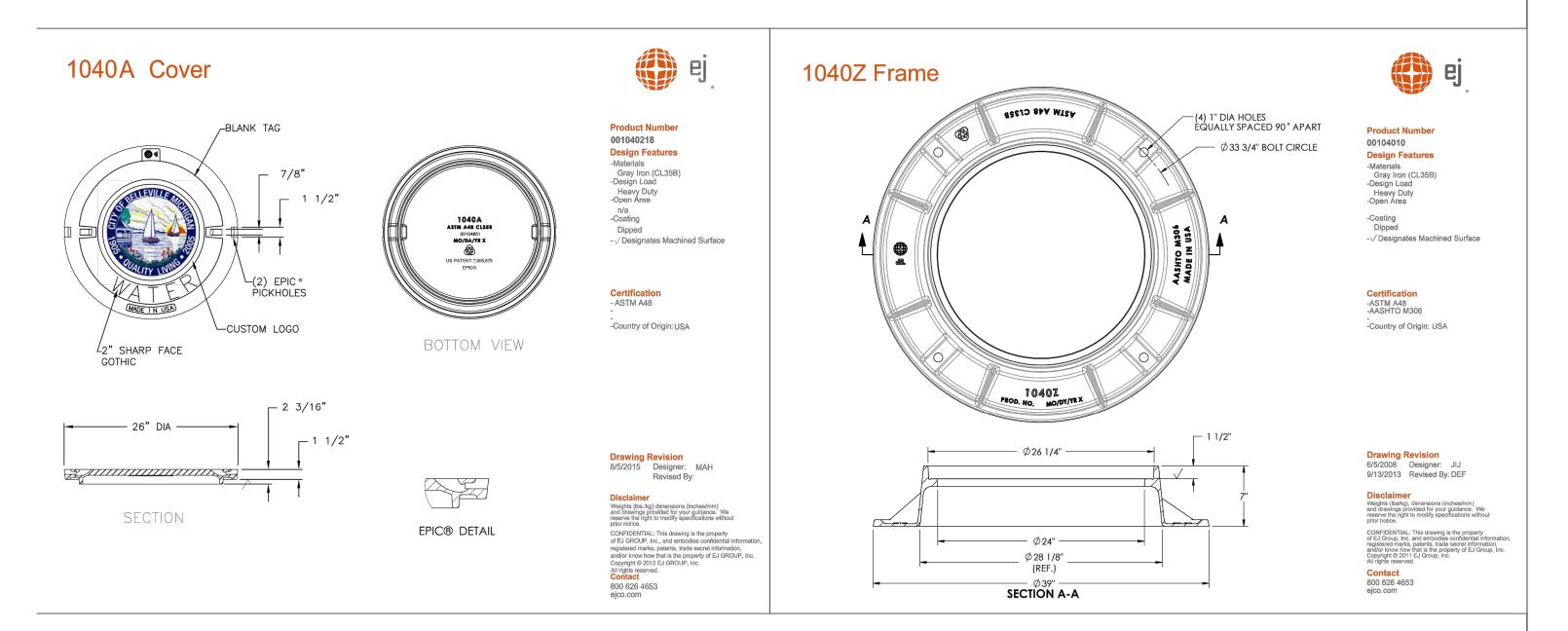
WATER DETAILS

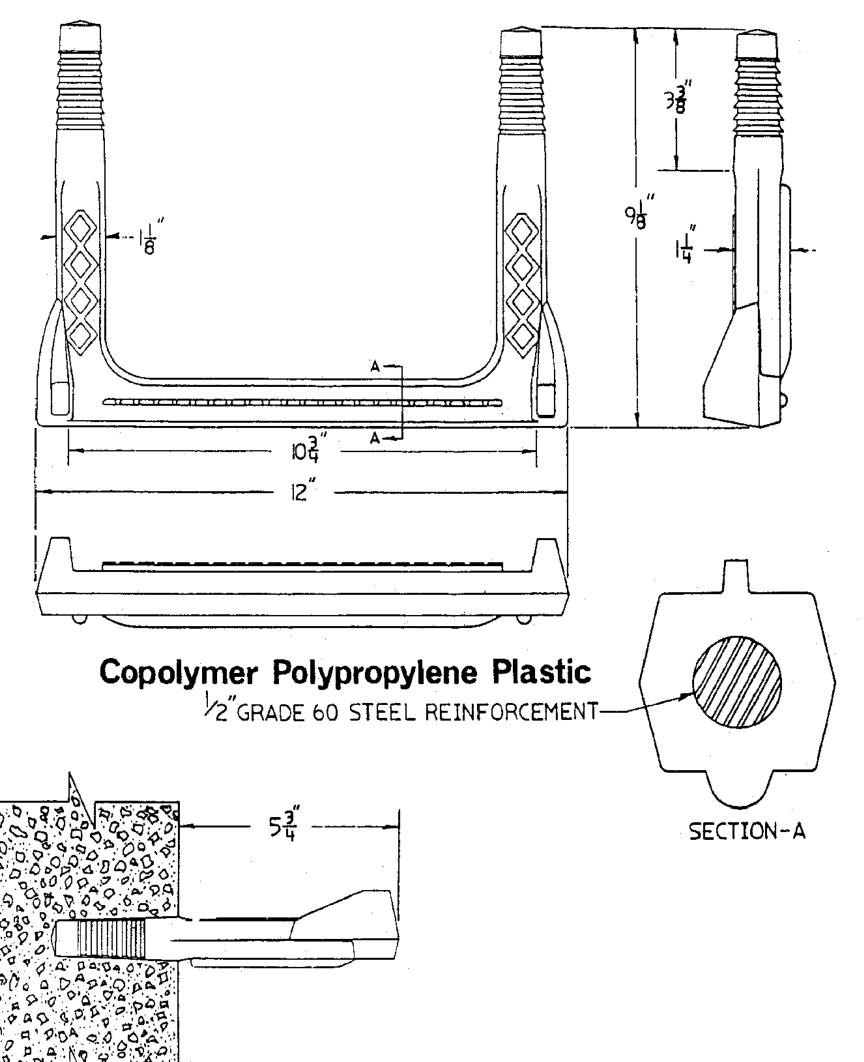
STANDARD WATER DOF BELLEVILLE

CITY OF BELLEV WAYNE COUNTY

SHEET **C7.3**







03/29/05 NTS**DESIGNED BY:** ES

DRAWN BY: ESCHECKED BY:

REVISIONS

PER CITY 09/08/06

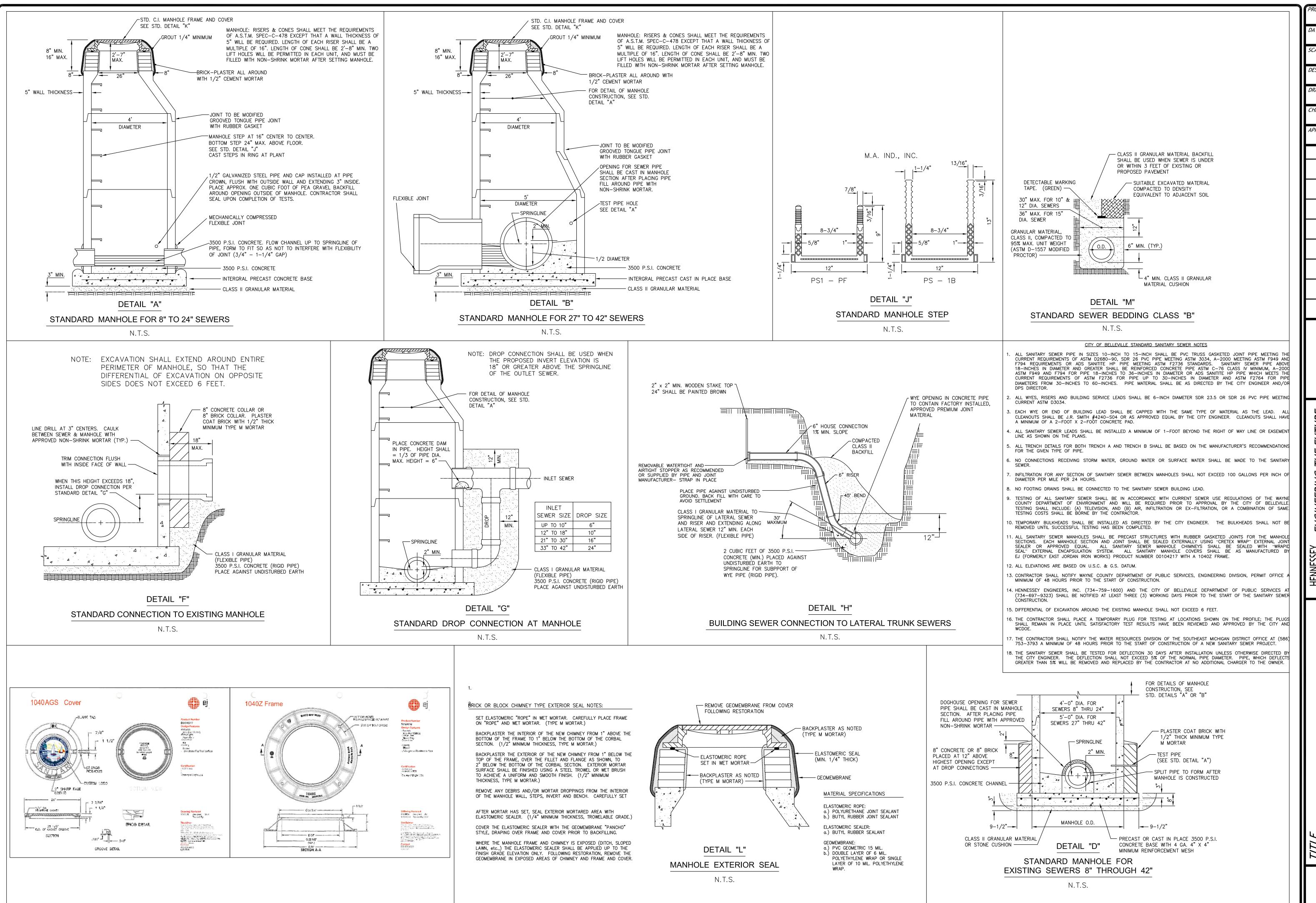
REVISED CASTINGS 10/12/15



DETAILS F BELLEVILLE COUNTY, MICHIGA WATER STANDARD

7 OF NE (

SHEET C7.4



9/12/17 NTSDESIGNED BY. RSRDRAWN BY: CHECKED BY: *APPROVED BY:* **REVISIONS**

AII \geq S 日 NIT \mathcal{O} · O 日

SHEET

PROPOSED STORM STRUCTURE INFORMATION

	THOI OSED STORM STROOTORE IN ORIMINTOR				
! 1	CB #14	CB #29	CB #42	CB #57	
676.50	RIM:" 676.25	RIM: "677.00	RIM: 677.00	RIM: "67	
NV: 673.80	12" INV: 673.05	12" INV: 673.75	12" INV: 672.61	15" IN\	
				15" IN\	
[!] 2	CB #15	CB #30	CB #43	OD #5	
677.00	RIM: 676.25	RIM: 677.00	RIM: 676.75	CB #58 RIM: 67	
NV: 673.47 NV: 673.47	12" INV: 671.76	12" INV: 673.45	12" INV: 672.37 30" INV: 670.87	15" IN\	
NV: 6/3.4/	12" INV: 671.76	12" INV: 673.45	30" INV: 670.87	15" IN\	
! 3	24" INV: 670.76	CB #31	30 INV. 670.87	13 111	
676.50	12" INV: 671.76	RIM:" 677.00	CB #44	CB #59	
NV: 673.77	CB #16	12" INV: 673.84	RIM: 676.50	RIM: "67	
	RIM: "676.25		30" INV: 670.77	12" IN\	
4	12" INV: 673.05	CB #32	30" INV: 670.77	"-	
676.50		RIM: 676.75	OD #45	CB #60	
NV: 673.08	CB #17	12" INV: 673.26	CB #45 RIM: 676.50	RIM: 67	
NV: 673.08	RIM: 676.25	12" INV: 673.26	30" INV: 670.66	42" IN 42" IN	
NV: 673.08	24" INV: 670.67	CB #33	30" INV: 670.66	42 IN 15" IN	
[!] 5	24" INV: 670.67	RIM: 677.00	30 1111. 070.00	12" IN\	
676.50	12" INV: 671.67	12" INV: 673.18	CB #46		
NV: 672.63		12" INV: 673.18	RIM: 676.80	CB #6	
NV: 672.63	CB #18	CB #34	18" INV: 670.77	RIM: 67	
	RIM: 676.25	RIM: 676.75	CB #47	42" IN	
[!] 6	12" INV: 673.05	12" INV: 672.80	RIM: 676.50	42" IN	
677.00	CB #19	15" INV: 672.80	18" INV: 670.57	CB #62	
NV: 673.17	RIM: 676.25		18" INV: 670.57	RIM: 67	
ı —	30" INV: 669.86	MH #3 RIM: 677.60		12" INV	
¹ 7	24" INV: 670.36	15" INV: 672.64	CB #48		
677.25	12" INV: 671.36	15" INV: 672.64	RIM: 676.50	CB #63	
NV: 672.50			18" INV: 670.40	RIM: 67	
INV: 671.50 NV: 672.00	CB #20	CB #35	24" INV: 670.40	18" IN\	
111. 072.00	RIM: 676.75	RIM: 677.00	CB #49	12" IN\	
10	30" INV: 669.60	15" INV: 672.54	RIM: 676.25	CB #6	
[!] 8 678 65	30" INV: 669.60	18" INV: 672.54	24" INV: 670.29	RIM: 67	
678.65 INV: 671.39	05 //04	CB #36	30" INV: 670.54	15" IN\	
INV: 671.39	CB #21	RIM: 677.00	42" INV: 669.54	15" IN\	
1111. 071.33	RIM: 676.75 12"INV: 673.56	18" INV: 672.46			
<u> </u>	12 1111. 675.56	18" INV: 672.46	CB #50	CB #65	
676.75	CB #22	CB #37	RIM: 677.40	RIM: 67 18" IN\	
NV: 673.51	RIM: 676.75	RIM: 677.00	12" INV: 673.57	15" IN\	
	12" INV: 673.37	18" INV: 672.32	CB #51		
¹ 10	12" INV: 673.37	18" INV: 672.32	RIM: 677.00	CB #66	
677.25		OD #30	12" INV: 673.28	RIM: 67	
INV: 671.31	CB #23	CB #38 RIM: 677.00	12" INV: 673.28	12" IN\	
INV: 671.31	RIM: 676.75 12"INV: 672.99	18" INV: 672.24		00 //0	
NV: 672.31	12" INV: 672.99	18" INV: 672.24	CB #52	CB #67 RIM: 67	
11	12 1111. 072.99	10 1144. 072.21	RIM: 676.60	18" IN\	
677.75	CB #24	CB #39	15" INV: 672.95	12" IN\	
NV: 671.12	RIM: 676.75	RIM: 677.25	12" INV: 672.95	12 1111	
NV: 671.12	24" INV: 673.54	12" INV: 673.90	00 //57	CB #68	
		MII #0	CB #53	RIM: 67	
12	CB #25	MH #2 RIM: 676.60	RIM: 676.50 15" INV: 672.62	18" IN\	
677.60 NV: 671.01	RIM: 676.75	18" INV: 672.16	15" INV: 672.62	42" IN	
NV: 671.01	12" INV: 672.55	18" INV: 672.16	10 HVV. 0/2.02	48" IN\	
NV: 671.01	12" INV: 672.55	10 HVV. 0/2.10	CB #54	00 //0	
13	15" INV: 672.55	CB #40	RIM: 676.75	CB #69	
677.00		RIM." 677 00	42" INIV: 669 34	RIM: 67	

30" INV: 670.93

CB #56

RIM: 677.20

15" INV: 672.09

OVERALL STORM SEWER LAYOUT

CB #26

CB #27

RIM: 676.75

RIM: 676.75

CB #28 RIM: 676.75

12" INV: 672.22

15" INV; 672.22

15" INV: 672.22

30" INV: 669.51

15" INV: 670.76

12" INV: 673.50

677.00 INV: 671.85 INV: 671.85 677.40 INV: 671.61 INV: 671.61 678.60 INV: 673.53 677.30 INV: 669.09 INV: 669.09 INV: 671.34 INV: 671.59 677.80 INV: 669.00 INV: 669.00 678.00 INV. 672.97 |63 678.00 INV: 672.32 INV. 672.32 ||64 677.50 INV: 673.27 INV: 673.27 |65 677.50 INV: 673.06 INV: 673.06 #66 677.50 INV: 673.64 #67 677.50 INV: 672.60 INV: 672.60 677.05 INV: 671.40 INV: 668.90 INV: 668.90 CB #69 RIM: 677.50 RIM: 676.75 RIM: "677.00 42" INV: 669.34 48" INV: 668.80 42" INV: 669.34 12" INV: 672.54 48" INV: 668.80 18" INV: 672.04 15" INV: 671.59 30" INV: 671.04 CB #70 CB #55 RIM: 677.30 RIM: 676.25 CB #41 RIM: 676.50 48" INV: 668.72 42" INV: 669.22 48" INV: 668.72 30" INV: 670.93 42" INV: 669.22

CB #71

RIM: "677.50

48" INV: 668.62

48" INV: 668.62

48" INV: 668.22 CB #78 RIM: 676.50 12" INV: 672.83 CB #79 RIM: 676.50 12" INV: 669.02 48" INV: 666.02 48" INV: 666.02 CB #80 RIM: 676.50 12" INV: 672.78 CB #81 RIM: 677.00 12" INV: 672.36 12" INV: 672.36 CB #82 RIM: "677.07 12" INV: 674.18 CB #83 RIM: "678.07 12" INV: 673.93 12" INV: 673.93 CB #84 RIM: "678.74 12" INV: 675.80 CB #85 RIM: 678.74 15" INV: 673.75 12" INV: 673.75

12" INV: 675.40

12" INV: 675.80

15" INV: 673.66 12" INV: 673.66

12" INV: 675.06

15" INV: 673.50 15" INV: 673.50

CB #86 RIM: 678.74

CB #87

MH #88

SCALE: 1" = 120'-0"

RIM: 678.90

RIM: 678.74

CB #72 RIM: 678.30

MH #4

CB #73

12" INV: 674.85

RIM: 678.35 12" INV: 672.55 12" INV: 672.55 12" INV: 672.55

RIM: 677.00 12" INV: 673.30

CB #74 RIM: 677.10 48" INV: 668.53

48" INV: 668.53 12" INV: 671.53

CB #75 RIM: 677.50 12" INV: 672.59

CB #76 RIM: 677.40 48" INV: 668.37

48" INV: 668.37 12" INV: 671.37

48" INV: 667.91 48" INV: 667.91

CB #77 RIM: 677.00 48" INV: 668.22

MH #1 RIM: 678.80

BELLEVILLE HIGH SCHOOL
EXPANSION AND REMODELING

PUBLIC SCHOOLS LE, MICHIGAN

BUREN

/AN BUR BELLE

\[\]

O

And feest

>

(1)

-

CO

4

SU1.

SEWER STORM

OVERALL

BELLEVILLE HIGH SCHOOL 209035.00 (BID PACKAGE #2)

